## LOGIX INSULATED CONCRETE FORMS <br> DESIGN MANUAL (USA)

## Build Anything Better. ${ }^{\text {TM }}$




## 1.0 - SYSTEM OVERVIEW

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## 1.1 - APPLICATION \& USE

Logix Insulated Concrete Forms are used to create solid reinforced concrete walls that are pre-insulated for use both above-and below-grade. Logix walls are particularly effective for residential, multi-residential, commercial, institutional, and industrial buildings.

Logix is available in a wide variety of special form units and accessories, including corners, brick ledges, straight panels, t-walls, pilasters, and knock-down forms permit the Logix system to be adapted to many different situations. Logix forms are available in 8 inch ( 203 mm ), 12 inch ( 305 mm ) and 16 inch ( 406 mm ) height for additional design flexibility. See Section "1.2-PRODUCT SPECIFICATION TABLE" on page 5.


## Typical ICF Components

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 1.1 - APPLICATION \& USE cont'd




## 1.2 - PRODUCT SPECIFICATION TABLE

Logix manufactures both assembled and unassembled insulated concrete form units. Logix assembled forms, known as "Logix PRO", are delivered to the job site as assembled form blocks. Logix unassembled forms (or knock-down forms), known as "Logix KD", are delivered to the job site in components that make up the form blocks - the form panels and KD Connectors. Logix KD are assembled on the job site.

Below is a summary of the types of Logix PRO and Logix KD forms available. However, contact a local Logix representative for availability of specific Logix products.

Logix PRO (assembled form blocks)

|  | DESCRIPTION |
| :--- | :--- |
| Logix Pro | White in color |
| Logix Pro Platinum ${ }^{3}$ | Offers higher R-value ${ }^{1}$ than Logix Pro. <br> Grey in color. Made with BASF Neopor. |
| Logix Pro TX | Logix Pro with termite resistant additive <br> Preventol $^{2}$. White in color. |
| Logix Pro Platinum ${ }^{3}$ TX | Logix Pro Platinum with Preventol. <br> Grey in color. |

Logix KD (unassembled form blocks)

|  | DESCRIPTION |
| :--- | :--- |
| Logix KD | White in color |
| Logix KD Platinum ${ }^{3}$ | Offers higher R-value ${ }^{1}$ than Logix KD. <br> Grey in color. Made with BASF Neopor. |
| Logix KD TX | Logix KD with termite resistant additive <br> Preventol $^{2}$. White in color. |
| Logix KD Platinum ${ }^{3}$ TX | Logix KD Platinum with Preventol. Grey <br> in color. |

Notes:

1. See Section 8.5 for Logix $R$-values.
2. Preventol is an effective termite resistant additive.
3. Care should be taken to protect exposed foam surfaces from reflected sunlight and prolonged solar exposure until wall cladding or finish material is applied. Shade exposed foam areas, or remove sources of reflective surfaces, where heat build up onto exposed foam might occur. For more information refer to BASF Technical Leaflet N-4 Neopor, "Recommendations for packaging, transporting, storing and installing building insulation products made from Neopor EPS foam." (The BASF Technical Leaflet is attached to every bundle of Logix Platinum forms delivered to a job site).

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 1.2 - PRODUCT SPECIFICATION TABLE cont'd

| LOGIX <br> FORM <br> PANELS | STANDARD |  |  |  |  | TAPER TOP |  |  |  |  | BRICK LEDGE |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 只 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Conc.Core Thickness | 4 | 6.25 | 8 | 10 | 12 | 4 | 6.25 | 8 | 10 | 12 | 4 | 6.25 | 8 | 10 | 12 |
| Width Top ${ }^{1}$ | 9.5 | 11.75 | 13.5 | 15.5 | 17.5 | 9.5 | 11.75 | 13.5 | 15.5 | 17.5 | 13.375 | 15.625 | 17.375 | 19.375 | 21.375 |
| Width Bot. ${ }^{1}$ | 9.5 | 11.75 | 13.5 | 15.5 | 17.5 | 9.5 | 11.75 | 13.5 | 15.5 | 17.5 | 9.5 | 11.75 | 13.5 | 15.5 | 17.5 |
| Form Type ${ }^{2}$ | KD/P | KD/P | KD/P | KD/P | KD | KD | KD/P | KD/P | KD/P | KD | KD/P | KD/P | KD/P | KD/P | KD |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Conc.Core Thickness |  |  |  |  |  | 4 | 6.25 | 8 | 10 | 12 | 4 | 6.25 | 8 | 10 | 12 |
| Width Top ${ }^{1}$ |  |  |  |  |  | 9.5 | 11.75 | 13.5 | 15.5 | 17.5 | 13.375 | 15.625 | 17.375 | 19.375 | 21.375 |
| Width Bot. ${ }^{1}$ |  |  |  |  |  | 9.5 | 11.75 | 13.5 | 15.5 | 17.5 | 9.5 | 11.75 | 13.5 | 15.5 | 17.5 |
| Form Type ${ }^{2}$ |  |  |  |  |  | KD | KD | KD | KD | KD | KD | KD | KD | KD | KD |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Conc.Core Thickness |  |  |  |  |  |  |  |  |  |  | 4 | 6.25 | 8 | 10 | 12 |
| Width Top ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  | 17.25 | 19.5 | 21.25 | 23.25 | 25.25 |
| Width Bot. ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  | 9.5 | 11.75 | 13.5 | 15.5 | 17.5 |
| Form Type ${ }^{2}$ |  |  |  |  |  |  |  |  |  |  | KD | KD | KD | KD | KD |

1. Width at Top and Bottom is measured from outside face to outside face of forms.
2. "KD" and "P" denotes Logix KD (unassembled forms) and Logix PRO (assembled forms), respectively.

3. "KD" and "P" denotes Logix KD (unassembled forms) and Logix PRO (assembled forms), respectively.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 1.2 - PRODUCT SPECIFICATION TABLE cont'd



1. "KD" and "P" denotes Logix KD (unassembled forms) and Logix PRO (assembled forms), respectively.

2. Height of forms for Half Height Forms $=8$ inches

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 1.2 - PRODUCT SPECIFICATION TABLE cont'd

| V12 <br> Logix <br> FORM <br> PANELS | V12 STANDARD |  |  |  |  | V12 TAPER TOP |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 足 |  |  |  |  |  |  |  |  |  |  |
| Conc.Core Thickness | 4 | 6.25 | 8 | 10 | 12 | 4 | 6.25 | 8 | 10 | 12 |
| Width Top ${ }^{1}$ | - | 11.75 | 13.5 |  |  |  | 11.75 | 13.5 |  |  |
| Width Bot. ${ }^{1}$ |  | 11.75 | 13.5 |  |  |  | 11.75 | 13.5 |  |  |
| Form Type ${ }^{2}$ | - | KD/P | KD/P | - |  |  | KD/P | KD/P | - | - |


|  | V12 Left Hand Corner Form | V12 Right Hand Corner Form |
| :---: | :---: | :---: |
| Form Type ${ }^{1}$ | KD/P | KD/P |
|  |  |  |
| Form Type ${ }^{1}$ | KD/P | KD/P |
|  |  |  |
| Form Type ${ }^{1}$ | KD/P | KD/P |

1. Width at Top and Bottom is measured from outside face to outside face of forms.
2. "KD" and "P" denotes Logix KD (unassembled forms) and Logix PRO (assembled forms), respectively.

## 1.3 - ACCESSORIES



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## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.1 - INTRODUCTION

For builders who want a competitive edge, Logix offers solid products and friendly local service. Our products are designed to perform better in the field, providing trouble-free, profitable installations time after time.

Our technical team is ready to respond to your queries with practical advice on quick and efficient installation. With contractor training provided through our numerous regional technical support offices, help is always close at hand.

We are the most experienced ICF manufacturers in North America, manufacturing top quality products at our nine plants located throughout the United States and Canada.

For more information, or to contact a Logix representative, visit our website at www.Logixicf.com and click "Contact Us". You can also register online to receive Logix updates.

This manual will be updated regularly. Current updates will be available at www.Logixicf.com.

## 2.2 - USEFUL TOOLS \& MATERIALS

- Pruning saw
- Cordless drill
- Screws
- Hot knife
- Electric chainsaw
- Fiberglass-reinforced tape
- Step ladder
- Rebar bender/cutter
- Internal vibrator
- Contractor-grade foam gun
- Low expansion foam adhesive
- Approved scaffold planks
- Transit or laser
- 48" (1220mm) level
- Bolt cutters
- String line
- Chalk line
- Wall alignment system (safety compliant)
- 36 inch (914 mm) plastic zip ties, or Logix Vertical \& Horizontal Hooks
- Concrete embedments
- Window and door buck material
- Sleeves for wall penetrations

NOTE: For more information on Logix Vertical \& Horizontal Hooks see Technical Bulletin No. 20

## 2.3 - ACCURATE FOOTINGS \& SLABS

The first step to a successful Logix installation is an accurate footing or slab. This means a footing or slab that is:

- Code compliant
- Designed in accordance with construction drawings and specifications
- Designed taking into account soil conditions, seismic area, number of stories, building loads, and water tables.



## 2.4 - WALL LAYOUT

Accurate wall layout is critical to ensure a complete and profitable Logix project.
Verify that wall layout is in accordance with plans and specifications.
In addition to straight Standard forms, Logix provides $45^{\circ}$ and $90^{\circ}$ corner form blocks. However, Logix can be easily cut on-site to fit any corner angle or radius. See "2.7.8 - RADIUS WALLS" on page 26.

Snap chalk lines


## 2.5 - PRODUCT HANDLING \& PLACEMENT

There are several methods to efficiently handle Logix forms. Unlike most ICF systems, the consistent 2-3/4 inch (70 mm ) panel thickness on Logix forms means that handling damage is minimized.


- Logix Standard Forms arrive stacked on disposable skids.
- The forms are strapped together for easy handling.
- Unloading can be accomplished manually or using alternate lifting equipment.
- Standard forms can be moved by two people using two $2 x 4 s$
- Corner forms come in bundles of four or twelve, and can easily be carried by one or two people.
- Specialized dollies are another convenient way to move Logix bundles.
- When transporting forms on an open trailer, position the forms so the wind travels through the webs to minimize drag.
- When tying forms down on an open trailer, ensure the forms are well secured and avoid form damage from strapping materials.
- If job site conditions require form protection, Logix bundle bags can be ordered.
- Logix forms are produced to the tightest tolerance in the industry, with a length tolerance of +/-1/8 inch ( $+/-3 \mathrm{~mm}$ ), and a height tolerance of $+/-1 / 16$ inch ( $+/-2 \mathrm{~mm}$ ).

When forms are unloaded, it is necessary to measure forms to determine uniform length and height. It is suggested to measure 2 forms per skid. In the unlikely event that forms are out of spec, please contact the local Logix representative immediately. Build Anything Better.

## 2.6 - JOBSITE EFFICIENCY

An efficient jobsite means a faster and safer installation, and ultimately a higher quality finished project.

- Keep all materials and tools outside of the footing area until the chalk lines have been snapped and the wall layout is complete. Generally, construction is accomplished from within the perimeter of the structure.
- When wall layout is complete, place forms at least 7 feet $(2.134 \mathrm{~m})$ inside the perimeter of the footings or slab to accommodate the wall alignment system.

- Space skids of standard forms around the inside of the entire perimeter.

NOTE: When placing courses of forms, always take forms from the closest skid. This will eliminate the effects of normal manufacturing variations between skids.

- Periodic checking of dimensions ensures accurate wall construction.
- Additional materials that should be located within the perimeter:
- Window and door bucks
- Rebar (straight or pre-bent)
- Alignment system
- Approved scaffold planks
- Tools


## 2.7 - LOGIX WALL CONSTRUCTION

When a form is cut, it can be identified using bars and webs. For example, a cut form with three bars, two webs, and three bars will be referred to as a " $3-2-3$ ".


By establishing a logical form pattern that takes into account the building dimensions, maximum efficiency will be achieved. It is important that the building dimensions have a tolerance of $+/-1 / 2^{\prime \prime}$ inch ( 13 mm ) or a stacked vertical joint will result. Such joints are acceptable if dimensions necessitate but will require additional form support on both sides of the form.

When building dimensions are based on 4 feet ( 1.219 m ) increments, it is suggested to alternate between left- and right-hand corners within each course.


Alternating corner forms

## 2.7 - Logix WALL CONSTRUCTION cont'd

### 2.7.1 - THE FIRST COURSE



STEP 1: Start first course at a corner and align with chalk line.


STEP 3: Secure forms end-to-end to maintain building dimensions using zip ties or Logix Hooks.
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$\cup$
$\supset$
$\underset{c}{ }$
STEP 2: Continue placing forms along the chalk line.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.7 - Logix WALL CONSTRUCTION cont’d



STEP 4: When forms are 4 ft or less from the second corner, place the second corner form.


STEP 5: Cut a Standard form to fit the space left between the corner and the previous Standard form.

At this point, determine if adjustments are needed to the building dimensions so the cut can be made on a line. If adjustments are needed, alter chalk lines accordingly.


If more than 3 bars are extending beyond any web, additional form support is required on both faces of the form.
STEP 6: Continue around the wall in this manner until the first course is complete and dimensions are verified.
Leave the first course of forms in place across door openings and low windows until forms have been placed and building dimensions have been verified to maintain the interlock pattern above openings.

STEP 7：Place necessary rebar in first course as specified and according to local code．
NOTE：Web ties are designed with＇rebar slots＇to provide secure placement of horizontal rebar，and allows for non－ contact lap splices．See＂2．8．2－HORIZONTAL \＆VERTICAL REINFORCEMENT＂on page 29.

STEP 8：Prior to starting the second course，install additional form support if required．


## 2．7．2－THE SECOND COURSE

STEP 1：Starting at the original corner，place appropriate corner form．When possible，alternate between left－and right－hand corners between courses．This will create a 16 ＂offset．

NOTE：It is necessary to firmly seat every form to the form below to minimize interlock settling．The interlock system is designed to secure forms betweens courses，which helps minimize form settling and movement during installation and concrete placement．

STEP 2：Continue placing forms around the wall，working in the same direction as the first course． Make sure to secure forms end－to－end，and between courses，with zip ties，Logix Hooks or foam adhesive．


## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.7 - Logix WALL CONSTRUCTION cont'd

(1)

STEP 3: All webs should line up vertically, except where building dimensions are other than 8 inch (203 mm ) increments. In this case, special cuts may be required to allow vertical alignment of webs. Webs are aligned when markers on the face of the form are vertically aligned.


STEP 4: Place necessary rebar after completion of second course.

NOTE: Web ties are designed with 'rebar slots' to provide secure placement of horizontal rebar, and allows for non-contact lap splices.


STEP 5: Form Lock can also be placed in the second course, if desired. Overlap Form Lock lengths by roughly 8 inch ( 203 mm ). Align the points of the zigzag pattern in the Form Lock directly above the webs.


STEP 6: Confirm that the wall is straight and level. If adjustment is required, shim or trim the bottom of the wall until level is achieved.

STEP 7: Use foam adhesive to fasten the straightened and leveled wall to the footing or slab. Insert the nozzle 1 inch ( 25 mm ) at the base of every other web along the chalk line, and shimmed and trimmed locations, and inject foam between the block and the footing.


When vertical joints are less than 8 inches ( 203 mm ) apart, additional form support is required.
It is important to note that at this point the wall pattern has been established. Course number 1 will be the pattern for all odd numbered courses ( $3,5,7$, etc.). Course number 2 will be the pattern for all even numbered courses.

Wall alignment system to be installed at some point between the second and fourth courses, at no more than 7 feet $(2.134 \mathrm{~m})$ intervals. See "2.11 - WALL BRACING \& ALIGNMENT SYSTEM" on page 44.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.7 - Logix WALL CONSTRUCTION cont'd

### 2.7.3 - ADDITIONAL COURSES

Installation of additional courses is the generally the same as the second course, described in the previous section.
STEP 1: Fasten every corner end-to-end to adjoining forms using zip ties, Logix Hooks, or adhesive foam.
Install Form Lock, if desired, every fourth of fifth course after the second course.
STEP 2: After completion of each course, place necessary rebar as specified and according to local code.
STEP 3: Secure forms end-to-end in the top course to maintain building dimensions.
STEP 4: Secure the top course to the forms below on both sides to prevent tipping during concrete placement.


STEP 5: If additional stories are planned, the interlock needs to be protected prior to concrete placement.

When vertical joints are less than 8 inches ( 203 mm ) apart additional form support is required.
If you need to stack identical corners in subsequent courses, you will need to provide additional form support where the stacked joints are created.


Vertical stacked joints requires additional form support.

Hold all reinforcement back 2 inches ( 51 mm ) from door and window buck material to ensure proper concrete coverage.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.7 - Logix WALL CONSTRUCTION cont'd

### 2.7.4 - CORNER BRICK LEDGE

Brick Ledge forms come only in straight units, so mitered cuts on site must be made to create corners with these blocks. Two methods can be used:

1. Freehand miter cutting.
2. Using a template.

NOTE: On a 6.25 inch ( 159 mm ) Logix Brick Ledge always start a miter cut in the middle of the first web beyond the corner form.

Extending a Brick Ledge block two webs beyond the corner block and making the cut will create a remaining piece that can be used for an inside corner elsewhere in the layout.


STEP 1: With the first Brick Ledge block, make a miter cut on the Brick Ledge panel.


STEP 3: With the second Brick Ledge block, make similar miter and butt-joint cuts.


STEP 2: With the first Brick Ledge block, make a buttjoint cut flush to the form below.


STEP 4: Place both cut Brick Ledge blocks to create the Brick Ledge $90^{\circ}$ corner.

## 2.7 - Logix WALL CONSTRUCTION cont'd



STEP 5: Secure the corner Brick Ledge with tape and foam.


STEP 6: Place rebar, as required, and remove foam from cavity where necessary.


DETAIL A

* $1 \mathrm{kN}=224.8 \mathrm{lb}$

See Section 6 -
Engineering in the LOGIX
Product Manual for
reinforcement details

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.7 - Logix WALL CONSTRUCTION cont'd

### 2.7.5 - KNOCK-DOWN FORMS

Logix Knock-down forms (Logix KD) are designed to offer the same benefits as the Logix solid forms (Logix PRO). However, Logix KD forms also

- reduce shipping costs and inventory requirements
- accommodates tilt-up wall panel construction
- allows hassle-free assembly of forms around complex rebar patterns (i.e. stirrup or rebar cage pattern in walls)
- allows custom block configurations (i.e. Taper Top-Brick Ledge, etc...)

Knock-down ties (KD connectors) connect to the embedded furring tabs


Logix KD Standard Form - disassembled view.


Logix KD Standard Form - assembled view.

### 2.7.5.1 - PRODUCT HANDLING

There are several methods to efficiently handle Logix KD forms. The high foam density and consistent 2-3/4 inch (70 mm ) panel thickness on Logix KD means that handling damage is minimized.

The forms arrive on-site unassembled. KD Connectors and panels arrive on-site packaged in boxes and bundled in stacks, respectively.

### 2.7.5.2 - ASSEMBLING AND INSTALLATION

As the forms are assembled on-site they are stacked in place to form the walls. Stacking the blocks, including required tools and methods, are the same when using Logix Pro forms.

Top and bottom KD connectors are required for each furring tab.

Connectors are inserted with rebar slots facing up.



## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.7 - Logix WALL CONSTRUCTION cont'd

### 2.7.5.3 - CORNER FORM SUPPORT

For any type of ICF knock-down system it is good practice to provide additional form support at the corners.
To ensure a safe and proper concrete pour the following corner form support is recommended:

- Using 2.5 inch ( 64 mm ) wood screws to fasten $2 \times 6$ vertically to the embedded furring tabs on both sides of the corner.
- For outside corners wrap steel strapping around the corners. For the bottom third of the concrete pour height evenly space two strappings for each course. Then one strap per course for the remaining pour height. Using 1.5 inch ( 38 mm ) wood screws the bands should attach to at least two furring tabs that
- For inside corners apply typical bracing as required.


Example of outside corner form support for KD forms.


Example of inside corner form support for KD forms.

### 2.7.6 - TEE WALLS

Wall T-junctions can be constructed using Logix T-walls, or by field-cutting Logix Standard forms.
Logix T-walls arrive to the job site assembled or disassembled. When assembled Logix T-walls provide sizes that are commonly used in construction. Each T-wall size comes in two different shapes, a long and short section, so that a running bond pattern is created when the T-wall forms are stacked.

Installation of Logix T-walls is straightforward. As with all Logix forms, the T-walls are stacked in the usual running bond pattern, and follows the same basic installation instructions detailed in "2.7-LOGIX WALL CONSTRUCTION" on page 10 .


| Logix T-wall <br> Sizes | Description |
| :--- | :--- |
| 4 to 6 | $4^{\prime \prime}$ connected to 6.25" Logix |
| 4 to 8 | $4^{\prime \prime}$ connected to $8^{\prime \prime}$ Logix |
| 4 to 10 | $4^{\prime \prime}$ connected to 10" Logix* |
| 4 to 12 | $4^{\prime \prime}$ connected to 12" Logix* |
| 6 to 6 | $6.25^{\prime \prime}$ connected to 6.25" Logix |
| 6 to 8 | $6.25^{\prime \prime}$ connected to 8" Logix |
| 6 to 10 | $6.25^{\prime \prime}$ connected to $10^{\prime \prime}$ Logix* |
| 6 to 12 | $6.25^{\prime \prime}$ connected to $12^{\prime \prime}$ Logix* |
| * Assembled without diagonal ties. |  |



## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.7 - Logix WALL CONSTRUCTION cont'd

### 2.7.6.1 - FIELD-CUT T-WALLS

When necessary, t-walls can be made field cutting Standard forms, or straight blocks.


When the entire wall has been checked for plumb and square, apply foam adhesive to the butt joints, and install additional form support, as required.

Another option for building a t-wall is to construct the entire continuous wall first. This method requires preplanning to ensure there is adequate reinforcement at every course to allow the t-wall to be attached securely. All other steps above need to be applied.

### 2.7.7 - GABLE WALLS

The preferred method to construct a gable end is on the floor to be installed as a one-piece unit.


Make sure all necessary roof attachment hardware is available prior to concrete placement, as it must be installed during or immediately after the pour.

NOTE: Pieces of plywood can be screwed into the $1 \times 4$ s during placement to help contain the concrete.
Another option for constructing a gable wall is to assemble the gable in place. Set the pitch for the gable by marking the first course appropriately. Subsequent courses should follow this pattern.


## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.7 - Logix WALL CONSTRUCTION cont'd

### 2.7.8 - RADIUS WALLS

There are a number of different methods for creating radius walls with Logix. Below, is a guide that will create radius walls based on 8 inch segments of Logix.

NOTE: This process will result in vertically stacked joints, and additional form support will be required prior to concrete placement.

See "2.21 - RADIUS WALLS" on page 83, for radius wall tables.


STEP 1: Cut forms into 8" sections with web centered in each section.


STEP 3: Cut the 8 " section at the edges along the radius lines. Mark and cut all form sections using this template.


STEP 2: Mark radius lines for an $8^{\prime \prime}$ cut section.


STEP 4: Connect and secure sections with zip-ties, tapes and foam to create the first course. Repeat the steps for each additional course, and connect each with zip ties or Logix hooks.

### 2.7.9 - LOGIX D-RV

Logix $\mathrm{D}-\mathrm{Rv}^{\top \mathrm{M}}$ are 2 inch thick foam panels made with a drainage layer. It provides a quick and easy alternative to providing drainage with the added benefit of increasing the $R$-value of a Logix wall assembly.

(The drainage layer may be required, either by code or design, when a direct applied finish, such as stucco, is used on an exterior ICF wall).

Logix D-Rv can be installed into the Logix form blocks either before or while the form blocks are stacked to build the wall. This speeds up the construction process and eliminates the need to apply the drain layer to the exterior face after a Logix wall has been built.

Offsetting the vertical joints of the D-Rv™ panels with the vertical joints of the Logix forms will create a stronger, more rigid wall structure.

For more information contact your local Logix representative or see Technical Bulletin No. 36, Logix D-Rv™ in the Logix Technical Library.

## 2.8 - REINFORCEMENT

Reinforcing steel (rebar) strengthens concrete walls to help minimize cracking and buckling under load due to backfill, wind, and other loads. Rebar also helps control cracking due to temperature swings and shrinkage.


### 2.8.1 - BASIC REINFORCEMENT

- Reinforcing steel must meet the requirements of ASTM A615, ASTM A996, or ASTM A706 for low-alloy steel. Minimum of Grade 40 ( 300 MPa ).
- Reinforcing steel in a Logix wall must have minimum $3 / 4$ inch ( 19 mm ) concrete cover.
- Hold the reinforcement back from door and window openings by $2^{\prime \prime}$ ( 51 mm ), or as required by design, or local building codes.
- Refer to Section 6, Engineering for the Logix prescriptive engineering tables.
- It is the responsibility of the installer to verify table rebar specifications with local building codes and engineering specs.


### 2.8.2 - HORIZONTAL \& VERTICAL REINFORCEMENT

It is the responsibility of the installer to verify table rebar specifications to comply with local building codes and engineering specs.

Refer to Section 6 for Logix prescriptive engineering tables, and Section 5.2.1 for typical reinforcement details.



Rebar slots in the web ties allow for non-contact lap splices of horizontal rebar, the preferred method when creating lap splices.


## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.8 - REINFORCEMENT cont'd

### 2.8.3 - TYPICAL REINFORCEMENT AT OPENINGS

It is the responsibility of the installer to verify table rebar specifications to comply with local building codes and engineering specs.

Refer to Section 6 for lintel reinforcement tables, and lintel details.


### 2.8.4 - LINTELS

Appropriate lintel rebar should be placed in the proper sequence directly above doors and windows to carry loads over these openings.


Before placing forms across the top of door or window openings, rest the bottom lintel bar(s) on buck material.

NOTE: Form Lock can be installed across the entire length of the lintel span. In some cases it may be required to install top lintel rebar before installing Form Lock, in order to achieve necessary concrete cover.


Refer to Section 6 for lintel reinforcement tables, and lintel details.

## LOGIX® ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.9 - WINDOW \& DOOR BUCKS

Bucks provide attachment surfaces for windows and doors while holding back concrete from these openings during concrete placement. Mark the center and edges of openings as you place courses and cut blocks as needed.

Refer to the rough opening (R/O) dimensions for windows and doors. Provide for openings in the wall taking into consideration the thickness of the chosen buck material. See window and door manufacturer info for R/O dimensions.

Cross bracing is required for all window and door bucks approximately 18 inches ( 457 mm ) on center to help withstand the pressures of concrete placement.

Window and door openings within 4 feet ( 1.220 m ) of corners require additional horizontal strapping from corner to across the opening.

Prior to placing window or door buck, confirm that bottom lintel rebar has been installed.
Bucks can be made from EPS foam, lumber or vinyl. Logix Pro Buck, made of dense EPS foam, is recommended for use with Logix ICF.

### 2.9.1 - LOGIX PRO BUCK

Recommended for use with Logix ICF is the Logix Pro Buck system. Designed for Logix, Pro Buck creates a complete thermal break in window and door openings. And unlike wood and vinyl bucks, Pro Buck is light weight, faster and easier to install, while creating little job site waste. For more information refer to the Logix Pro Buck Installation Guide.

For efficiency, a table long enough to accommodate connecting and cutting Pro Buck sections together is recommended. This can be done by simply using a pair of sawhorses and a section of plywood, or $2 x$ lumber, such as $2 \times 10$ or $2 \times 12$ pieces.


## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.9 - WINDOW AND DOOR BUCKS cont’d

When the walls are built to the height of the opening installation of the Pro Buck can begin. The rough opening is measured between the Pro Bucks. Therefore, to account for the $1.5^{\prime \prime}$ thickness of Pro Buck, the opening in the Logix ICF wall should be cut 3 " wider and 3 " taller than the rough opening.


STEP 1: Assemble Pro Buck for the jambs, and cut the lapped ends to fit the height of the opening minus $1.5^{\prime \prime}$, which is the thickness of the Pro Buck at the header.


STEP 3: Install Pro Buck at the sill. To avoid debris in the wall cavity, cut min. $4^{\prime \prime}$ port holes at $16^{\prime \prime}$ on center before placing in the opening.


Cut a $2 x$ to fit the width of the opening between the two Pro Buck jambs. The $2 x$ should be centered and fastened to the exposed Pro Buck furring strips before setting into place. This will stiffen the Pro Buck, and prevent excessive deflection when placed.

STEP 2: Install Pro Buck at the header. Cut the lapped ends to fit the entire width of the opening. The ends of Pro Buck will sit directly on the Pro Buck jamb pieces.


STEP 4: Continue installing forms above the opening. Use zip ties around the tie-back loop to secure the Logix forms to the Pro Buck at the header.

Once the Pro Buck pieces are placed in the opening add $2 x$ wood bracing, and Pro Buck Brackets, to secure the Pro Bucks during concrete placement. Wood screws are recommended when fastening wood bracing to Logix Pro Buck.

NOTE: Using a membrane flashing is recommended to cover the joints between Pro Bucks and the Logix blocks.


1. Internal furring strips are easy to locate as they are in the same spot as the exposed furring strips that run across the face of Pro Buck.
2. Wind Devil fasteners are available from www.wind-lock.com. Finishes such as stucco, or acrylic textured finishes can be applied directly over Wind Devil fasteners.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.9 - WINDOW AND DOOR BUCKS cont'd

Non-corrosive wood screws are recommended for the attachment of window or door frames. Inset or flanged windows and doors are fastened to the furring strips molded into the Logix Pro Buck. The furring strips are anchored into the concrete providing proper load transfer from the window/door to the concrete substrate.

To determine the fastener type and spacing for load rated windows and doors, withdrawal and lateral load resistance of specific fasteners are provided below.

## Direct Fastening to Furring Strips

|  | Allowable Withdrawal $^{1}$ | ${\text { Allowable } \text { Lateral }^{1}}^{\text {\#6 wood screw, min 1" long }}$ |
| :--- | :---: | :---: |
| \#8 wood screw, min 1.25" long | 30 lb | 72 lb |
| \#10 wood screw, min 1" long | 38 lb | 188 lb |

1. Withdrawal factor of safety $=5$, allowable lateral load based on the lesser of factor of safety of 3.2 or $75 \%$ of proportional limit. Based on independent fastener testing conducted by QAI Laboratories, in accordance with ASTM D1761, and ASTM E2634. and lateral load resistance of specific fasteners are provided below.

Direct Fastening of Logix Wall Plate

|  | Allowable Withdrawal $^{1}$ | Allowable Lateral $^{1}$ |
| :--- | :---: | :---: |
| $\# 8-18 \times 1{ }^{\text {" }}$ " long self-tapping screw | 102 lb | 142 lb |
| $\# 10-16 \times 1.5^{\prime \prime}$ long self-tapping screw | 106 lb | 171 lb |

1. Withdrawal factor of safety $=5$, lateral resistance factor $=0.5 \& 0.53$ for \#8 and \#10 screws, respectively. Based on independent fastener testing conducted by QAI Laboratories, in accordance with ASTM D1761, and ASTM E2634.

To insert Logix Wall Plate cut a narrow slit on the face of Pro Buck.



Bracing support for opening can support the Wall Plate during concrete placement.

Wall Plate at front face of Pro Buck reinforcement.

The Wall Plate securely anchors into the concrete core. When placed transversely to the opening holes punched in the Wall Plate allow for the placement of perimeter

Pro Buck can also be installed length wise along the opening and temporarily fastened to the furring strips at predrilled holes, if required.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.9 - WINDOW AND DOOR BUCKS cont'd

### 2.9.2 - TREATED PLYWOOD BUCK

Following are several methods for building bucks. Regardless of the method chosen, pre-planning is required to optimize chosen finish materials.

STEP 1: Rip 3/4 inch ( 19 mm ) treated plywood to full form width.
STEP 2: Rip treated $2 \times 4$ diagonally on table saw at $180^{\circ}$ angle.

STEP 3: Assemble buck with appropriate fasteners with $2 x 4 s$ creating a dovetail detail.
STEP 4: Assemble buck sides and top with access holes cut in bottom piece for placement of concrete. Two $2 x 4 s$ can also be used for the bottom to allow concrete placements.

STEP 5: Place pre-assembled buck in opening and fasten in place with foam adhesive. The buck can also be installed in opening as separate pieces.

STEP 6: Install temporary cross bracing to withstand concrete pressure. Attaching screws through the buck and into closest webs can provide additional buck support.

NOTE: Pressure treated wood for window bucks are normally required only if the bottom of the window buck frame is located at or below ground level. Check with local building codes to determine if your area requires pressure treated window bucks.


### 2.9.3 - SOLID WOOD BUCK

STEP 1: Choose appropriate wood product based on the dimension of the forms:

- 4" (102mm) form: $9.5^{\prime \prime}(241 \mathrm{~mm})$
-6.25" (159mm) form: $11.75^{\prime \prime}$ (298mm)
- 8" (203mm) form: 13.5" (343mm)
- 10" ( 254 mm ) form: 15.5" (394mm)

STEP 2: Cut top piece of buck to fit the width of the opening.
STEP 3: Cut sides of buck, remembering that the top piece rests on the side pieces.
STEP 4: Cut two $2 x 4 s$ for the bottom to allow concrete placement.
STEP 5: Assemble buck and place in opening.
STEP 6: Once the buck is in place, it must be centered and secured. This can be done by attaching $1 \times 4 \mathrm{~s}$ to the edges of the buck, extending the edge of the $1 \times 4$ over the foam to hold the buck firmly in place. Alternately, the buck can be secured with foam adhesive and tape.

STEP 7: Solid wood bucks will require additional concrete anchors to create a permanent attachment to the concrete.


## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 2.9 - WINDOW AND DOOR BUCKS cont'd

### 2.9.4 - RADIUS OPENINGS

Radius windows and doors can be assembled at the site with shortened pieces of Logix Pro Buck or lumber buck material.

STEP 1: Create the template for the radius opening with OSB or plywood that matches door or window rough opening.

STEP 2: Using template, draw outline of radius on wall, allowing for buck material thickness. Cut accordingly.

STEP 3: Cut buck material into approximately 4 inch ( 102 mm ) widths to create radius buck.
STEP 4: Cut side and bottom buck pieces. Leave openings in the bottom piece for concrete placement and consolidation.

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### 2.9.5 - METAL JAMBS

Metal jambs are typically used in commercial applications. Many metal jamb companies will pre-bend jambs to fit Logix forms. Contact your local Logix representative for more details.


## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.10 - ADDITIONAL FORM SUPPORT

The time spent prior to concrete placement pays huge dividends in job efficiency, accuracy, and profitability.


Provide wood strapping on both sides of Logix at window and door openings less than 4 feet from a corner. Run strapping across opening. Fasten to embedded furring tabs, and bracing around openings.


Provide wood strapping on both sides of Logix when vertical joints are directly on top of each other, or offset between joints is less than 8 " between courses.


Wood strapping is required around window and door openings to maintain straightness. In addition, cross bracing with $2 \times 4$ supports is required inside window and door bucks to hold bucks in place and prevent sagging. Use foam adhesive on bucks to provide additional buck support.


Foam adhesive should be used to secure all Height Adjusters.


The top course and lintels should be secured with adhesive foam, zip ties, or Logix Horizontal and Vertical Hooks.


The middle of large openings should be vertically braced to prevent tipping.


All outside corners can be reinforced with tape, or wood strapping, and zip ties.


Radius walls should be secured with foam adhesive and flexible strapping material.

NOTE: All forms should be firmly seated to prevent settling.

### 2.11 - WALL BRACING \& ALIGNMENT SYSTEM

A bracing system provides support for the wall and acts an alignment system to keep the walls straight and plumb during concrete placement. Typically, the wall alignment system is installed on the inner side of the Logix wall, and installed after placing 2 to 4 courses of Logix forms (depending on wind and other conditions).


Recommended minimum spacing and bracing locations:

- no more than 2 feet ( 0.610 m ) from each corner or wall end, and every 7 feet ( 2.134 m ) or less thereafter, in accordance with OSHA/OHSA requirements.
- on either side of every door and window opening.
- along door and window openings that span more than 6 feet ( 1.829 m )

NOTES: Prior to concrete placement, make certain walls are aligned perfectly plumb, or leaning slightly inward. The wall must not lean out at all.

A string line must be used to achieve straight walls. See Section "2.7.3 - ADDITIONAL COURSES" on page 16.

Before, during and after concrete placement, the diagonal turnbuckle arm is used to adjust wall straightness to stringline.

Proprietary bracing systems are available through ICF dealers or bracing suppliers.
For tall wall bracing and alignment see Section 3.2, Tall Wall Bracing Systems.

### 2.12 - FLOOR CONNECTIONS

Any type of floor system can be easily integrated with Logix. For any questions or assistance, please contact your local Logix representative.

### 2.12.1 - LEDGER WITH ANCHOR BOLTS \& JOIST HANGERS




STEP 1: Snap chalk lines and cut openings for bolt locations.


STEP 3: Place concrete.


STEP 2: Install ledger with anchor bolts.


STEP 4: Install joist hangers.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.12 - FLOOR CONNECTIONS Cont’d

### 2.12.2 - STEEL ANGLE IRON LEDGER

When floor spans become very long or concrete topping is applied to the floor, a wood ledger may not be adequate to support floor loads. In this case a steel angle iron can be used in place of a wood ledger. The angle iron can support much more weight and also eliminates the need for joist hangers, as the floor system sits right on the angle.

To install an angle iron ledger follow the steps in Section "2.12.1 - LEDGER WITH ANCHOR BOLTS \& JOIST HANGERS" on page 45 , but use pieces of plywood to temporarily hold the bolts in place. After the pour drill and bolt on the angle iron. Local steel fabricators may be able to pre-drill your angle iron.

Another alternative is to pre-fabricate an angle iron with anchor bolts or nelson studs welded directly to the angle. The entire assembly is then cast in place. This application is described below.


STEP 2: Install $2 \times 4$ to support angle assembly.


STEP 3: Install strapping to support angle assembly.


STEP 4: Pour concrete and cast the assembly in place.

NOTE: It is code in some areas for the angle assembly to be primed.


STEP 5: After some curing place floor systems on the angle and establish layout. Once layout is complete fasten the floor joist to the angle iron, as specified. You may decide to attach a nailing surface to the bottom leg of the angle iron to nail joists to.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.12 - FLOOR CONNECTIONS Cont'd

### 2.12.3 - BRICK LEDGE FOR TOP \& BOTTOM CHORD BEARING SYSTEMS

The Logix Brick Ledge form can create a load bearing surface to support floor systems, including top and bottom chord bearing trusses or joists.


Top chord bearing on Logix Brick Ledge.


STEP 1: Install a course of Logix Brick Ledge, and place required reinforcement.


STEP 3: As concrete is placed, install embedments, as required.


Top chord bearing on Logix Brick Ledge.


STEP 2: When installing a course above the Logix Brick Ledge add additional form support to prevent tilting or separating.

NOTE: If the Logix block in the course above the Brick Ledge is of a smaller width than the Brick Ledge, additional form support will be required.

### 2.12.4 - LEDGER WITH SIMPSON BRACKET \& JOIST HANGERS

The ICFVL \& ICFVL-W ledger connector system from Simpson Strong-Tie is designed for mounting steel or wood ledgers on ICF walls.


STEP 1: Snap a chalk line to mark the bottom of the ledger and insert ICFVL brackets, as specified.


STEP 2: Secure the ICFVL brackets before placing concrete. Fastening strapping across the brackets or installing the ledgers prior to concrete placement will help ensure full concrete embedment of the ICFVL brackets.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.12 - FLOOR CONNECTIONS Cont’d



STEP 3: Place and consolidate concrete. Once set, slip the ICFVL-W or ICFVL-CW underneath the wood ledger and drive eight ICF-D3.25 screws through the ledger and into the ICFVL bracket. ICF-D3.25 screws are supplied by Simpson Strong-Tie.

For steel ledgers use four \#14 x 3/4" screws to attach the ledger to the ICFVL brackets. These screws are not supplied by Simpson Strong-Tie.


STEP 4: Connect the floor joists to the ledgers, as required.

NOTE: Industry studies show that hardened fasteners can experience performance problems in wet environments. Accordingly, use this product in dry environments only. In addition, due to its corrosive nature, treated lumber should not be used with this product.

Use extra caution when installing the hangers on both sides of a wall. Consult your local Simpson Strongtie rep or contact Simpson Strongtie at (800) 999-5099 prior to installation.

Complete technical data is available at www. strongtie.com
Simpson Strong-Tie Ledger Connector Loads \& Spacings

|  |  | Simpson Strong-Tie Ledger Connector Loads \& Spacings |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} 4 " \\ \text { LOGIXICF } \end{gathered}$ | $\begin{aligned} & 6 ", 8^{\prime \prime} \& 10 " \\ & \text { LOGIXICF } \end{aligned}$ | $\begin{gathered} 4 " \\ \text { LOGIX ICF } \\ \hline \end{gathered}$ | $\begin{aligned} & 6^{\prime \prime}, 8 " \& 10 " \\ & \text { LOGIX ICF } \end{aligned}$ | Spacing to Replace Anchor Bolts ${ }^{\text {3,4,6 }}$ |  |  |  |  |  |  |  |
| dger Type | Model No. | Allowable Vertical Resistance ${ }^{2}$ | Allowable Vertical Resistance ${ }^{2}$ | Factored Vertical Resistance | Factored Vertical Resistance | 1/2" Dia. Bolts at |  |  |  | 5/8" Dia. Bolts at |  |  |  |
| dger Type |  | $\begin{aligned} & \text { lbs } \\ & \text { (kN) } \end{aligned}$ | $\begin{aligned} & \hline \text { lbs } \\ & \text { (kN) } \end{aligned}$ | $\begin{aligned} & \text { Ibs } \\ & \text { (kN) } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{lbs} \\ & \text { (kN) } \end{aligned}$ | $\begin{gathered} 12 " \\ (305 \mathrm{~mm}) \end{gathered}$ | 24" <br> (610mm) | $\begin{gathered} 36 " \\ (914 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} \hline 48 " \\ (1220 \mathrm{~mm}) \\ \hline \end{gathered}$ | $\begin{gathered} 12 " \\ (305 \mathrm{~mm}) \end{gathered}$ | 24" <br> ( 610 mm ) | $\begin{gathered} 36^{\prime \prime} \\ (914 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} \hline 48^{\prime \prime} \\ (1220 \mathrm{~mm}) \end{gathered}$ |
| 2xD.Fir-L/SPF | ICFVL <br> w/ ICFVL-W | $\begin{aligned} & 1375 \\ & (6.12) \end{aligned}$ | $\begin{gathered} 1894 \\ (8.42) \end{gathered}$ | $\begin{aligned} & 1890 \\ & (8.41) \end{aligned}$ | $\begin{gathered} \hline 2630 \\ (11.70) \end{gathered}$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $3^{\prime}-9^{\prime \prime}$ $(1143 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ |
| $13 / 4$ " LVL | ICFVL w/ ICFVL-CW | $\begin{aligned} & 1375 \\ & (6.12) \end{aligned}$ | $\begin{gathered} 1894 \\ (8.42) \end{gathered}$ | $\begin{aligned} & 1890 \\ & (8.41) \end{aligned}$ | $\begin{gathered} 2630 \\ (11.70) \end{gathered}$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $\begin{gathered} 3^{\prime}-6^{\prime \prime} \\ (1067 \mathrm{~mm}) \end{gathered}$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ |
| (0.054") 16ga | ICFVL | $\begin{gathered} 1770 \\ (7.87) \end{gathered}$ | $\begin{gathered} 1894 \\ (8.42) \end{gathered}$ | $\begin{gathered} 2435 \\ (10.83) \end{gathered}$ | $\begin{gathered} 2630 \\ (11.70) \end{gathered}$ | $\begin{gathered} 1^{1}-3^{\prime \prime} \\ (381 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 2^{\prime}-3^{\prime \prime} \\ (686 \mathrm{~mm}) \end{gathered}$ | -- | -- | $\begin{gathered} 1^{\prime} \\ (305 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} \text { '2 } \\ (610 \mathrm{~mm}) \end{gathered}$ | -- | -- |
| (0.068") 14ga | ICFVL | $\begin{gathered} 1770 \\ (7.87) \end{gathered}$ | $\begin{gathered} 1894 \\ (8.42) \end{gathered}$ | $\begin{gathered} 2435 \\ (10.83) \end{gathered}$ | $\begin{gathered} 2630 \\ (11.70) \end{gathered}$ | $1^{\prime}$ $(305 \mathrm{~mm})$ | $2^{\prime}$ $(610 \mathrm{~mm})$ |  | -- | $\begin{gathered} 9^{\prime \prime} \\ (229 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 1^{\prime}-6 " \\ (457 \mathrm{~mm}) \end{gathered}$ | -- | -- |


|  |  | $\begin{gathered} 4 " \\ \text { LOGIX ICF } \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 6^{\prime \prime}, 8^{\prime \prime} \& 10^{\prime \prime} \\ & \text { LOGIX ICF } \\ & \hline \end{aligned}$ | $\begin{gathered} 4^{\prime \prime} \\ \text { LOGIX ICF } \end{gathered}$ | $\begin{aligned} & \hline 6^{\prime \prime}, 8^{\prime \prime} \& 10^{\prime \prime} \\ & \text { LOGIX ICF } \end{aligned}$ | Spacing to Replace Anchor Bolts ${ }^{3,4,6}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ledger Type | Model No. | Allowable Vertical Resistance ${ }^{2}$ | Allowable Vertical Resistance ${ }^{2}$ | Factored Vertical Resistance | Factored Vertical Resistance | 2-5/8" Dia. Bolts at |  |  |  | 3/4" Dia. Bolts at |  |  |  |
|  |  | lbs (kN) | lbs <br> (kN) | lbs (kN) | lbs $(\mathrm{kN})$ | $\begin{gathered} 12 " \\ (305 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 24 " \\ (610 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 36 " \\ (914 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} \hline 48^{\prime \prime} \\ (1220 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 12 " \\ (305 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 24 " \\ (610 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 36^{\prime \prime} \\ (914 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 48^{\prime \prime} \\ (1220 \mathrm{~mm}) \end{gathered}$ |
| 2xD.Fir-L/SPF | ICFVL <br> w/ ICFVL-W | $\begin{aligned} & 1375 \\ & (6.12) \end{aligned}$ | $\begin{aligned} & 1894 \\ & (8.42) \end{aligned}$ | $\begin{aligned} & 1890 \\ & (8.41) \end{aligned}$ | $\begin{gathered} \hline 2630 \\ (11.70) \end{gathered}$ | 1' $^{\prime}-9^{\prime \prime}$ $(533 \mathrm{~mm})$ | $\begin{gathered} 3^{\prime}-99^{\prime \prime} \\ (1143 \mathrm{~mm}) \end{gathered}$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $3^{\prime}-6^{\prime \prime}$ $(1067 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ | $4^{\prime}$ $(1220 \mathrm{~mm})$ |
| $13 / 4$ " LVL | ICFVL <br> w/ ICFVL-CW | $\begin{aligned} & 1375 \\ & (6.12) \end{aligned}$ | $\begin{gathered} 1894 \\ (8.42) \end{gathered}$ | $\begin{aligned} & 1890 \\ & (8.41) \end{aligned}$ | $\begin{gathered} 2630 \\ (11.70) \end{gathered}$ | $\begin{gathered} 1^{\prime}-9^{\prime \prime} \\ (533 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 3^{\prime}-6^{\prime \prime} \\ (1067 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 4^{\prime} \\ (1220 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 4^{\prime} \\ (1220 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 2^{\prime}-9^{\prime \prime} \\ (838 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 4^{\prime} \\ (1220 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 4^{\prime} \\ (1220 \mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 4^{\prime} \\ (1220 \mathrm{~mm}) \end{gathered}$ |
| (0.054") 16ga | ICFVL | $\begin{gathered} 1770 \\ (7.87) \end{gathered}$ | $\begin{gathered} 1894 \\ (8.42) \end{gathered}$ | $\begin{gathered} 2435 \\ (10.83) \end{gathered}$ | $\begin{gathered} 2630 \\ (11.70) \end{gathered}$ |  | -- | -- | -- |  |  | -- | -- |
| (0.068") 14ga | ICFVL | $\begin{gathered} 1770 \\ (7.87) \end{gathered}$ | $\begin{gathered} 1894 \\ (8.42) \end{gathered}$ | $\begin{gathered} 2435 \\ (10.83) \end{gathered}$ | $\begin{gathered} 2630 \\ (11.70) \end{gathered}$ |  | -- | -- | -- |  | -- |  |  |

Allowable lateral load $=1905 \mathrm{Ibs}(8.47 \mathrm{kN})$ (Applicable to all form sizes).
$1 \mathrm{kN}=224.8 \mathrm{lbs}=102 \mathrm{Kg}$

1. Minimum steel ledger specification is $F y=33 \mathrm{ksi}(230 \mathrm{MPa})$ and $\mathrm{Fu}=45 \mathrm{ksi}(310 \mathrm{MPa})$ in accordance with CSA S136-94 2. No load duration increase is allowed.
2. Spacing is based on vertical load only. 5. Minimum concrete compressive strength, f'c, is $2500 \mathrm{psi}(17.25 \mathrm{MPa})$.
3. The designer may specify different spacing based on the load requirements.
4. For more information contact Simpson Strongtie at www.simpsonstrongtie.co
Note: Industry studies show that hardened fasteners can experience performance problems in wet environments. Accordingly, use this product in dry environments only.
In addition, due to its corrosive nature, treated lumber should not be used with Simpson Strongties.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.12 - FLOOR CONNECTIONS Cont'd

### 2.12.5 - TRANSITION LEDGE

A transition ledge typically occurs at the floor level where a wider Logix wall transitions to a narrower Logix wall above the floor line, and usually up to the roof line.


The ledge created when transitioning from a wider to a narrower wall can provide a suitable bearing length for many types of floor systems. The bearing length will vary depending on the thickness and type of Logix forms used. For a complete list of bearing lengths see Section 5.4.1, Bearing Lengths.

### 2.12.5.2 - TRANSITION LEDGE WITH CORNER BLOCKS

Transitioning from a wider block to a narrower block is commonly used in cases where a thinner wall becomes more economical (i.e., below grade wall to above grade wall), or to create a ledge that can support a floor or roof system, or finishes such as brick veneer.

When transitioning at corner locations using corner blocks, you might find that the interlocking knobs on the top side of the wider bottom block (bottom course) do not interlock or align with the underside of the top narrower block (top course). As a result, the top course will not sit or snap into its proper position.

This typically occurs in transitions at corner locations, and is easily resolved by following a few simple steps outlined below.


Proper alignment of top course to bottom course. Interlock aligns with underside of top course.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.12 - FLOOR CONNECTIONS Cont’d



STEP 1: Cut the interlocks off the wider corner blocks (it may be necessary to cut the interlocks off the rest of the blocks on the bottom course to ensure the top course can be placed flush on top of the previous course).
As an alternative, Taper Top blocks for the bottom course can be used. The Taper Tops provide more flexibility since they can be adjusted to ensure the interlocks align with the top course.


STEP 3: Install the top course beginning with the corner block and continuing around the building perimeter.

### 2.12.6 - TAPER TOP WITH SILL PLATE

The Taper Top form creates a greater bearing surface at the top of Logix walls.



STEP 1: Taper Top forms need to be foamed down or otherwise secured to the course below.


STEP 2: Trowel concrete flush with top of forms, or inset as required. Be sure to check for level.

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STEP 3: Insert embedments as required.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.12 - FLOOR CONNECTIONS Cont'd

### 2.12.7 - CONCRETE FLOOR SYSTEMS

Building with Logix will allow you to explore many concrete floor system options. Our walls are stronger and can support added weight that wood or steel frame buildings may not. Concrete floor systems are very popular in multi-residential buildings where the transmission of sound and fire are a concern. They are also growing in popularity in single-family residential applications.

### 2.12.7.1 - PRECAST CONCRETE FLOORS

Pre-cast floor systems are poured at the factory and shipped to site then craned in place. They are usually tensioned with steel cables cast in the concrete to provide maximum strength. Pre-cast floor are fast and can have very long clear spans.

Typically the Logix wall is constructed to the desired height and the pre-cast planks sit directly on the cured concrete. The planks, typically 4 feet ( 1.220 m ) wide, are craned in place and the groves between planks are


### 2.12.7.2 - COMPOSITE FLOOR SYSTEMS

Composite floors are a combination of steel and concrete that is bonded together to create a very strong floor allowing for longer spans and wider joist spacings.

There are a number of brands designed for ICFs including Hambro, iSpanEcospan and Total Joist. Consult your floor manufacturer and your local design engineer for more information.


### 2.13 - ROOF CONNECTIONS

Roof connections can be attached to the Logix wall in a variety of ways. Several factors can affect which method to use such as area of the country and wind conditions. There are a number of tie-down options made by Simpson Strong-Tie, including brands designed for ICFs, such as Burmon tie-down systems.


INSET SILL PLATE
This method of sill plate attachment is the most energy efficient. The Logix foam on each side provides an excellent thermal barrier.


TIE-DOWN TO CONCRETE
This method anchors the roof truss to the concrete.


TOP MOUNTED SILL PLATE
This method is typically used when additional wall height is required.


TIE-DOWN TO SILL PLATE
This method anchors the roof truss to the sill plate. (Burmon Anchor Tie-down)

### 2.14 - SERVICE PENETRATIONS

Identify and size all service and utility penetrations. Install all appropriate and properly sized sleeves where required, remembering that lightweight sleeves can be crushed during concrete placement.

List of possible service penetrations

- Dryer vent
- Water heater vent
- Water
- Sewer
- Electrical main service
- Gas line
- A/C line
- Furnace vent
- Air Exchange/HRV
- Central vacuum
- Ducting
- Bathroom vent
- Kitchen appliance venting
- Fireplace rough opening and vent
- Pet door


Cut appropriate sized holes for penetrations.


Install all required services through the ICF prior to concrete placement, and secure with spray foam.

### 2.15 - CONCRETE PLACEMENT

### 2.15.1 - PRE-PLACEMENT CHECKLIST

DATE:
FOREMAN:
JOB:
Prior to placing concrete in Logix insulated concrete forms, be certain to mark off each item on the checklist provided in this section.
__ 1. String line in place around the top of entire perimeter?
___ 2. Walls straight and plumb (not leaning out)?
__ 3. Top course foamed or tied down with zip ties or Logix Hooks end to end to maintain dimensions?
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$\Sigma$
$\qquad$ 11. All buck concrete anchors installed?
___ 12. All horizontal and vertical rebar in place?
13. All lintel reinforcing in place?
14. All penetrations installed?
15. All beam pockets in place?
16. All floor embedments installed?
_17. Are anchor bolts and hold-downs on site?
18. Has cavity of wall been checked, and foreign material removed?
19. Plywood, screw gun, and saw on site?
20. Interlock protected by tape, or other covering?
21. Proper concrete mix and slump ordered?
22. Concrete vibrator on site?
23. Pump equipped with reducer or 2 1/2" trimmer hose available?

### 2.15.2 - MIX DESIGN

Minimum compressive concrete strength is typically $3,000 \mathrm{psi}(20 \mathrm{MPa})$ at 28 days. However, this will depend on the structure and loading conditions. For seismic areas mix design should be confirmed with local codes or by an engineer.

The following maximum aggregate sizes are recommended for use in Logix walls:

|  | Form Cavity Size, in. (mm) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | $4(102)$ | $6.25(159)$ | $8(203)$ | $10(254)$ | $12 *(305)$ |
| Max. <br> Aggregate <br> Size, in. (mm) | $3 / 8(9.5)$ | $3 / 8(9.5)$ <br> to $1 / 2(13)$ | $3 / 4(19)$ | $3 / 4(19)$ | $3 / 4(19)$ |

Always consult your local ready mix companies for appropriate concrete mix design.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.15 - CONCRETE PLACEMENT Cont'd

### 2.15.3 - BEST PRACTICES

The most important stage of a successful Logix project is the concrete placement. Extra workers at this stage are important - be certain to have enough on hand during the pour to safely handle placement, consolidation, alignment, embedments, and cleanup.

An experience crew ensures the concrete is properly placed and consolidated. The following are recommended practices and considerations when placing concrete.

- Concrete slump should be 5 inch $(127 \mathrm{~mm})$ to 6 inches $(152 \mathrm{~mm})$ for best results.
- Use an internal vibrator with a head size of $3 / 4$ inch ( 19 mm ) to 1 inch $(25 \mathrm{~mm})$ and maximum 1 hp motor. Do not use a vibrator with a head larger than 1 inch ( 25 mm ).
- Appropriate internal vibration assures the strongest walls possible and is especially important for below grade application where the greatest loads occur.
- The rule of thumb for internal vibration is fast in and slow out, always moving, with a withdrawal rate of approximately 3 inch ( 76 mm ) per second.
Other methods of placement include conveyor truck, crane and bucket, and directly off the ready mix truck.
- Lift height is determined by many factors, such as air temperature, concrete temperature, slump, etc. In general, lift heights should not exceed $4 \mathrm{ft}(1.220 \mathrm{~m}$ ) per hour.
- When placing concrete below freezing or at temperatures above $100^{\circ} \mathrm{F}\left(38^{\circ} \mathrm{C}\right)$, it's important to protect all exposed concrete with insulation.
- When placing concrete in 4 inch ( 102 mm ) forms, it is recommended that the pump truck be fitted with a 2.5 inch ( 76 mm ) flexible hose end.


### 2.15.4 - PLACING CONCRETE

STEP 1: Complete the pre-placement checklist.


STEP 2: Begin concrete placement under openings, filling those areas and consolidating.


STEP 3: Beginning no closer than 3 feet ( 0.914 m ) from a corner, start filling the wall from the top, allowing the concrete to flow gently toward the corner. Then fill in that corner from the opposite side using the same technique.

STEP 4: Continue placing concrete around entire wall in appropriately sized lifts, using the same technique at each corner to minimize fluid pressure.

STEP 5: As the concrete is being placed, consolidation is taking place to remove air and voids to ensure structural integrity.


STEP 6: Check and adjust wall alignment using string lines and turnbuckles.


STEP 7: Return to starting location and begin the next lift. Follow all the techniques established above.

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## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.15 - CONCRETE PLACEMENT Cont'd

### 2.15.5 - POST-PLACEMENT CHECKLIST

DATE:
FOREMAN:
JOB:
After placing concrete in Logix insulated concrete forms, be certain to mark off each item on the checklist provided in this section.
$\qquad$ 1. Has consolidation been completed?
$\qquad$ 2. Are walls straightened to string line?
$\qquad$ 3. In extreme temperatures, has exposed concrete been protected?
$\qquad$ 4. Have all anchors and embeds been installed?
$\qquad$ 5. Has spilled concrete been disposed of?
$\qquad$ 6. Has final check for straight and plumb been done?

### 2.16 - ELECTRICAL INSTALLATIONS

Electrical and plumbing installation are typically performed after concrete placement.
The exception to this rule is the placement of conduit that penetrates the wall, which must be performed before concrete placement.

Installing electrical wiring and boxes is accomplished by creating channels in the EPS foam. When installed in Logix walls directly against the concrete, electrical boxes will extend $1 / 2$ inch ( 13 mm ) beyond the foam to match the thickness of $1 / 2$ inch ( 13 mm ) sheetrock.


Various tools can be used to create the channels and spaces for wiring and boxes:

- Electrical chainsaw with an adjustable roller depth stop
- Hot knife
- Circular saw with a masonry blade

Make the wiring channels narrow so there will be a friction fit with the wiring. The wiring needs to remain embedded well into the foam to meet local electrical codes. Foam adhesive can be spot-applied into the channel to help hold the wiring in place.

### 2.17 - PLUMBING INSTALLATIONS

In most cases, buildings are designed so plumbing pipes are not carried through the Logix walls, except for utility entry and exit points.

However, in some cases it may be required to embed pipe in the EPS. For example, a kitchen vent tube may need to be installed vertically in the EPS foam. Pipes embedded in the foam cannot exceed 1-1/2 inch ( 38 mm ) in diameter. Fittings embedded in the foam cannot exceed 2-1/2 inch ( 64 mm ) diameter.

An external faucet will require the installation of a hose sleeve through the wall prior to concrete placement. This will permit replacement of the faucet or pipe should it ever be necessary.

If connecting to existing sewer lines, establish the location of the required opening and ensure clearances, since this is difficult to change.


Pipes embedded within the Logix foam panels.

### 2.18 - INTERIOR \& EXTERIOR FINISHES

### 2.18.1 - VAPOR \& AIR BARRIERS

The Logix wall assembly has no need for an additional vapor barrier, the solid concrete core covered with the low permeance EPS foam insulation on the inside wall face keeps water vapor from penetrating the wall.

The fact that the inner face of EPS foam maintains a similar temperature as the inside air of the building and that a Logix wall has no cavity means that no condensation can occur in a Logix wall assembly.

The Logix wall assembly has no need for an air barrier (building wrap) layer as the solid concrete core and low permeance EPS foam insulation on the outside wall face keeps air and moisture from penetrating the wall.


Typical Logix wall assembly - no additional vapor barrier, house wrap and air barrier required.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.18 - INTERIOR \& EXTERIOR FINISHES cont'd

### 2.18.2 - INTERIOR DRYWALL

Drywall should be installed in the same manner on a Logix wall as on a stud wall, with the following time-saving exceptions:

- All furring tabs (studs) are on 8 inch ( 203 mm ) centers from floor to ceiling for easy attachment of any type of interior wall finish.
- The butt joints of the sheetrock do not need to fall on webs (studs) as the foam provides solid backing wherever the joints fall. However, the edge of sheetrock panels should not exceed more than 4" from webs.
- A foam-compatible adhesive can be used to effectively fasten the sheetrock to the Logix wall along with screws. Always make sure to verify the local code for types and spacing for sheetrock fasteners. Typically, adhesive alone is not allowed as a fastener of sheetrock, but again check with local building codes.

Many local building codes require the application of $1 / 2$ inch $(13 \mathrm{~mm})$ drywall or other suitable thermal barrier in any living space even though the EPS foam has a fire retardant component. Always verify local building code requirements.

Non-habitable spaces such as crawl spaces, attics, and other types of hidden areas typically do not require a thermal barrier (drywall).

Embedded furring tabs are fixed at each corner of the Logix $90^{\circ}$ corner forms for solid sheetrock fastening at all corners.


### 2.18.3 - EXTERIOR SIDING

Siding material of some kind must be installed over the EPS foam to protect it from the UV rays of the sun. Foam left exposed to the sun will slowly develop a dusty surface.

NOTE: When using Logix Platinum Series care should be taken to protect exposed foam surfaces from reflected sunlight and prolonged solar exposure until wall cladding or finish material is applied. Shade exposed foam areas, or remove sources of reflective surfaces, where heat build up onto exposed foam might occur. For more information refer to BASF Technical Leaflet N-4 Neopor, "Recommendations for packaging, transporting, storing and installing building insulation products made from Neopor EPS foam." (The BASF Technical Leaflet is attached to every bundle of Logix Platinum forms delivered to a job site).

Metal and vinyl siding can be installed directly over the top of the EPS.
Although air guns can be used, Logix recommends the use of screw guns when attaching exterior siding. Always follow manufacturer's recommendations and local codes to determine the size and spacing of fasteners for all siding products.

Any type of siding that is used on a typical wood-framed building can be used on a Logix building.
The siding channel stock around doors and windows can be fastened to whatever type of buck material was chosen, in a similar fashion as wood framed building.


## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.18 - INTERIOR \& EXTERIOR FINISHES cont'd

### 2.18.4 - STEEL PANEL SIDING

Steel panel siding can be applied vertically to a Logix wall when the style of the panel matches the Logix web spacing at 8 inch ( 203 mm ) on center increments for fastening purposes.


When a panel siding is chosen that doesn't fit with 8 inch ( 203 mm ) increment for fastening, two different methods are available:


Typical Logix wall assembly - Metal Panel Siding with strapping
METHOD 1: A $1 / 2$ inch $(13 \mathrm{~mm})$ or $3 / 4$ inch ( 19 mm ) strip of wood can be attached horizontally to the webs in the wall to provide the manufacturer's specified fastener spacing.


Typical Logix wall assembly - Metal Panel Siding placed horizontally. METHOD 2: The panels can be installed horizontally, by fastening directly into the webs.

NOTE: Although air guns can be used, Logix recommends the use of screw guns when attaching exterior siding. Always follow manufacturer's recommendations and local codes to determine the size and spacing of fasteners for all siding products.

### 2.18.5 - WOOD SIDING

Any wood siding can be attached to the Logix wall in the same manner as to a traditional framed building. The spacing of the web studs on 8 inch ( 203 mm ) centers allows for industry standard spacing of fasteners. Typically, screws are used for attaching wood siding or even half-log siding to the Logix wall.

Although air guns can be used, Logix recommends a screw gun with screws in clips (Quik Drive). This is usually the fastest method for applying wood siding. Always follow manufacturer's recommendations and local codes to determine the size and spacing of fasteners for all siding products.

A good practice for installing wood siding on a wall, is to apply the siding over vertical 1 inch $\mathbf{x} 2$ inch ( $25 \mathrm{~mm} \times 51$ mm ) wood nailing strips with a screen at the bottom. The screen keeps insects out while the space allows air to circulate behind the siding. The air circulation helps equalize the moisture content in the wood siding, which makes for much more dimensionally stable siding and longer lasting application.


## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.18 - INTERIOR \& EXTERIOR FINISHES cont'd

### 2.18.6 - EIFS

There are now acrylic-based stucco products available that are more flexible and easier to work with than traditional cement-based stucco. Collectively these products are known as EIFS (Exterior Insulation Finish Systems) and almost always require an EPS substrate.

Because Logix blocks are made with EPS, they are a natural fit for EIFS finishes. In addition, the webs in Logix blocks are embedded $1 / 2$ inch ( 13 mm ) deep in the EPS foam to comply with EIFS manufacturer requirements.

It is important to follow the EIFS manufacturer's application procedures.


Typical Logix wall assembly - EIFS example. Consult EIFS manufacturer for recommended application procedures..

### 2.18.8 - CEMENT COMPOSITE SIDING

Recently the new cement fiber siding products have gained popularity. This type of siding can usually be fastened directly to the Logix webs.

Although air guns can be used, Logix recommends a screw gun to fasten flat-headed exterior screws at 16 inch (406 mm ) centers. The screws pull the siding in tight and hold the siding securely in place.

Some manufacturers may require the siding to be strapped out to allow air space behind. Vertical or shake patterns will require strapping for fastening. See illustrations in Section 2.18 .4 and 2.18 .5 for strapping examples.

Always follow manufacturer's recommendations and local codes to determine the size and spacing of fasteners for all siding products.

Check with your siding manufacturer for specific requirements.

Furring tabs are embedded 1/2" from surface of Logix foam panels and are anchored into the concrete.

Furring tabs are spaced 8 " on center horizontally — and run nearly the entire height of Logix ICF blocks.


Typical Logix wall assembly - Cement fibre siding installed horizontally.

### 2.18 - INTERIOR \& EXTERIOR FINISHES cont'd

### 2.18.9 - BRICK VENEER

The Logix Brick Ledge form units are used to support a brick veneer as the exterior finish material. The Brick Ledge forms are simply placed at a level where the brick is desired to begin. The design of the form creates a reinforced concrete ledge.

With standard reinforcing, the Brick Ledge can bear up to $1300 \mathrm{lb} / \mathrm{ft}(19 \mathrm{kN} / \mathrm{m})$ of wall.
$\varnothing$

With site-specific engineering, up to $3000 \mathrm{lb} / \mathrm{ft}(44 \mathrm{kN} / \mathrm{m})$ of wall is attainable.
To install Brick Ledge form units, follow the instructions in section "2.7.4 - CORNER BRICK LEDGE" on page 18 of the guide. When reinforcing steel and concrete are in place within the wall, brick is laid on the ledge and tied back to the webs with brick ties as specified.


### 2.18.10 - BELOW GRADE WATERPROOFING, DAMPPROOFING \& PARGING

There are many methods available to protect the "below grade" and the "just above grade" areas of the exterior of your building.

Dampproofing is used on concrete or masonry surfaces to repel water in above grade walls. The 2.75 inch ( 70 mm ) foam panels of the Logix insulated concrete forms act as dampproofing, therefore, no additional dampproofing treatment is required.

NOTE: Although dampproofing above grade walls is not typically required, check with local building codes for dampproofing requirements.


### 2.18.10.1 - BELOW GRADE WATERPROOFING

Logix recommends a rubberized "peel and stick" waterproofing membrane. The membrane is applied vertically to the wall from grade level down to and overlapping the top of the footing. It is recommended to use protection board, such as $1 / 2$ inch rigid foam boards, or drainage boards, to prevent damage to the waterproofing membrane during backfilling.

Proper free-draining backfill material is recommended for below-grade walls.
NOTE: Membrane should be installed within one week prior to backfill being placed. Sunlight and high temperatures may cause the membrane to begin to "sag" which may cause wrinkles in the material. This may result in tears or punctures during the placement of the backfill material. Should you choose to use one of the many other types of waterproofing available be sure to follow the manufacturer's recommended installation procedures.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.18 - INTERIOR \& EXTERIOR FINISHES cont'd

### 2.18.10.1 - BELOW GRADE WATERPROOFING

STEP 1: Prep the wall and footing area to be covered by removing all dirt and debris. If the ICF foam panels have been subjected to prolonged UV exposure a chalky layer of dust will develop on its surface. Be sure to remove the dust layer by sweeping the surface with a broom.

STEP 2: Snap chalk lines for the "grade" line.
STEP 3: Measure the height from grade line to footing. Add enough length to cover the top of the footing and cut pieces of membrane to length.


STEP 4: Apply the membrane at corners first. Hang the membrane vertically, and starting at the top pull back the first $8^{\prime \prime}$ to $10^{\prime \prime}$ of the release paper and press. Continue pulling back the release paper and pressing the membrane to the wall. Make sure to wrap the corners with the membrane.


STEP 5: Starting at a corner continue applying cut pieces of membrane around the wall, maintaining 2 inch overlap by using the printed marks on the membrane as a guide.

NOTE: Extreme temperatures, both cold and hot, may cause the installer to consider other types of waterproofing. Be sure to follow the manufacturer's installation process.

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### 2.18.10.2 - ABOVE GRADE PARGING

The area that is above grade line and below the exterior siding material must be parged to protect the EPS from damage.

Parging is a coating material that is applied to give a finished appearance to the small area of wall that is above grade level but below where the siding materials will begin. Logix Prepcoat is the preferred option for this area.

STEP 1: Prep the wall area to be covered by removing any dirt or debris. The wall may need to be "scuffed" to reveal fresh EPS beads.

STEP 2: Mix Prepcoat dry material with water to a pasty consistency.
STEP 3: Using a trowel apply a thin, $1 / 16$ " $-1 / 8$ " ( $2 \mathrm{~mm}-3 \mathrm{~mm}$ ) "skim coat" of Prepcoat.
STEP 4: Pre-cut pieces of Logix fiber mesh $1^{\prime \prime}-2^{\prime \prime}(25 \mathrm{~mm}-51 \mathrm{~mm})$ wider than the area to be parged. This will allow for an over-lap over the waterproofing membrane to create a "drip ledge".

STEP 5: Embed the mesh in the skim coat firmly.
STEP 6: Once the area is dry to the touch apply a second coat of Prepcoat. This coat can be painted or stained if desired.


### 2.19 - ATTACHING FIXTURES

For attaching fixtures Logix provides furring tabs spaced every 8 inches, which provides more fastening points than stud walls.


Different methods are used to attach fixtures depending on whether the fixture is light or heavy in weight.

### 2.19.1 - LIGHT WEIGHT FIXTURES

Fixtures that are light in weight, such as small picture frames or mirrors, can be attached to the wall without having to fasten into the furring tabs by using typical hanging pins, finishing nails or plugs.

Fixtures such as curtain rods, large picture frames or mirrors, bathroom accessories, etc., require a more secure attachment to the wall.

The Grappler, a product made specifically for ICFs, provides a stronger attachment for fixtures that are light in weight but require a more secure hold. The Grappler is also useful in areas where a stronger fastening point is required in an area where furring tabs may be absent. The Grappler is a $4^{\prime \prime} \times 8^{\prime \prime}$ steel meshed plate that is pressed into the surface of the Logix form panels before drywall is placed. Once the drywall is installed the Grappler is sandwiched between the ICF and drywall creating a much stronger and secure attachment area.

### 2.19.2 - HEAVY WEIGHT FIXTURES

Additional backing is recommended to support heavier wall fixtures, such as kitchen cabinetry, wall mounted fixtures, grab bars, hand rails, etc.

Different attachment methods can be employed depending on the type of attachment.

### 2.19.2.1 - CABINETS



METHOD 1: Plywood board can be attached to the Logix wall behind the heavier cabinets in place of gypsum board, providing a thermal barrier comparable to gypsum and a strong attachment surface for heavier items and fixtures. Be certain to attach the plywood board to the Logix webs with a sufficient number of screws to hold heavy items in place for when loads are applied.


METHOD 2: Create horizontal channels behind the cabinets equal in width to a $2 \times 4$ and install $2 \times 4$ backing directly to the concrete surface using sufficiently long concrete screws and a rotohammer. Attach the cabinets to the $2 \times 4 \mathrm{~s}$.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.19 - ATTACHING FIXTURES Cont’d

### 2.19.2.2 - GRAB BARS

METHOD 1: Before placing drywall, place the Grapplers (see Section "2.19.1 - LIGHT WEIGHT FIXTURES" on page 78) onto Logix at grab bar fastening points. Install the drywall and fasten the grab bar to the Grapplers.


METHOD 2: Use Tapcon screws to anchor the grab bar directly to the concreted.


METHOD 3: For a stronger hold remove the foam and replace with wood blocking behind the grab bar mounting bracket. The wood blocking should be mechanically fastened to the concrete.

### 2.19.2.3 - TELEVISIONS

Furring tabs at $\mathbf{8 "}^{\prime \prime}$ on center.


METHOD 1: Face mounted TVs up to 200lbs can be secured to the furring tabs with a minimum of 4 course thread screws. Care must be taken to ensure the screws are properly fastened to the furring tabs. Fastening to Grapplers in combination with furring tabs will also work.

Before installing mounting bracket conceal plywood with drywall compound to blend with drywall (drywall compound not shown for clarity).
METHOD 2: Replace the drywall behind the mounting bracket with plywood.

Fasten the plywood with sufficient number of screws to the furring tabs. will ve foam and replace with $1 / 2^{\prime \prime}$ thick strapping anchored to concrete with Tapcons.


METHOD 3: TV mounts that swivel causes heavier loading conditions and should be anchored to the concrete with plywood and tapcons.

Placing strapping directly against furring tabs ensures $1 / 2^{\prime \prime}$ thick foam is removed and provides good solid backing.

### 2.20 - HOLDING POWER OF SCREWS FASTENED TO LOGIX FURRING TABS

Web fastener withdrawal and shear testing using course and fine thread drywall screws. Tests were conducted on furring tabs embedded $1 / 2$ inch ( 52 mm ) from the surface of the 2.75 inch ( 70 mm ) Logix EPS panels.

|  | Max. Average <br>  <br> Withdrawal <br> Resistance | Allowable <br> Withdrawal <br> Resistance | Max. Average <br> Shear Resistance | Allowable Shear <br> Resistance $^{2}$ |
| :--- | :---: | :---: | :---: | :---: |
| Coarse Thread Drywall <br> Screw | $166 \mathrm{lb}(75.3 \mathrm{~kg})$ | $33 \mathrm{lb}(15.0 \mathrm{~kg})$ | $367 \mathrm{lb}(166.5 \mathrm{~kg})$ | $49 \mathrm{lb}(22.2 \mathrm{~kg})$ |
| Fine Thread Drywall <br> Screw | $1691 \mathrm{bb}(76.7 \mathrm{~kg})$ | $34 \mathrm{lb}(15.4 \mathrm{~kg})$ | $328 \mathrm{lb}(148.8 \mathrm{~kg})$ | $49 \mathrm{lb}(22.2 \mathrm{~kg})$ |

$1 \mathrm{~kg}=9.81$ Newtons

1. Allowable withdrawal resistance values are based on a factor of safety of 5 .
2. Allowable shear resistance values are based on a factor of safety of 3.2 within defined deflection limits (for more detailed information contact info@Logixicf.com)

NOTE: The numbers in this table represent resistance at failure. Good building practice mandates a minimum of a 5 to 1 safety factor in calculating fastener loading. For complete test results on additional fasteners, see Section 8 in the Logix Design Manual or consult your local Logix representative.


| Outside Radius, <br> ft. (m) | Form Cavity Width |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4" (102mm) |  | 6.25" (159mm) |  | 8" (203mm) |  | 10" (254mm) |  |
|  | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) |
| 3 (0.914) | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline \hline 13 / 16 \\ & (21) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 13 / 32 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 1 \text { 19/64 } \\ (33) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 135 / 64 \\ (39) \\ \hline \end{gathered}$ |
| 3.5 (1.067) | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 11 / 16 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 59 / 64 \\ (23) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (28) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 1 \text { 19/64 } \\ (33) \\ \hline \end{gathered}$ |
| 4 (1.219) | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 32 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 51 / 64 \\ (20) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 61 / 64 \\ (24) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{array}{r} 11 / 8 \\ (29) \\ \hline \end{array}$ |
| 4.5 (1.372) | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 32 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 45 / 64 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 32 \\ (21) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 1 \\ (25) \\ \hline \end{gathered}$ |
| 5 (1.524) | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5 / 8 \\ (16) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 / 4 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 57 / 64 \\ (23) \\ \hline \end{gathered}$ |
| 5.5 (1.676) | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | 27/64 <br> (11) | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{aligned} & 9 / 16 \\ & (14) \\ & \hline \end{aligned}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 43 / 64 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 51 / 64 \\ (20) \\ \hline \end{gathered}$ |
| 6 (1.829) | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 33 / 64 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5 / 8 \\ (16) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 47 / 64 \\ (19) \\ \hline \end{gathered}$ |
| 6.5 (1.981) | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{aligned} & 9 / 16 \\ & (14) \\ & \hline \end{aligned}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 43 / 64 \\ (17) \\ \hline \end{gathered}$ |
| 7 (2.134) | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{aligned} & 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 32 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5 / 8 \\ (16) \\ \hline \end{gathered}$ |

## NOTES:

1. Field cut Logix Standard forms (straight forms) into widths, C, according to Logix Radius Walls table. For inside radius field cut additional foam, A, accordingly.
2. Secure each radius section with zip ties, Logix Hooks, tape or foam.
3. The field cuts, C, are kept at $8^{\prime \prime}$ (203mm), 16" (406mm), 24" ( 610 mm ) or $48^{\prime \prime}$ ( 1220 mm ) lengths. The field cuts, $A$, are determined depending on required radius. The combined field cuts, A and C, results in an outside radius which is within $1 \%$ of the design radius for radii less than $60 \mathrm{ft}(18.3 \mathrm{~m})$, and $1 \%$ to $2 \%$ for radii between 60 ft and 100 ft ( 18.3 m to 30.5 m ).

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.21 - RADIUS WALLS Cont'd

| Outside Radius, ft. (m) | Form Cavity Width |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4" (102mm) |  | 6.25 " (159mm) |  | 8" (203mm) |  | 10" (254mm) |  |
|  | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) |
| 7.5 (2.286) | $\begin{gathered} \hline \hline 8 \\ (203) \\ \hline \end{gathered}$ | $5 / 16$ <br> (8) | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 31 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 37 / 64 \\ (15) \\ \hline \end{gathered}$ |
| 8 (2.438) | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 35 / 64 \\ (14) \\ \hline \end{gathered}$ |
| 8.5 (2.591) | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 33 / 64 \\ (13) \\ \hline \end{gathered}$ |
| 9 (2.743) | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 31 / 64 \\ (12) \end{gathered}$ |
| 9.5 (2.896) | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 41 / 64 \\ (16) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ |
| 10 (3.048) | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 39 / 64 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ \text { (9) } \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{aligned} & 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ |
| 10.5 (3.200) | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 37 / 64 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ |
| 11 (3.353) | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 35 / 64 \\ (14) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ |
| 11.5 (3.505) | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 32 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | 5/16 <br> (8) | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 / 8 \\ (10) \\ \hline \end{gathered}$ |
| 12 (3.658) | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 2 \\ & (13) \\ & \hline \end{aligned}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ |
| 12.5 (3.810) | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 31 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 37 / 64 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ |
| 13 (3.962) | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 64 \\ (8) \\ \hline \end{gathered}$ |
| 13.5 (4.115) | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 32 \\ (13) \end{gathered}$ | $\begin{gathered} \hline 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ |
| 14 (4.267) | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{aligned} & 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 39 / 64 \\ (15) \\ \hline \end{gathered}$ |
| 14.5 (4.420) | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 32 \\ (15) \\ \hline \end{gathered}$ |
| 15 (4.572) | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 37 / 64 \\ (15) \\ \hline \end{gathered}$ |
| 15.5 (4.724) | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 35 / 64 \\ (14) \\ \hline \end{gathered}$ |
| 16 (4.877) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 / 8 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 17 / 32 \\ & (13) \\ & \hline \end{aligned}$ |
| 16.5 (5.029) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 8 \\ (203) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 33 / 64 \\ (13) \\ \hline \end{gathered}$ |
| 17 (5.182) | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 1 / 2 \\ (13) \\ \hline \end{gathered}$ |
| 17.5 (5.334) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 33 / 64 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 31 / 64 \\ (12) \\ \hline \end{gathered}$ |
| 18 (5.486) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 1 / 2 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 15 / 32 \\ & (12) \\ & \hline \end{aligned}$ |
| 18.5 (5.639) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 31 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ |
| 19 (5.791) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 / 8 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ |


| Outside Radius, ft. (m) | Form Cavity Width |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4" (102mm) |  | 6.25 " (159mm) |  | 8" (203mm) |  | 10" (254mm) |  |
|  | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) |
| 19.5 (5.944) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 15 / 32 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \end{gathered}$ | $\begin{gathered} \hline 3 / 8 \\ (10) \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \end{gathered}$ | $\begin{aligned} & \hline 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ |
| 20 (6.096) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ |
| 20.5 (6.248) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $21 / 64$ <br> (8) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{aligned} & 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ |
| 21 (6.401) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{aligned} & 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ |
| 21.5 (6.553) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ |
| 22 (6.706) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $5 / 16$ <br> (8) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $21 / 64$ <br> (8) | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ |
| 22.5 (6.858) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 3 / 8 \\ & (10) \\ & \hline \end{aligned}$ |
| 23 (7.010) | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \\ \hline \end{gathered}$ |
| 23.5 (7.163) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ |
| 24 (7.315) | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{array}{r} 3 / 8 \\ (10) \\ \hline \end{array}$ | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ |
| 24.5 (7.468) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 47 / 64 \\ (19) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ |
| 25 (7.620) | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 32 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ |
| 25.5 (7.772) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 45 / 64 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 64 \\ (8) \\ \hline \end{gathered}$ |
| 26 (7.925) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 33 / 64 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 45 / 64 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 64 \\ (8) \\ \hline \end{gathered}$ |
| 26.5 (8.077) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 33 / 64 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 11 / 16 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $5 / 16$ <br> (8) |
| 27 (8.230) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 2 \\ & (13) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 43/64 <br> (17) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $5 / 16$ <br> (8) |
| 27.5 (8.382) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 2 \\ & (13) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 32 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ |
| 28 (8.534) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 31 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 41 / 64 \\ (16) \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 16 \\ (406) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \end{gathered}$ |
| 28.5 (8.687) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 41 / 64 \\ (16) \\ \hline \end{gathered}$ | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \end{gathered}$ | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ |
| 29 (8.839) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (16) \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{aligned} & 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ |
| 29.5 (8.992) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 39/64 <br> (15) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $23 / 64$ <br> (9) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ |
| 30 (9.144) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 39 / 64 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ |
| 30.5 (9.296) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 32 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 45 / 64 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ |
| 31 (9.449) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 37/64 <br> (15) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 45 / 64 \\ (18) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ |

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.21 - RADIUS WALLS Cont'd

| Outside Radius, <br> ft. (m) | Form Cavity Width |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4" (102mm) |  | $6.25{ }^{\prime \prime}$ ( 159 mm ) |  | 8" (203mm) |  | 10" (254mm) |  |
|  | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) |
| 31.5 (9.601) | $\begin{gathered} \hline \hline 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 27 / 64 \\ (11) \end{gathered}$ | $\begin{gathered} \hline 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 37 / 64 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 11 / 16 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 13 / 32 \\ (10) \\ \hline \end{gathered}$ |
| 32 (9.754) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 27/64 <br> (11) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 9 / 16 \\ & (14) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 43/64 <br> (17) | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ |
| 32.5 (9.906) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 9 / 16 \\ & (14) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 32 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ |
| 33 (10.058) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 35 / 64 \\ (14) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 32 \\ (17) \\ \hline \end{gathered}$ | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ |
| 33.5 (10.211) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 17 / 32 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 41 / 64 \\ (16) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{aligned} & 3 / 8 \\ & (10) \end{aligned}$ |
| 34 (10.363) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 17 / 32 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 41 / 64 \\ (16) \\ \hline \end{gathered}$ | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \\ \hline \end{gathered}$ |
| 34.5 (10.516) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 33 / 64 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{array}{r} 5 / 8 \\ (16) \\ \hline \end{array}$ | $\begin{gathered} 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \\ \hline \end{gathered}$ |
| 35 (10.668) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 33 / 64 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 39 / 64 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ |
| 35.5 (10.820) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{aligned} & 1 / 2 \\ & (13) \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 39 / 64 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ |
| 36 (10.973) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 2 \\ & (13) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 32 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ |
| 36.5 (11.125) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 3 / 8 \\ & (10) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 2 \\ & (13) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 19 / 32 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ |
| 37 (11.278) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 31 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 37 / 64 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ |
| 37.5 (11.430) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 31 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 37 / 64 \\ (15) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ |
| 38 (11.582) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 15 / 32 \\ & (12) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 9 / 16 \\ & (14) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 64 \\ (8) \\ \hline \end{gathered}$ |
| 38.5 (11.735) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 9 / 16 \\ & (14) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ |
| 39 (11.887) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 35 / 64 \\ (14) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 64 \\ (8) \\ \hline \end{gathered}$ |
| 39.5 (12.040) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 35 / 64 \\ (14) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 64 \\ (8) \\ \hline \end{gathered}$ |
| 40 (12.192) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 32 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 24 \\ (610) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ |
| 40.5 (12.344) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 32 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (16) \\ \hline \end{gathered}$ |
| 41 (12.497) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 32 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (16) \\ \hline \end{gathered}$ |
| 41.5 (12.649) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 33 / 64 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 39 / 64 \\ (15) \\ \hline \end{gathered}$ |
| 42 (12.802) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 33 / 64 \\ (13) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 39 / 64 \\ (15) \\ \hline \end{gathered}$ |
| 42.5 (12.954) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 2 \\ & (13) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 32 \\ (15) \\ \hline \end{gathered}$ |
| 43 (13.106) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $5 / 16$ <br> (8) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 2 \\ & (13) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 32 \\ (15) \\ \hline \end{gathered}$ |


| Outside Radius, ft. (m) | Form Cavity Width |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4" (102mm) |  | 6.25" (159mm) |  | 8" (203mm) |  | 10" (254mm) |  |
|  | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) |
| 43.5 (13.259) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 1 / 2 \\ (13) \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 19 / 32 \\ (15) \end{gathered}$ |
| 44 (13.411) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 31 / 64 \\ (12) \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 37 / 64 \\ (15) \\ \hline \end{gathered}$ |
| 44.5 (13.564) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 19/64 <br> (8) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 31 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 37 / 64 \\ (15) \\ \hline \end{gathered}$ |
| 45 (13.716) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 31 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{aligned} & 9 / 16 \\ & (14) \\ & \hline \end{aligned}$ |
| 45.5 (13.868) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $19 / 64$ <br> (8) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 9 / 16 \\ & (14) \\ & \hline \end{aligned}$ |
| 46 (14.021) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 19/64 <br> (8) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 15/32 <br> (12) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 35/64 <br> (14) |
| 46.5 (14.173) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | 35/64 <br> (14) |
| 47 (14.326) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{array}{r} 13 / 8 \\ (10) \\ \hline \end{array}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 35 / 64 \\ (14) \\ \hline \end{gathered}$ |
| 47.5 (14.478) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 3 / 8 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 29 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 17 / 32 \\ (13) \end{gathered}$ |
| 48 (14.630) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{array}{r} \hline 3 / 8 \\ (10) \\ \hline \end{array}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 29 / 64 \\ (12) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 32 \\ (13) \\ \hline \end{gathered}$ |
| 48.5 (14.783) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 8 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 7 / 16 \\ & \hline(11) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 32 \\ (13) \end{gathered}$ |
| 49 (14.935) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 33 / 64 \\ (13) \\ \hline \end{gathered}$ |
| 49.5 (15.088) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 17/64 <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $23 / 64$ <br> (9) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 33 / 64 \\ (13) \\ \hline \end{gathered}$ |
| 50 (15.240) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 27 / 64 \\ (11) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 33 / 64 \\ (13) \\ \hline \end{gathered}$ |
| 50.5 (15.392) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $17 / 64$ <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $23 / 64$ <br> (9) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 27/64 <br> (11) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 1 / 2 \\ (13) \\ \hline \end{gathered}$ |
| 51 (15.545) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 17/64 <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $11 / 32$ <br> (9) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 27/64 <br> (11) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{array}{r} 1 / 2 \\ (13) \\ \hline \end{array}$ |
| 51.5 (15.697) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $17 / 64$ <br> (7) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 27 / 64 \\ (11) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 1 / 2 \\ (13) \end{gathered}$ |
| 52 (15.850) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 31 / 64 \\ (12) \\ \hline \end{gathered}$ |
| 52.5 (16.002) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 31 / 64 \\ (12) \\ \hline \end{gathered}$ |
| 53 (16.154) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 31 / 64 \\ (12) \\ \hline \end{gathered}$ |
| 53.5 (16.307) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $21 / 64$ <br> (8) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ |
| 54 (16.459) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ |
| 54.5 (16.612) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ |
| 55 (16.764) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 25 / 64 \\ (10) \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 32 \\ (12) \\ \hline \end{gathered}$ |

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.21 - RADIUS WALLS Cont'd

| Outside Radius, ft. (m) | Form Cavity Width |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4" (102mm) |  | 6.25 " (159mm) |  | 8" (203mm) |  | 10" (254mm) |  |
|  | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) |
| 55.5 (16.916) | $\begin{gathered} \hline 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline \hline 25 / 64 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline \hline 29 / 64 \\ (12) \\ \hline \end{gathered}$ |
| 56 (17.069) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ |
| 56.5 (17.221) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $5 / 16$ <br> (8) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ |
| 57 (17.374) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $15 / 64$ <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $5 / 16$ <br> (8) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 29 / 64 \\ (12) \\ \hline \end{gathered}$ |
| 57.5 (17.526) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 3 / 8 \\ & (10) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ |
| 58 (17.678) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (10) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ |
| 58.5 (17.831) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{array}{r} \hline 7 / 16 \\ (11) \\ \hline \end{array}$ |
| 59 (17.983) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 7 / 16 \\ & (11) \\ & \hline \end{aligned}$ |
| 59.5 (18.136) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ \text { (9) } \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ |
| 60 (18.288) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ |
| 60.5 (18.440) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 23 / 64 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ |
| 61 (18.593) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 19 / 64 \\ \text { (8) } \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ \text { (9) } \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 27 / 64 \\ (11) \\ \hline \end{gathered}$ |
| 61.5 (18.745) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ |
| 62 (18.898) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 13 / 32 \\ & (10) \\ & \hline \end{aligned}$ |
| 62.5 (19.050) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ |
| 63 (19.202) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ |
| 63.5 (19.355) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 64 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 32 \\ (10) \\ \hline \end{gathered}$ |
| 64 (19.507) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 13/64 <br> (5) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $21 / 64$ <br> (8) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ |
| 64.5 (19.660) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 13 / 64 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ |
| 65 (19.812) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 64 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ |
| 65.5 (19.964) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $13 / 64$ <br> (5) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $17 / 64$ <br> (7) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $21 / 64$ <br> (8) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ |
| 66 (20.117) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 64 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 25 / 64 \\ (10) \\ \hline \end{gathered}$ |
| 66.5 (20.269) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 64 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $17 / 64$ <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{aligned} & 3 / 8 \\ & (10) \end{aligned}$ |
| 67 (20.422) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 64 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{array}{r} 3 / 8 \\ (10) \\ \hline \end{array}$ |


| Outside Radius, ft. (m) | Form Cavity Width |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4" (102mm) |  | 6.25" (159mm) |  | 8" (203mm) |  | 10" (254mm) |  |
|  | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) |
| 67.5 (20.574) | $\begin{gathered} \hline 48 \\ (1,219) \\ \hline \end{gathered}$ | 13/64 <br> (5) | $\begin{gathered} \hline 48 \\ (1,219) \\ \hline \end{gathered}$ | 17/64 <br> (7) | $\begin{gathered} \hline 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 3 / 8 \\ (10) \\ \hline \end{gathered}$ |
| 68 (20.726) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 64 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{array}{r} \hline 3 / 8 \\ (10) \\ \hline \end{array}$ |
| 68.5 (20.879) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | 17/64 <br> (7) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 3 / 8 \\ (10) \\ \hline \end{gathered}$ |
| 69 (21.031) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $17 / 64$ <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 23/64 <br> (9) |
| 69.5 (21.184) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $23 / 64$ <br> (9) |
| 70 (21.336) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 19/64 <br> (8) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $23 / 64$ <br> (9) |
| 70.5 (21.488) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $23 / 64$ <br> (9) |
| 71 (21.641) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $23 / 64$ <br> (9) |
| 71.5 (21.793) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{aligned} & \hline 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $23 / 64$ <br> (9) |
| 72 (21.946) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $19 / 64$ <br> (8) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ |
| 72.5 (22.098) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $3 / 16$ <br> (5) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 19/64 <br> (8) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $11 / 32$ <br> (9) |
| 73 (22.250) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ |
| 73.5 (22.403) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $15 / 64$ <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $19 / 64$ <br> (8) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $11 / 32$ <br> (9) |
| 74 (22.555) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 11/64 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 15/64 <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $11 / 32$ <br> (9) |
| 74.5 (22.708) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 11/64 <br> (4) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $15 / 64$ <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $9 / 32$ <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 32 \\ (9) \\ \hline \end{gathered}$ |
| 75 (22.860) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 11/64 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 15/64 <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $11 / 32$ <br> (9) |
| 75.5 (23.012) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 11/64 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 15/64 <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 9/32 <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 21/64 <br> (8) |
| 76 (23.165) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ |
| 76.5 (23.317) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 11/64 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 15/64 <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $21 / 64$ <br> (8) |
| 77 (23.470) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | 11/64 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $15 / 64$ <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ |
| 77.5 (23.622) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 11/64 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $15 / 64$ <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 9/32 <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $21 / 64$ <br> (8) |
| 78 (23.774) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 11/64 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 15/64 <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 17/64 <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 21/64 <br> (8) |
| 78.5 (23.927) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $17 / 64$ <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 21 / 64 \\ (8) \\ \hline \end{gathered}$ |
| 79 (24.079) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 11/64 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $17 / 64$ <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ |

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.21 - RADIUS WALLS Cont'd

| Outside Radius, ft. (m) | Form Cavity Width |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4" (102mm) |  | 6.25" (159mm) |  | 8" (203mm) |  | 10" (254mm) |  |
|  | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) |
| 79.5 (24.232) | $\begin{gathered} \hline 48 \\ (1,219) \\ \hline \end{gathered}$ | 11/64 <br> (4) | $\begin{gathered} \hline 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 48 \\ (1,219) \\ \hline \end{gathered}$ | 17/64 <br> (7) | $\begin{gathered} \hline 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ |
| 80 (24.384) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 11/64 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $17 / 64$ <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ |
| 80.5 (24.536) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 11 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 17/64 <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ |
| 81 (24.689) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 32 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 16 \\ (8) \\ \hline \end{gathered}$ |
| 81.5 (24.841) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 5/32 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $17 / 64$ <br> (7) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ |
| 82 (24.994) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 5/32 <br> (4) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | 17/64 <br> (7) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ |
| 82.5 (25.146) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 5/32 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5 / 16 \\ (8) \\ \hline \end{gathered}$ |
| 83 (25.298) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 5/32 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \\ \hline \end{gathered}$ |
| 83.5 (25.451) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $5 / 32$ <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 19/64 <br> (8) |
| 84 (25.603) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 5/32 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $19 / 64$ <br> (8) |
| 84.5 (25.756) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | 5/32 <br> (4) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $13 / 64$ <br> (5) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | 19/64 <br> (8) |
| 85 (25.908) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 32 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 13/64 <br> (5) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $19 / 64$ <br> (8) |
| 85.5 (26.060) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $5 / 32$ <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 13/64 <br> (5) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 19/64 <br> (8) |
| 86 (26.213) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 5/32 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 64 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 19 / 64 \\ (8) \end{gathered}$ |
| 86.5 (26.365) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $5 / 32$ <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $13 / 64$ <br> (5) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 19/64 <br> (8) |
| 87 (26.518) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | 5/32 <br> (4) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | 13/64 <br> (5) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | 19/64 (8) |
| 87.5 (26.670) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 5/32 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 13/64 <br> (5) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ |
| 88 (26.822) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 5/32 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 13/64 <br> (5) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 15/64 <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $9 / 32$ <br> (7) |
| 88.5 (26.975) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 32 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 13 / 64 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ |
| 89 (27.127) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 9/64 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 13/64 <br> (5) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 15/64 <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ |
| 89.5 (27.280) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $9 / 64$ <br> (4) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | 13/64 <br> (5) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $15 / 64$ <br> (6) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ |
| 90 (27.432) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 13/64 <br> (5) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $15 / 64$ <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ |
| 90.5 (27.584) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 9/64 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $13 / 64$ <br> (5) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 15/64 <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 1 / 32 \\ (7) \\ \hline \end{gathered}$ |
| 91 (27.737) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ |


| Outside Radius, ft. (m) | Form Cavity Width |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4" (102mm) |  | $6.25{ }^{\prime \prime}$ ( 159 mm ) |  | 8" (203mm) |  | 10" (254mm) |  |
|  | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) | C, in. (mm) | A, in. (mm) |
| 91.5 (27.889) | $\begin{gathered} \hline 48 \\ (1,219) \end{gathered}$ | 9/64 <br> (4) | $\begin{gathered} \hline 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} \hline 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline 48 \\ (1,219) \end{gathered}$ | $\overline{15 / 64}$ <br> (6) | $\begin{gathered} \hline \hline 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 9 / 32 \\ (7) \\ \hline \end{gathered}$ |
| 92 (28.042) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 32 \\ (7) \\ \hline \end{gathered}$ |
| 92.5 (28.194) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $9 / 64$ <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $15 / 64$ <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $17 / 64$ <br> (7) |
| 93 (28.346) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 15 / 64 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ |
| 93.5 (28.499) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $9 / 64$ <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $3 / 16$ <br> (5) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $15 / 64$ <br> (6) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $17 / 64$ <br> (7) |
| 94 (28.651) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ |
| 94.5 (28.804) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $9 / 64$ <br> (4) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ |
| 95 (28.956) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ |
| 95.5 (29.108) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | 9/64 <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ |
| 96 (29.261) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ |
| 96.5 (29.413) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 9 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ |
| 97 (29.566) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 9 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ |
| 97.5 (29.718) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $9 / 64$ <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 17 / 64 \\ (7) \\ \hline \end{gathered}$ |
| 98 (29.870) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $9 / 64$ (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 16 \\ (5) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ |
| 98.5 (30.023) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $9 / 64$ (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ |
| 99 (30.175) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 8 \\ & (3) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 11 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ |
| 99.5 (30.328) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 8 \\ & (3) \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $11 / 64$ <br> (4) | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ |
| 100 (30.480) | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{aligned} & 1 / 8 \\ & \text { (3) } \\ & \hline \end{aligned}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 11 / 64 \\ (4) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \end{gathered}$ | $\begin{gathered} 7 / 32 \\ (6) \\ \hline \end{gathered}$ | $\begin{gathered} 48 \\ (1,219) \\ \hline \end{gathered}$ | $\begin{aligned} & 1 / 4 \\ & (6) \\ & \hline \end{aligned}$ |

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

### 2.22 - TALL WALLS

Logix walls can be constructed to any height provided proper engineering and construction methods are used.


Logix tall walls should be designed in accordance with ACI 318 or CAN/CSA A23.3.
Constructing tall walls follows the same basic steps described throughout Section 2. In addition, building taller walls is done in much the same way as concrete pours using traditional formwork. Generally, Logix blocks are stacked and braced, normally 10 to 12 feet high. The concrete is then placed. After the concrete sets Logix blocks are then stacked another 10 to 12 feet, and bracing is raised or extended higher to support the wall, as well as keeping the 3 wall plumb. This process is continued until the specified wall height is reached.


To ensure a smooth build, the following items should be considered:

- Load tables in Section 6 can be used as a design aid for both the builder and designer. However, tall wall designs should be reviewed and approved by a local licensed professional engineer.
- In higher wind areas taller walls may require guy wires for additional support. Typically, this will be determined by the engineer of record.
- Proper consolidation of concrete can be achieved by adequate vibrating. However, depending on the drop height, and the steel congestion, external vibration, in addition to internal vibration, should be considered, particularly at corners, openings, and congested areas of rebar. (External vibrators made specifically for ICFs are available. See Section "2.23SUPPORTING PRODUCTS" on page 94.
- Since tall walls are typically poured using a pump truck, using a 2 1/2" trimmer hose can provide better control of the concrete pour.
- If required, roughen the surface of all cold joints to ensure a good bond between the surface of the old pour and the subsequent pour. In addition, ensure adequate rebar embedments are provided.
- For the final stage of the pour, a Logix Taper Top block can be used, if required, for the top course of the wall. This provides a larger opening for concrete to flow into the wall and also provides a larger bearing area for supporting elements.
- Several tall wall bracing and alignment systems are available. For more information see Section 3.2, Tall Wall Bracing Systems.

NOTE: Both ACI 318 and CAN/CSA A23.3 permit cold joints when concrete is poured in stages.

### 2.23 - SUPPORTING PRODUCTS

A list of supporting ICF products are shown below. Consult with the listed manufacturer prior to using with Logix Insulated Concrete Forms. Please note: the products listed below does not prohibit the use of Logix ICFs with other supporting products not listed.

FOOTINGS

| Product Name | Manufacturer | Contact | Website |
| :--- | :--- | :--- | :--- |
| Form-A-Drain | CertainTeed Corp. | $708-301-4449$ | certainteed.com |

EXTERIOR FINISHES

| Product Name | Manufacturer | Contact | Website |
| :--- | :--- | :--- | :--- |
| Durock | Alfacing International Ltd. | $1-888-238-6345$ | durock.com |
| Senerflex | Degussa Wall Systems, Inc. | $1-800-221-9255$ | senergy.cc |
| Sto EIFS System | Sto Corp. | $1-800-221-2397$ | stocorp.com |
| GrailCoat | GrailCoat | $1-877-472-4528$ | grailcoat.com |
| TAFS (Textured Acrylic Finishes | dryvit | $1-800-263-3308$ | dryvit.com |
| SoftCoat PB System | Total Wall, Inc. | $1-888-702-9915$ | totalwall.com |
| Akroflex | Omega Products Corp. | $602-721-5027$ | omega-products.com |
| Impact System | parex | $1-800-537-2739$ | parex.com |
| PermaCrete | Quality Systems | $1-800-607-3762$ | permacrete.com |
| Crack Guard | Poly-Wall | $1-800-846-3020$ | poly-wall.com |
| WeatherWall Systems | Eco Specialty Products Ltd. | $1-888-481-5507$ | ecocoatings.ca |

## WATERPROOFING

| Product Name | Manufacturer | Contact | Website |
| :--- | :--- | :--- | :--- |
| System III | Epro | $1-800-882-1896$ | eproserv.com |
| Blueskin WP2000 | Bakor, Inc | $1-800-387-9598$ | bakor.com |
| Colphene 3000 | Soprema, Inc | $1-800567-1492$ | soprema.com |
| Delta-MS Clear | Cosella-Dorken Products, Inc. | $1-888-4 D E L T A 4$ | cosella-dorken.com |
| Platon | Armtec Ltd. | $1-800-265-7622$ | systemplaton.com |
| Tamko TW60 | Tamko, Inc. | $1-800-641-4691$ | tamko.com |
| Grace waterproofing products | Grace Construction Products | See website | graceconstruction.com |
| Aqua-Wrap/Green Sheild | Aqua Seal Inc. | $1-888-282-3861$ | aquasealusa.com |
| Protecto Universal Primer Free Membrane | Protecto Wrap | $1-800-759-9727$ | protecowrap.com |

CONNECTION SYSTEMS

| Product Name | Manufacturer | Contact | Website |
| :--- | :--- | :--- | :--- |
| ICF Ledger Connector System | Simpson Strong-Tie Co., Inc. | $1-800-999-5099$ | simpsonstrongtie.com |
| ICF-Connect | ICF-Connect Ltd. | $1-866-497-1576$ | icfconnect.com |

ADHESIVE \& SEALANTS

| Product Name | Manufacturer | Contact | Website |
| :--- | :--- | :--- | :--- |
| Enerfoam Sealant/Enerbond Adhesive | Dow Chemical Company | $1-800-800-$ FOAM | dow.com/buildingproducts |
| PL300 | Loctite | $1-800-624-7767$ | www.loctiteproducts.com |

WALL BRACING \& ALIGNMENT SYSTEMS

| Product Name | Manufacturer | Contact | Website |
| :--- | :--- | :--- | :--- |
| Uniscaffold, LLC | Uniscaffold | $1-208-791-5624$ | www.uniscaffold.com |
| Giraffe Bracing | Giraffe Bracing | $1-888-778-2285$ | www.giraffebracing.com |
| Plumwall | Plumwall Ltd. | $1-905-786-7586$ | www.plumwall.com |
| Mono-Brace | Tapco | $814-336-6549$ | www.mono-brace.com |
| Amazing Brace | Lakeland Group | $905-372-7413$ | www.lakeland-multitrade.com |

EXTERNAL VIBRATORS

| Product Name | Manufacturer | Contact | Website |
| :--- | :--- | :--- | :--- |
| Brecon | Brecon Inc. | $815-463-8073$ | http://icfvibrator.com |
| Arkie Wall Banger | Available from Wind-lock | $1-800-872-5625$ | - |

SUPPLIERS OF SUPPORTING ICF PRODUCTS

| Company | Contact | Website |
| :--- | :--- | :--- |
| Wind-lock | $1-800-872-5625$ | wind-lock.com |
| Grace Construction Products | See website | graceconstruction.com |

Build Anything Better. ${ }^{\text {m }}$
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3.2 - LOCATION \& SPACING ..... 3-4
3.3 - INSTALLATION ..... 3-5
3.4 - TALL WALL BRACING ..... 3-7
3.4.1 - TALL WALL BRACING SYSTEMS USING SCAFFOLDING ..... 3-8

## 3.1 - INTRODUCTION

A bracing system provides temporary support for the wall and acts as an alignment system to keep the walls straight and plumb during concrete placement. Typically, the wall alignment system is installed on the inner side of the Logix wall.

There are a number of proprietary systems available. However, each bracing unit typically consists of a vertical upright steel channel with slots for attaching screws to the Logix webs, a turnbuckle arm, and a scaffold bracket. Normally, wall bracing systems are installed after placing 2 to 4 courses of Logix forms (depending on wind and other conditions).


## 3.2 - LOCATION \& SPACING

- Place bracing no more than $2 \mathrm{ft}(610 \mathrm{~mm}$ ) from each corner or wall end, and every 7 ft ( 2134 mm ) or less thereafter, in accordance with OSHA/OHSA requirements.
- Every door and window opening should be flanked on either side by bracing units.


The middle of large openings should be vertically braced to prevent tipping.

## 3.3 - INSTALLATION



## Front View



Perspective Cut Section

STEP 1: Attach the upright steel channel to the Logix webs with a \#10 screw in each course. The screws should be snug but not tight.


STEP 2: Attach a turnbuckle arm to the upright with a bolt and then secure to the floor or ground. In light or sandy soils, additional care must be taken to secure diagonal turnbuckle. Ensure wall is close to plumb and threads on the turnbuckle is secured.


STEP 3: The scaffold bracket is then inserted behind the top of the turnbuckle and secured at the bottom with an additional bolt.


STEP 4: Place the appropriate scaffolding planks and rails according to safety regulations. For requirements on toe board and handrail configuration, consult OSHA/OHSA.

STEP 5: Prior to concrete placement, make certain walls are leaning slightly inward. The wall must not lean out at all.


STEP 6: A stringline must be used to achieve straight walls.
STEP 7: Before, during and after concrete placement, the diagonal turnbuckle arm is used to adjust wall straightness to stringline.

## 3.4 - TALL WALL BRACING

Tall walls are constructed in much the same way as concrete pours using traditional formwork. In general, the Logix blocks are stacked and braced, normally 10 to 12 feet high. The concrete is then placed. After the concrete sets the Logix blocks are then stacked another 10 to 12 feet, and bracing is raised or extended higher to support the wall, as well as keeping the wall plumb. This process is continued until the specified wall height is reached.


In higher wind areas taller walls may require guy wires for additional support.
Logix can be built to any height using either proprietary bracing systems or traditional scaffolding.
There are a number of proprietary tall wall bracing and alignment systems available. Many of the systems are designed to accommodate walls heights from 30 to 50 feet. For a list of some of these systems see " 2.23 SUPPORTING PRODUCTS" on page 94.

With minor modifications traditional scaffold (masonry scaffold) systems can also be used as the bracing and alignment system for tall walls. In addition, more experienced builders may have their own custom bracing systems designed to meet their preferred method of construction.

NOTE: When using wall bracing systems always follow the manufacturer's recommended installation practices, including all required federal and local safety guidelines. Users of Logix and bracing systems should always follow OSHA/OHSA guidelines.

LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 3.4 - TALL WALL BRACING cont'd

### 3.4.1 - TALL WALL BRACING SYSTEMS USING SCAFFOLDING

The following installation instructions demonstrates the use of scaffolding as a tall wall bracing and alignment system. The scaffolding system described is available from Form Systems, Inc. For more information contact your local Logix representative.


STEP 1: Complete two courses making sure they are straight, level and well anchored (Figure A).


STEP 3: Insert the screw jacks into the base frames as seen in Figure C. Create a base frame by attaching two $7 \mathrm{ft}(2.134 \mathrm{~m}$ ) ledgers (the horizontal pipes) to two base frames. Each ledger end has a wedge to anchor the system together (Figure D). To remove, hit from below. Once base frame is in place, level in all directions.


STEP 2: The first scaffolding items needed are the base frames and screw jacks. The left end of the base frame as seen in Figures B and C is the end that will sit against the forms to allow the screw jacks to be adjusted.


STEP 4: There are two kinds of vertical poles. Poles with the $2 / 3$ rosettes go against the wall. Those with the full rosettes go into the center cup of the base frame (Figure C).


STEP 5: Install the two-foot ledgers that will hold the decks in place on every third rosette from the bottom. Note that the only $7 \mathrm{ft}(2.134 \mathrm{~m})$ ledger required against the wall is on the base frame. The rest of the scaffolding will require 7 ft ( 2.134 m ) ledgers only on one side (Figure F).


STEP 6: Place one wire clip per course at each vertical 2/3 rosette pole (Figure E).


STEP 7: Insert 7ft ( 2.134 m ) ledgers for railings in the two rosettes above the planks (Figure G).
STEP 8: There are two adjustable diagonals. One is $4 \mathrm{ft}(1.220 \mathrm{~m})$ long and is intended to go to the inside of the vertical poles. It's designed to align the wall during the second or third build. For the first build, use the 10ft ( 3.048 m ) external adjustable diagonal (Figure G).
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## 4.1 - INTRODUCTION

Calculating the number of forms needed is a simple task with Logix.
An important thing to remember in estimating is that walls with different heights should be calculated separately. As the wall heights change, so do the quantities required.

There are several tools available to aid in estimating:

- Drawing a wall section on graph paper before estimating a project saves time and effort.
- The Logix One Minute Estimator provides rough estimates for preliminary estimates, and is available as an app or online.
- The Logix Estimator provides more accurate and very detailed estimates and is on Windows. However, the Logix Estimate can work on a Mac provided Windows Parallel is installed. This program is available for download.

The Logix Estimator and One Minute Estimator are available through the "Download Apps" link on any of the Logixicf.com web pages.

The Logix Estimator (Desktop App)


When you build with Logix ICF, the Logix Estimator will quickly create detailed and accurate take offs, cut lists and more, and will generate professional and accurate customer quotes with the margins you need.
« Download the Logix Estimator


## 4.2 - MATERIAL TAKE-OFF LIST

The material take off is the first step in any estimate.
__ Linear feet of exterior and interior Logix walls
_ Height of walls
__ Number of courses in wall
___ Thickness of wall (4", $6.25^{\prime \prime}, 8^{\prime \prime}, 10^{\prime \prime}$ or $12^{\prime \prime}$ )
__ Number of 90 o corners (both inside and outside)
_ Number of 450 corner (both inside and outside)
_ Linear feet of Brick Ledge
__ Linear feet of Taper Top
__ Linear feet of Double Taper Top
__ Square feet of parge coating "stucco" (height x length) between grade and siding
__ Square feet of water proofing (height x length) from grade to lap over footing
__ Square feet of door and window openings
__ Linear feet of buck material
__ Number of beam pockets (End Caps)
__ Linear feet of end walls (End Caps)
__ Linear feet of Height Adjusters (both sides of wall)

## SQUARE FOOTAGE OF DIFFERENT FORM TYPES

| Standard (straight): | 5.33 sf |
| :--- | :--- |
| Standard V12 (straight) | 4.00 sf |
| Brick Ledge: | 5.33 sf |
| Taper Top: | 5.33 sf |
| Double Taper Top: | 5.33 sf |
| $90^{\circ}$ Corner (outside face): | 5.36 sf (5.89sf for 10" and 12" corner forms) |
| $90^{\circ}$ Corner V12 (outside face): | 4.02 sf |
| $45^{\circ}$ Corner (outside face): | 3.89 sf |
| $4 "$ Height Adjuster: | 0.67 sf |
| Pilaster: | 3.49 sf max. |

Build Anything Better."

## 4.3 - ESTIMATING FORMS

Standard, $45^{\circ}$ and $90^{\circ}$ Corner forms are $16^{\prime \prime}$ in height. Standard V12 and Corner V12 forms are $12^{\prime \prime}$ in height. The following steps are based on 16" heights, however, the same procedure outlined in Section 4.3 .1 is followed for 12" high forms. (Currently, $45^{\circ}$ forms in V12 are not available and are formed on-site.)

### 4.3.1 - STANDARD FORMS \& CORNERS

STEP 1: Determine the total lineal feet of walls (both interior and exterior walls that will be built using Logix). Add an extra 2 ft for every $45^{\circ}$ or $90^{\circ}$ inside corner to the total lineal feet of walls. With this new lineal footage, multiply by the height of the walls to determine the property's total square footage. When figuring the total square footage of walls with different heights it's easiest to figure each wall separately and then add totals together.

Subtract the total square footage of all window and door openings.
STEP 2: Determine number of $45^{\circ}$ forms (A) by multiplying number of $45^{\circ}$ turns by the number of courses (i.e. 6 courses $x 4$ turns). Then multiply the number of $45^{\circ}$ forms by $3.89 \mathrm{sf} /$ form. Then subtract this from your gross square footage of wall determined in Step 1.

If no $45^{\circ}$ turns continue with Step 3.
STEP 3: Determine number of $90^{\circ}$ corner forms (B) by multiplying number of $90^{\circ}$ turns by the number of courses (i.e. 6 courses $x 4$ turns). Then multiply the number of $90^{\circ}$ forms by $5.36 \mathrm{sf} /$ form (or 5.89 sf for $10^{\prime \prime}$ or $12^{\prime \prime}$ corner forms). Then subtract this from your square footage of wall determined in Step 2 (if no $45^{\circ}$ turns used, then subtract from gross square footage determined in Step 1).

STEP 4: Divide square footage of wall determined in Step 3 by 5.33 to determine gross number of Standard forms required. (C)

NOTE: Standard forms are all $16^{\prime \prime}(406 \mathrm{~mm})$ tall and $48^{\prime \prime}(1220 \mathrm{~mm})$ long with a wall area of 5.33 sf each. All $90^{\circ}$ Corners are $16^{\prime \prime}$ tall. The $4^{\prime \prime}, 6.25^{\prime \prime}$ and $8^{\prime \prime}$ Ninety degree corner forms cover a wall area of 5.36 sf (measured at the longer side of the corner form). The $10^{\prime \prime}$ and $12^{\prime \prime}$ Ninety degree corner forms cover a wall area of 5.89sf.
A. Number of $45^{\circ}$ forms required:
B. Number of $90^{\circ}$ forms required:
C. Number of Standard forms required:
D. Total number of forms required:
$\qquad$
$\qquad$
$\qquad$

### 4.3.2 - BRICK LEDGE FORMS

NOTE: Brick Ledge forms are available in straight units only. Corner applications require miter cutting Brick Ledge forms on site.

Brick Ledge forms only come in $6.25^{\prime \prime}, 8^{\prime \prime}, 10^{\prime \prime}$ and $12^{\prime \prime}$ cavity sizes.
STEP 1: Measure the total linear feet of Brick Ledge needed and divide by 4 (the length in feet of each block) to determine the total number of Brick Ledge forms needed. When miter cutting Brick Ledge corners, add one Brick Ledge form for waste at each corner to the total Brick Ledge count.

STEP 2: Subtract the number of Brick Ledge forms from the total number of Standard forms determined earlier to avoid ordering too many Standard forms.

### 4.3.3 - DOUBLE TAPER TOP \& TAPER TOP FORMS

NOTE: The above forms are available in straight units only. Corner applications require miter cutting the forms on site.

Taper Top and Double Taper Top forms come in 6.25 ", 8 ", $10^{\prime \prime}$ or $12^{\prime \prime}$ cavity sizes.
Follow Steps 1 and 2 in Section 4.3.2 to estimate the number of Taper Top or Double Taper Top forms required.

### 4.3.4 - HEIGHT ADJUSTERS

A 2 ft Height Adjuster $=0.66 \mathrm{sf}$. The number of 2 ft long Height Adjusters needed is equal to the total linear footage .
NOTES: Height Adjusters come in one size, $4^{\prime \prime} \times 24^{\prime \prime} \times 2.75^{\prime \prime}$ thick. Remember to count both sides of the wall. Height Adjusters can be used in window openings to adjust height without cutting standards.

### 4.3.5 - END CAPS

NOTES: End Caps are $16^{\prime \prime}$ tall and 2-1/4" thick. End Caps come in all wall cavity sizes $-4 ", 6.25^{\prime \prime}, 8^{\prime \prime}, 10^{\prime \prime}$ and $12^{\prime \prime}$. Use End Caps at end wall applications. Use two End Caps for each beam pocket. Use End Caps for step foundations if necessary. End Caps can be used to form side bucks on door and window openings.

## 4.4 - CONCRETE

### 4.4.1-4" WALLS

STEP 1: Take the square footage of all wall area and subtract the square footage of all window and door openings.
STEP 2: Multiply by 0.333 ft (the width of the cavity) to get the cubic feet of concrete required.
STEP 3: Divide by 27cf to determine the total number of yards of concrete required (or divide by 35.32 to determine meters of concrete required).

Example: 1845sf of wall area minus 322 sf of window and door area equals 1523 sf of net wall area. 1523 sf times 0.333 ft equals 507 cf divided by 27 cf per yard equals 18.8 yards of concrete required. Or divide 507 cf by 35.32 for meters required. In this case, 14.4 meters.

### 4.4.2-6.25" WALLS

STEP 1: Take the square footage of all wall area and subtract the square footage of all window and door openings.
STEP 2: Multiply by 0.521 ft (the width of the cavity) to get the cubic feet of concrete required.
STEP 3: Divide by 27cf to determine the yards of concrete required (or divide by 35.32 to determine meters required).

Example: 1845sf of wall area minus 322 sf of window and door are equals 1523 sf of net wall area. 1523sf times 0.521 ft equals 793 cf divided by 27 cf per yard equals 29.4 yards of concrete. Or divide 793 cf by 35.32 for meters required. In this case, 22.5.

### 4.4.3-8" WALLS

STEP 1: Take the square footage of all wall area and subtract the square footage of all window and door openings.
STEP 2: Multiply by 0.667 ft (the width of the cavity) to get the cubic feet of concrete required.
STEP 3: Divide by 27 to determine the yards of concrete required (or by 35.32 to determine meters required).
Example: 1845 sf of wall area minus 322 sf of window and door area equals 1523 sf of net wall area. 1523 sf times 0.667 ft equals 1016 cf divided by 27 cf per yard equals 37.6 yards of concrete. Or divide 1016 cf by 35.32 for meters required. In this case, 28.8.

### 4.4.4-10" WALLS

STEP 1: Take the square footage of all wall area and subtract the square footage of all window and door openings.
STEP 2: Multiply by 0.833 ft (the width of the cavity) to get the cubic feet of concrete required.
STEP 3: Divide by 27cf to determine the total number of yards of concrete required (or by 35.32 to determine meters of concrete required).

Example: 1845sf of wall area minus 322 sf of window and door area equals 1523 sf of net wall area. 1523 sf times 0.833 ft equals 1269 cf divided by 27 cf per yard equals 47.0 yards of concrete required. Or divide 1269 cf by 35.32 for meters required. In this case, 35.9 meters.

### 4.4.5-12" WALLS

STEP 1: Take the square footage of all wall area and subtract the square footage of all window and door openings.
STEP 2: Multiply by 1 ft (the width of the cavity) to get the cubic feet of concrete required.

### 4.4.6 - ADD EXTRA CONCRETE FOR TAPER TOPS

Multiply linear feet of Taper Top by 0.003 cubic yards or cubic meters 0.002 to determine the additional yards or meter of concrete needed.

Example: 200If of Taper Top forms would require an additional 0.6 yards of extra concrete (200If $\times 0.003=0.6$ yards).

### 4.4.7 - ADD EXTRA CONCRETE FOR DOUBLE TAPER TOPS

Multiply linear feet of Double Taper Tops by 0.006 cubic yards or cubic meters 0.005 to determine the additional yards or meter of concrete needed.

Example: 200If of Taper Top forms would require an additional 1.2 yards of extra concrete ( $2001 \mathrm{f} \times 0.006=1.2$ yards).

### 4.4.8 - ALTERNATE METHOD FOR CALCULATING CONCRETE

An alternate method to calculate concrete is to use the chart below. Simply multiply the total number of forms by the appropriate multiplier to determine the cubic yards or cubic meters of concrete required.

| ) | Form Size | Cubic Yards per Form Unit | Cubic Meters per Form Unit |
| :---: | :---: | :---: | :---: |
| z | 4" | 0.066 | 0.050 |
| $\vdash$ | 6.25" | 0.103 | 0.079 |
|  | 8" | 0.132 | 0.100 |
| - | 10" | 0.165 | 0.126 |
| $\stackrel{\vdash}{\sim}$ | 12" | 0.198 | 0.151 |

## 4.5 - REBAR

Rebar estimating varies from wall to wall depending on factors such as height, vertical loading, horizontal loading, backfill heights, etc.

NOTE: Each Brick Ledge will require six stirrups to tie the horizontal rebar in the corbel to the horizontal rebar in the interior of the form.

## 4.6 - WATERPROOFING

Multiply linear footage of walls by the height of backfill. When calculating backfill height, make sure to add enough height to allow the waterproofing materials to extend over the edge of the footing.

Divide this number by the square footage per roll of membrane material to determine the total number of rolls required.

If using a rigid waterproofing board, do not include a footing overlap in you calculations.

## 4.7 - PARGING

Parging typically covers from the top of the waterproofing membrane to a height 2" above the bottom edge of the siding.

Multiply the linear footage of wall by height of parging to determine total square footage of parging required.
Divide this number by the square footage per bag of parging material to determine the total number of bags required.

## LOGIX® ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## 4.8 - COURSE HEIGHT TABLE

This table shows wall heights that are readily achieved using Standard Logix forms used in combination with 4" (102mm) Height Adjusters and/or 12" (305mm) V12 forms.

|  |  | HEIGHT OF WALL WHEN ADDITIONAL COURSES OF HEIGHT ADJUSTER OR V12s ARE ADDED |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Number of Standard Courses | Height of Wall for Standard Courses | 4" Height Adjuster | 1 Course of V12 | 2 Courses of V12 | 3 Courses of V12 |
| 1 | 1' - 4" (406mm) | 1' - 8" (508mm) | 2' - 4" (711mm) | 3' - 4" (1016mm) | 4' - 4" (1321mm) |
| 2 | 2' - 8" (813mm) | 3' - 0' (914mm) | 3' - 8" (1118mm) | 4' - 8" (1422mm) | 5' - 8" (1727mm) |
| 3 | $4^{\prime}$ - 0 " ( 1219 mm ) | 4' - 4" (1321mm) | 5' - 0" (1524mm) | $6^{\prime}$ - 0 " ( 1829 mm ) | 7' - 0" (2134mm) |
| 4 | 5' - 4' (1626mm) | 5' - 8" (1727mm) | 6' - 4' (1930mm) | 7' - 4" (2235mm) | 8' - 4" (2540mm) |
| 5 | 6' - 8" (2032mm) | 7' - 0" (2134mm) | 7' - 8" (2337mm) | 8' - 8" (2642mm) | 9' - 8" (2946mm) |
| 6 | 8' - 0" (2438mm) | 8' - 4" (2540mm) | 9' - 0" (2743mm) | 10' - 0" (3048mm) | 11' - 0" (3353mm) |
| 7 | 9'-4" (2845mm) | 9' - 8" (2946mm) | 10'-4" (3150mm) | 11'-4" (3454mm) | 12' - 4" (3759mm) |
| 8 | 10' - 8" ( 3251 mm ) | 11' - 0" (3353mm) | 11' - 8" (3556mm) | 12' - 8" (3861mm) | 13' - 8" (4166mm) |
| 9 | 12' - 0" (3658mm) | 12'-4" (3759mm) | 13' - 0" (3962mm) | 14' - 0" (4267mm) | 15' - 0" (4572mm) |
| 10 | 13'-4" (4064mm) | 13' - 8" (4166mm) | 14' - 4" (4369mm) | 15' - 4" (4674mm) | 16' - 4" (4978mm) |
| 11 | 14' - 8" (4470mm) | 15' - 0" (4572mm) | 15' - 8" (4775mm) | 16' - 8" (5080mm) | 17' - 8" (5385mm) |
| 12 | 16' - 0" (4877mm) | 16' - 4" (4978mm) | 17' - 0" (5182mm) | 18' - 0" (5486mm) | 19' - 0" (5791mm) |
| 13 | 17'-4" (5283mm) | 17' - 8' (5385mm) | 18'-4" (5588mm) | 19'-4" (5893mm) | 20' - 4" (6198mm) |
| 14 | 18' - 8" (5690mm) | 19' - 0" (5791mm) | 19'-8" (5994mm) | 20' - 8" (6299mm) | 21' - 8" (6604mm) |
| 15 | 20' - 0" (6096mm) | 20' - 4" (6198mm) | 21' - 0" (6401mm) | 22' - 0" (6706mm) | 23' - 0" (7010mm) |
| 16 | 21'-4" (6502mm) | 21' - 8" (6604mm) | 22'-4" (6807mm) | 23'-4" (7112mm) | 24' - 4" (7417mm) |
| 17 | 22'-8" (6909mm) | 23' - 0" (7010mm) | 23' - 8" (7214mm) | 24' - 8" (7518mm) | 25' - 8" (7823mm) |
| 18 | 24' - 0" (7315mm) | 24' - 4" (7417mm) | 25' - 0" (7620mm) | 26' - 0" (7925mm) | 27' - 0" (8230mm) |
| 19 | 25' - 4" (7722mm) | 25' - 8" (7823mm) | 26' - 4" (8026mm) | 27'-4" (8331mm) | 28' - 4" (8636mm) |
| 20 | 26' - 8" (8128mm) | 27' - 0" (8230mm) | 27' - 8" (8433mm) | 28'-8" (8738mm) | 29' - 8" (9042mm) |
| 21 | 28' - 0" (8534mm) | 28'-4" (8636mm) | 29'-0" (8839mm) | 30' - 0" (9144mm) | 31' - 0" (9449mm) |
| 22 | 29'-4" (8941mm) | 29'-8" (9042mm) | 30' - 4" (9246mm) | 31' - 4" (9550mm) | 32' - 4" (9855mm) |
| 23 | 30' - 8" (9347mm) | 31' - 0" (9449mm) | 31' - 8" (9652mm) | 32' - 8" (9957mm) | 33' - 8" (10262mm) |
| 24 | 32' - 0" (9754mm) | 32'-4" (9855mm) | 33' - 0" (10058mm) | 34' - 0" (10363mm) | 35' - 0" (10668mm) |
| 25 | 33'-4" (10160mm) | $33^{\prime}-8{ }^{\prime \prime}(10262 \mathrm{~mm})$ | 34' - 4' (10465mm) | 35' - 4' (10770mm) | 36' - 4' (11074mm) |

## 4.9 - ESTIMATING FORM

Customer Name:
Date: $\qquad$
Project Name: $\qquad$
Wall Type (Circle): Frost Wall Basement Main Floor Second Floor Other

| Form Size (Circle): | $4 "$ | $6.25 "$ | $8 "$ | 10 | $12 "$ |
| :--- | :--- | :--- | :--- | :--- | :--- |

## Estimating Data

|  | Lineal Feet (LF) of Wall |  | LF Height Adjusters |
| :--- | :--- | :--- | :--- |
|  | Wall Height |  | LF Extended Brick Ledge |
|  | Number of $90^{\circ}$ Turns |  | LF Taper Top Form |
|  | Number of $45^{\circ}$ Turns |  | Height of Backfill |
|  | Number of Logix Courses |  | Square Footage (SF) of Openings |
|  | Number of Courses of Standards |  | Gross SF of Wall (GSF) |
|  | LF Form Lock |  | Net SF of Wall (NSF) |


| Quantity | Description | Notes |
| :--- | :--- | :--- |
|  | Standard Forms |  |
|  | Standard V12 Forms |  |
|  | $90^{\circ}$ Corner Forms |  |
|  | $90^{\circ}$ V12 Corner Forms |  |
|  | $45^{\circ}$ Corner Forms |  |
|  | Brick Ledge |  |
|  | Taper Top Forms |  |
|  | Double Taper Top Forms |  |
|  | Number of Height Adjusters (2' each) |  |
|  | Number of Form Lock (12.5' each) |  |
|  | Filament Tape (1 roll/50 blocks) |  |
|  | Zip Ties (1 bag/200 blocks) |  |
|  | Waterproofing Membrane (200sf/roll) |  |
|  | Rolls of Fiber Mesh (475sf/roll) |  |
|  | Bags of Prepcoat (85sf/bag) |  |
|  | LF/Type Rebar |  |
|  | Cubic Yards of Concrete |  |
|  | LF Window/Door Buck |  |
|  | Number of Alignment System Sets |  |
|  | Man Hours/sf |  |

## 5.0 - CAD DRAWINGS


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## 5.0 - CAD DRAWINGS

CAD drawings applicable for residential and commercial projects are available in the Technical Library at logixicf.com/technical-library in .dwg, .dxf, pdf and .jpg file formats. In addition, please refer to the Technical Library for updated and new drawings.

LOGIX carries both assembled form units, known as LOGIX PRO, and unassembled (or knock-down) systems known as LOGIX KD. In addition, LOGIX carries a number of accessories meant to make designing and constructing with ICFs much faster and easier.

NOTE: The tables and drawings represented herein are believed to be accurate and conforming to current design and construction practices. However, the tables and drawings should be used as a reference guide only. The user shall check to ensure the drawing meets local building codes, design and construction practices by consulting local building officials and professionals, including any additional requirements. Logix reserves the right to make changes to the tables and drawings without notice and assumes no liability in connection with the use of the tables and drawings including modification, copying or distribution.

## 5.1-LOGIX PRODUCTS <br> 5.1.1 - PRO FORMS










CAD DRAWINGS-PROFORMS







5.1.1.9 - V12 STANDARD


CAD DRAWINGS-PRO FORMS

### 5.1.2 - KD FORMS (KNOCK-DOWN FORMS)







CADDRAWINGS-KDFORMS







5.1.2.5 - LOGIX T-WALL


### 5.1.3 - ACCESSORIES

### 5.1.3.1 - MISC






CAD DRAWINGS - ACCESORIES: MISC



5.1.3.1.4 - LOGIX XTENDER 5.1.3.1.5-LOGIX HORIZONTAL \& VERTICAL

|  |  |
| :--- | :--- |
| Joint between blocks | $\mathrm{B} \longleftarrow$ |


STEEL






$\frac{\text { SIDE ELEVATION }}{\text { (with Xtenders) }}$









### 5.1.3.2 - PRO BUCK






### 5.1.3.3 - HEAT-SHEET









### 5.1.3.5 - D-RV PANEL INSERTS



S $\perp$ y ヨSNI f ヨ N $\forall$ d $\wedge$ y-





CAD DRAWINGS - ACCESSORIES: D-RVPANELINSERTS





5.2.1.2-9'-4" WALL WITH THICKENED SLAB

CAD DRAWINGS - WALLSECTIONS





### 5.2.2-1 STORY PLUS BASEMENT








CAD DRAWINGS - WALLSECTIONS
 5.2.2.7-10" TO 6.25" LOGIX TRANSITION




### 5.2.3-2 STORY PLUS BASEMENT



CAD DRAWINGS - WALLSECTIONS

## 5.3 - FOOTINGS AT EXTERIOR WALL 5.3.1 - PRE-CAST SLABS




### 5.3.2 - GRADE BEAM \& PILES








### 5.3.3 - BRICK LEDGE











### 5.3.4 - FOOTINGS FORMED WITH LOGIX




TING FORMED WITH LOGIX
BRICK LEDGE







## 5.4-FOOTINGS AT INTERIOR WALL <br> 5.4.1 - GRADE BEAM \& PILES



### 5.4.2 - SHALLOW FOOTINGS







## 5.5-FOUNDATION WALLS

### 5.5.1 - CRAWL SPACE





5.5.1.4-6.25" TO 4" LOGIX CRAWL SPACE










### 5.5.2 - FROST WALLS












5.5.2.8 - CAST-IN-PLACE SLAB WITH XP-1

$\square$


### 5.5.3 - BASEMENTS











### 5.5.4 - WATERPROOFING





5.5.4.2 - BRICK LEDGE FLASHING DETAILS


CAD DRAWINGS-FOUNDATION WALLS

## 5.6 - FLOOR CONNECTIONS AT EXTERIOR WALL 5.6.1 - LOGIX BEARING LENGTHS





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CAD DRAWINGS - FLOOR CONNECTIONSATEXTERIORWALL

### 5.6.2 - WOOD JOISTS





| E |  |
| :---: | :---: |
|  |  |









































### 5.6.3 - STEEL JOISTS






5.6.3.6 - OPEN WEB STEEL JOIST FORM
SUPPORT AT FLOOR TRANSITION
NOTES:

1. See Section 6 - Engineering in the LOGIX Design Manual or the
LOGIX Field Manual for reinforcement details.
2. A protective cover, such as tarp, should be placed over Logix form
panels in the vicinity where on-site welding and torch work is
conducted.

5.6.3.5 - STEEL ANGLE TO JOIST




### 5.6.4 - CAST-IN-PLACE




CAD DRAWINGS - FLOOR CONNECTIONSATEXTERIORWALL








5.6.4.9 - STAIR LANDING





### 5.6.5 - PRE-CAST SLABS



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5.6.5.6 - SPANCRETE TOPPING FLUSH TO

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## 5.7-FLOOR CONNECTIONS AT INTERIOR WALL






### 5.7.2 - PRE-CAST SLABS







### 5.7.3 - STEEL JOISTS





## 5.8 - ROOF \& PARAPETS AT EXTERIOR WALL

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5.8.2.4 - ICF PARAPET: FLAT ROOF ON OPEN WEB JOIST WITH INSULATIO







5.8.2.8 - PARAPET WITH SLOPED ROOF



### 5.8.3 - PRE-CAST





### 5.8.4 - STRAPS \& ANCHORS










### 5.8.5 - STRUCTURAL INSULATED PANELS









## 5.9 - ROOF \& PARAPETS AT INTERIOR WALL 5.9.1 - WOOD



### 5.9.2 - STEEL



only. The user shall check to ensure the drawing mee local building codes, design and construction practices by


5.10.1 - WEEP SCREED \& FLASHING






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### 5.11.2 - ATTACHMENTS










CAD DRAWINGS - EXTERIOR FINISHES \& ATTACHMENTS







### 5.12 - WINDOW, DOOR \& GARAGE OR BAY OPENINGS 5.12.1 - WINDOWS









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## 




















## 







## 





### 5.12.2 - DOORS







## 





### 5.12.3 - GARAGE OR BAY



(








### 5.13-WALL-TO-WALL CONNECTIONS 5.13.1 - FRAMED WALLS



CAD DRAWINGS-WALL-TO-WALLCONNECTIONS








### 5.13.2 - EXISTING WALLS






### 5.13.3 - WALL JOGS






CAD DRAWINGS-WALL-TO-WALLCONNECTIONS
 TO 8" T-WALL WITH END CAP











### 5.14 - STEEL REINFORCING

5.14.1 - WEB TIE REBAR SLOT LOCATIONS

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### 5.15 - BEAM CONNECTIONS 5.15.1 - WOOD BEAMS











SNOPD N







5.15.2.11 - STEEL DECK PORCH COVER

CAD DRAWINGS - BEAM CONNECTIONS





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CAD DRAWINGS-BEAM CONNECTIONS



### 5.15.3 - CAST-IN-PLACE





### 5.16 - COLUMN CONNECTIONS 5.16.1 - WOOD COLUMNS



CAD DRAWINGS-COLUMNCONNECTIONS

### 5.16.2 - STEEL COLUMNS





CADD R A WINGS - COLUMNCONNECTIONS







### 5.16.3 - CONCRETE COLUMNS







### 5.17 - LEDGE \& CORBELS

5.17.1 - LOGIX BRICK LEDGE










### 5.17.2 - FORMED BRICK LEDGE



### 5.17.3 - ANGLE IRON SEATS








### 5.17.4 - CORBELS





### 5.18 - STC WALL ASSEMBLIES











ECTION PORT FRAME
Logi 1 CF ( 8 "shown)

Projection
portframe


[^1]







5.20.7 - POOL SKIMMER

S 700 O

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## DISCLAIMER

By using the Logix Design Manual, in part or in whole, the user accepts the following terms and conditions.

The Logix Design Manual shall be used for the sole purpose of estimating, design or construction of Logix Insulated Concrete Forms used in residential, commercial or industrial structures.

The information represented herein is to be used as a reference guide only. The user shall check to ensure the information provided in this manual, including updates and amendments, meets local building codes and construction practices by consulting local building officials, construction and design professionals, including any additional requirements.

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## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## INTRODUCTION

Logix walls are intended to be used both above and below grade, and can carry large vertical as well as lateral loads. They are particularly effective for residential, commercial and industrial buildings; providing excellent insulation as well as thermal mass and structural strength. They can be easily adapted to accommodate concrete floors and other "non-standard" building systems.

Construction must be in conformance with the Logix Design Manual, including assembly of formwork, bracing, accurate rebar positioning, concrete mix design \& placement, and details for interconnection with the other building components.

## STRUCTURAL DESIGN AND PERFORMANCE

The Logix Building System can be used for an infinite variety of building situations with proper engineering. This report, with its load tables and diagrams, is intended to assist with the structural design of buildings using the Logix system for the basement only, or continuing to two stories abovegrade and/or roof. Where unusual conditions are encountered, it is recommended that the user consult a designer who can evaluate the loadings to the various components and who can appreciate the limitations of "prescriptive" design under unusual conditions. Connection details have generally been excluded from this report because of the great variety of floor and roof systems that can be used with the Logix wall system. The designer should refer to the Logix Design Manual and the literature for the various proprietary products that are available for connections, which are an important part of the total design.

## REINFORCEMENT TABLES

Above- and below-grade walls, lintel and shear wall reinforcement tables are provided in this report. The tables were developed using the applicable sections of Chapter 16 of the International Building Code 2018, Sections 404 and 611 of the International Residential Code 2012, and ACI 318 Building Code Requirements for Structural Concrete.

Table 1 makes use of plain concrete foundation walls adapted from the IRC 2018, Table 404.1.2(8), for Logix used below-grade. For walls that fall outside the scope of Table 1, Tables 2A, 2B, 2C and 2D are provided, which cover wall reinforcement for larger walls and larger loading conditions.

Tables 3A and 3B provides reinforcement tables for Logix walls used above-grade.

## HELIX TSMR TABLES - ALTERNATIVE TO REBAR REINFORCEMENT TABLES

Where applicable, Logix prescriptive engineering with Helix TSMR (Twisted Steel Micro Rebar), may be used in lieu of the reinforcement requirements in Tables 2A to 2D, and Tables 3A and 3B. Helix is steel fibre reinforcement that can significantly reduce the amount of horizontal and vertical reinforcement in above- and below-grade concrete walls, with exception of lintel and shear wall reinforcement. For more information, refer to the Logix Prescriptive Engineering Manual, developed by Helix specifically for Logix.

## LIMITATIONS

Building limitations used to develop above- and below-grade tables include:
Building perimeter $=80 \mathrm{ft}$ max $\times 40 \mathrm{ft}$ max
Roof clear span $=40 \mathrm{ft}$ max
Floor clear span $=32 \mathrm{ft}$ max
Number of stories above grade $=2$ max
Number of stories below grade $=1$
Tables 4A to 4E and Tables 5A to 5E provide lintel tables for factored uniform and concentrated loading conditions, respectively.

More specific design assumptions and limitations are located with the corresponding reinforcement tables.

## NOTES FOR TABLE 1 - BELOW-GRADE TABLE ADAPTED FROM IRC 2018

Table 1 was developed adapting Table 404.1.2(8), Minimum Vertical Reinforcement For 6-, 8-, 10 -Inch And 12 -Inch Nominal Flat Basement Walls, of IRC 2018. Table 1 allows the use of foundation walls without reinforcement (in lieu of Tables 2A to 2D) provided the walls meet the following criteria:

1. Minimum 28day compressive strength of concrete $=2500 \mathrm{psi}$
2. Concrete foundation walls with corbels (ie, brick ledge), brackets or other projections built into the wall for support of masonry veneer or other purposes are not within the scope of the tables in this section
3. Where vertical rebar is not required (NR), provide minimum horizontal rebar as follows (Table 404.1.2(1)):
4. Maximum unsupported height of basement wall is LESS than or equal to 8 ft - One No. 4 bar within 12 inches of the top of the wall story and one No. 4 bar near mid-height of the wall story
5. Maximum unsupported height of basement wall is GREATER than 8 ft - One No. 4 bar within 12 inches of the top of the wall story and one No. 4 bar near third points in the wall story
6. Walls are not subject to hydrostatic pressure from ground water
7. Walls must be laterally supported at top and bottom of wall before backfilling
8. Interpolation is not permitted
9. Maximum 60 feet in plan dimensions, floors not more than 32 feet or roofs not more than 40 feet in clear span. Buildings shall not exceed 2 stories above-grade with each story not more than 10 feet high. Maximum ground snow load of 70 psf, and located in Seismic Design Categories A, B or C. For Seismic Design Categories D0, D1, or D2 see Items 7 to 9.
10. In Seismic Design Category D0, D1, and D2, concrete foundation walls supporting above grade concrete or Logix walls shall comply with above and below-grade tables in this manual, ACl 318 , ACI 332 or PCA 100
11. In Seismic Design Category D0, D1, and D2, where Table 1 permits plain concrete, and supporting light-frame walls shall comply with the following:
12. Wall height shall not exceed 8 feet
13. Unbalanced backfill height shall not exceed 4 feet
14. Minimum thickness for plain concrete foundation walls shall be 7.5 inches except that 6 inches is permitted where the maximum wall height is 4 feet, 6 inches
15. Minimum reinforcement shall consist of one \#4 horizontal bar within the top 12 inches of the wall
16. Backfill shall not be placed against the wall until the wall has sufficient strength and has been anchored to the floor above, or has been sufficiently braced to prevent damage by the back fill.
17. For walls that fall outside the scope Table 1 see "Notes for Tables 2A to 2D - Logix Below-grade Tables."

LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS
TABLE 1 - LOGIX BELOW-GRADE WALLS MINIMUM VERTICAL REINF - IRC2018

TABLE 1 - LOGIX BELOW-GRADE WALLS MINIMUM VERTICAL REINFORCEMENT - IRC2018
NOTE: LOGIX recommends builders, owners and/or designers using these tables confirm that on-site building conditions are w/in the scope of the tables being used.

| Height of Basement Wall, ft | Max. Unbalanced Backfill Height, ft | 6.25" LOGIX |  |  | 8" LOGIX |  |  | 10" LOGIX |  |  | 12" LOGIX |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Design Lateral Soil Load (psf per foot of depth) |  |  | Design Lateral Soil Load (psf per foot of depth) |  |  | Design Lateral Soil Load (psf per foot of depth) |  |  | Design Lateral Soil Load (psf per foot of depth) |  |  |
|  |  | 30 | 45 | 60 | 30 | 45 | 60 | 30 | 45 | 60 | 30 | 45 | 60 |
| 5 | 5 | RR | RR | RR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
| 6 | 4 | RR | RR | RR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
|  | 5 | RR | RR | RR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
|  | 6 | RR | RR | RR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
| 7 | 4 | RR | RR | RR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
|  | 5 | RR | RR | RR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
|  | 6 | RR | RR | RR | NR | NR | RR | NR | NR | NR | NR | NR | NR |
|  | 7 | RR | RR | RR | NR | RR | RR | NR | NR | NR | NR | NR | NR |
| 8 | 4 | RR | RR | RR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
|  | 5 | RR | RR | RR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
|  | 6 | RR | RR | RR | NR | NR | RR | NR | NR | NR | NR | NR | NR |
|  | 7 | RR | RR | RR | NR | RR | RR | NR | NR | RR | NR | NR | NR |
|  | 8 | RR | RR | RR | RR | RR | RR | NR | RR | RR | NR | NR | NR |
| 9 | 4 | RR | RR | RR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
|  | 5 | RR | RR | RR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
|  | 6 | RR | RR | RR | NR | NR | RR | NR | NR | NR | NR | NR | NR |
|  | 7 | RR | RR | RR | NR | RR | RR | NR | NR | RR | NR | NR | NR |
|  | 8 | RR | RR | RR | RR | RR | RR | NR | RR | RR | NR | NR | RR |
|  | 9 | RR | RR | RR | RR | RR | RR | NR | RR | RR | NR | NR | RR |
| 10 | 4 | RR | RR | RR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
|  | 5 | RR | RR | RR | NR | NR | NR | NR | NR | NR | NR | NR | NR |
|  | 6 | RR | RR | RR | NR | NR | RR | NR | NR | NR | NR | NR | NR |
|  | 7 | RR | RR | RR | NR | RR | RR | NR | NR | RR | NR | NR | NR |
|  | 8 | RR | RR | RR | RR | RR | RR | NR | RR | RR | NR | NR | RR |
|  | 9 | RR | RR | RR | RR | RR | RR | RR | RR | RR | NR | RR | RR |
|  | 10 | RR | RR | RR | RR | RR | RR | RR | RR | RR | NR | RR | RR |

NOTES:

1. "NR" denotes plain concrete or no reinforcement required, except 6.25 " LOGIX will requires \#4@32" on center for Grade 40 Steel Bars and \#4@48" on center for Grade 60 Steel Bars.
2. "RR" denotes reinforcement required. Refer to Tables 2A to 2D for LOGIX Below-grade tables for required reinforcement.
3. Table 1 values are based on concrete with a minimum specified compressive strength of $2,500 \mathrm{psi}$
4. Bar Spacing Shall not exceed 48 inches on center and shall not be less than one-half the nominal wall thickness.
5. Table 1 shall be read in conjunction with " Notes for Table R404.1.2(1) to Table R404.1.2(9) - Below-grade Table Adapted from IRC 2018".

## NOTES FOR TABLES 2A TO 2D - LOGIX BELOW-GRADE TABLES

Tables 2A to 2D are recommended for use when larger walls and/or loading conditions fall outside the scope of Table 1. Alternatively, and where applicable.

Tables 2A to 2D shall be used in conjunction with corresponding Figures 2A to 2D, the notes listed below, and the building limitations noted in the "Reinforcement Tables" section, which form the basis of these tables.

1. Vertical rebar spacing shown in the tables provide simple placement between ICF ties.
2. Steel yield strength $=40 \mathrm{ksi}, 28$ day concrete compressive strength $=3 \mathrm{ksi}$
3. Rebar spacing is based on 40 ksi reinforcing steel. For spacing based on 60 ksi reinforcing steel multiply spacings by 1.5 .
4. Deflection criteria $=\mathrm{L} / 240$
5. Snow load $=70$ psf
6. Assumed eccentricity $=3 "$ (to account for loads on Logix Brick Ledge).
7. The basement walls must be supported at the top and bottom of the wall.
8. For light vehicles parked or travelling near the wall use reinforcement corresponding to 1 feet higher backfill.
9. Where spaces have been left blank, the corresponding bar size is presumed to be less economical and/or practical than that shown. Consult a local licensed engineer to determine proper design.
10. For walls with over $50 \%$ of height exposed to wind, also check rebar requirements for abovegrade walls.
11. Except as noted for seismic design, horizontal rebar shall be \#4 at 32 inches on center. At least one rebar shall be placed at the bottom course and top course.
12. In Seismic Design Categories D0, D1, and D2, the reinforcing steel shall meet the requirements of ASTM A 706 for low-alloy steel with a minimum yield strength of 60 ksi .
13. For townhouses in Seismic Category C, the minimum vertical reinforcement shall be one \#5 at 24 inches on center or one \#4 bar at 16 inches on center, and the minimum horizontal reinforcement shall be one \#4 bar at 16 inches on center.
14. For all buildings in Seismic Design Categories D0, D1 and D2, the minimum vertical reinforcement shall be one \#5 at 18 inches on center or one \#4 bar at 12 inches on center, and the minimum horizontal reinforcement shall be one \#5 bar at 16 inches on center.
15. Horizontal reinforcement shall be continuous around building corners using corner bars or by bending the bars. The minimum lap splice shall be 24 inches. For townhouses in Seismic Design Categories D0, D1, and D2, each end of all horizontal reinforcement shall terminate with a standard hook or lap splice.
16. Carefully consider floor/wall connection details for lateral loads, especially with higher backfills, walkout basements, and active seismic areas.
17. Soil density is often referred to as "equivalent fluid density" or design fluid pressure.
18. Where applicable alternative Helix dosage Tables 2A-H to 2D-H may be used in lieu of Logix reinforcement Tables 2A to 2D.

## NOTES FOR TABLES 2A to 2D－LOGIX BELOW－GRADE TABLES Cont＇d



Fig 2A
Assumed typical flooring，wall \＆roof for Table 2A．Height \＆ thickness of above－grade walls， floor \＆roof spans，including materials（i．e．，wood frame， concrete，and cladding）can vary provided the total factored load on basement wall does not exceed 6.7 kips／ft．


Fig 2B
Assumed typical flooring，wall \＆roof for Table 2B．Height \＆thickness of above－grade walls，floor \＆roof spans， including materials（i．e．，wood frame，concrete，and cladding） can vary provided the total factored load on basement wall does not exceed $8 \mathrm{kips} / \mathrm{ft}$ ．


Fig 2C
Assumed typical flooring，wall \＆roof for Table 2C．Height \＆thickness of above－grade walls，floor \＆roof spans， including materials（i．e．，wood frame，concrete，and cladding） can vary provided the total factored load on basement wall does not exceed 8 kips／ft．


Fig 2D
Assumed typical flooring，wall \＆roof for Table 2D．Height \＆thickness of above－grade walls，floor \＆roof spans， including materials（i．e．，wood frame，concrete，and cladding） can vary provided the total factored load on basement wall does not exceed 9 kips／ft．

| MaximumHeightBasementWall, ft | Maximum <br> Unbalanced <br> Backfill <br> Height, ft <br> 4 | Bar Spacing in. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | MaximumEquivalent Density 30pcf |  |  |  |  | MaximumEquivalent Density 45pcf |  |  |  |  | MaximumEquivalent Density 60pcf |  |  |  |  | MaximumEquivalent Density 75pcf |  |  |  |  |
|  |  | 48 | 48 | 48 | 48 | 48 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 |
|  | 5 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 |
|  | 6 | 24 | 48 | 48 | 48 | 48 | 24 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 16 | 24 | 32 | 48 | 48 |
|  | 7 | 24 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 8 | 16 | 32 | 40 | 48 | 12 | 16 | 24 | 32 | 48 |
|  | 8 | 16 | 32 | 40 | 48 | 48 | 12 | 16 | 32 | 40 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 |
| 9 | 4 | 48 | 48 | 48 | 48 | 48 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 48 | 48 | 48 | 48 |
|  | 5 | 32 | 48 | 48 | 48 | 48 | 24 | 48 | 48 | 48 | 48 | 24 | 32 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 |
|  | 6 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 32 | 40 | 48 |
|  | 7 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 40 | 48 | 8 | 16 | 24 | 32 | 40 |
|  | 8 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 40 | 48 | 8 | 16 | 16 | 32 | 40 | 8 | 12 | 16 | 24 | 32 |
|  | 9 | 12 | 24 | 32 | 48 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 |
| 10 | 4 | 48 | 48 | 48 | 48 | 48 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 48 | 48 | 48 | 48 |
|  | 5 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 24 | 32 | 48 | 48 | 48 | 16 | 32 | 40 | 48 | 48 |
|  | 6 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 32 | 40 | 48 |
|  | 7 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 16 | 16 | 32 | 40 |
|  | 8 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 12 | 16 | 24 | 24 |
|  | 9 | 12 | 16 | 32 | 40 | 48 | 8 | 12 | 16 | 24 | 40 | 6 | 8 | 16 | 16 | 24 | 6 | 8 | 12 | 16 | 24 |
|  | 10 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 |
| 11 | 4 | 48 | 48 | 48 | 48 | 48 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 |
|  | 5 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 |
|  | 6 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 40 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 40 | 48 |
|  | 7 | 16 | 32 | 40 | 48 | 48 | 12 | 24 | 32 | 40 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 |
|  | 8 | 16 | 24 | 32 | 48 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 16 | 16 | 24 |
|  | 9 | 12 | 16 | 24 | 40 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 16 | 16 | 24 | 6 | 8 | 12 | 16 | 16 |
|  | 10 | 8 | 16 | 24 | 32 | 40 | 6 | 8 | 16 | 16 | 24 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 |
|  | 11 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 8 | 8 | 12 |
| 12 | 4 | 48 | 48 | 48 | 48 | 48 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 |
|  | 5 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 |
|  | 6 | 24 | 40 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 40 | 48 |
|  | 7 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 32 | 40 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 |
|  | 8 | 12 | 24 | 32 | 48 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 |
|  | 9 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 8 | 8 | 16 | 16 |
|  | 10 | 8 | 16 | 16 | 24 | 40 | 6 | 8 | 12 | 16 | 24 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 |
|  | 11 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 |
|  | 12 | 6 | 8 | 16 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 8 | 8 | 12 | 6 | 6 | 6 | 8 | 8 |
|  |  | \#4 | \#5 | \#6 | \#7 | \#8 | \#4 | \#5 | \#6 | \#7 | \#8 | \#4 | \#5 | \#6 | \#7 | \#8 | \#4 | \#5 | \#6 | \#7 | \#8 |

NOTES:

1. Reinforcement to be placed on interior face of concrete wall. Effective depth of vertical rebar (exterior face of concrete to center of vertical rebar) $=4.375^{\prime \prime}$
2. Table 2 A shall be read in conjunction with Fig 2 A , and section "NOTES FOR TABLES 2 A to 2 D - LOGIX BELOW-GRADE TABLES."
3. Steel yield strength $=40 \mathrm{ksi}, 28$ day concrete compressive strenght $=3 \mathrm{ksi}$.
4. Where cells show "-" engineering is required.

| Maximum <br> Height <br> Basement <br> Wall, ft | Maximum Unbalanced Backfill Height, ft | Bar Spacing, in. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Maximum Equivalent Density 30pcf |  |  |  |  | Maximum Equivalent Density 45pcf |  |  |  |  | Maximum Equivalent Density 60pcf |  |  |  |  | Maximum Equivalent Density 75pcf |  |  |  |  |
| 8 | 4-5 | 48 | 48 | 48 | 48 | 48 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 |
|  | 6 | 40 | 48 | 48 | 48 | 48 | 24 | 48 | 48 | 48 | 48 | 24 | 32 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 |
|  | 7 | 32 | 48 | 48 | 48 | 48 | 24 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 24 | 40 | 48 | 48 |
|  | 8 | 24 | 40 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 32 | 40 | 48 | 12 | 16 | 32 | 32 | 48 |
| 9 | 4-5 | 48 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 |
|  | 6 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 48 | 48 | 48 |
|  | 7 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 32 | 40 | 48 |
|  | 8 | 24 | 32 | 48 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 40 | 48 | 8 | 16 | 24 | 32 | 40 |
|  | 9 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 32 | 40 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 24 | 24 | 32 |
| 10 | 4-5 | 48 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 |
|  | 6 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 48 | 48 | 48 |
|  | 7 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 40 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 32 | 40 | 48 |
|  | 8 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 16 | 24 | 24 | 40 |
|  | 9 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 40 | 8 | 12 | 16 | 24 | 32 |
|  | 10 | 12 | 24 | 32 | 40 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 16 | 16 | 24 |
| 11 | 4-5 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 |
|  | 6 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 48 | 48 | 48 |
|  | 7 | 24 | 40 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 24 | 32 | 40 | 48 | 12 | 16 | 32 | 32 | 48 |
|  | 8 | 16 | 32 | 48 | 48 | 48 | 12 | 16 | 32 | 40 | 48 | 12 | 16 | 24 | 32 | 40 | 8 | 12 | 24 | 24 | 32 |
|  | 9 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 16 | 16 | 24 |
|  | 10 | 12 | 16 | 32 | 40 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 16 | 16 | 24 | 6 | 8 | 16 | 16 | 24 |
|  | 11 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 12 | 12 | 16 |
| 12 | 4-5 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 24 | 32 | 48 | 48 | 48 |
|  | 6 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 40 | 48 | 48 | 16 | 24 | 40 | 48 | 48 |
|  | 7 | 24 | 40 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 32 | 40 | 48 | 12 | 16 | 32 | 32 | 48 |
|  | 8 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 32 | 40 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 24 | 24 | 32 |
|  | 9 | 16 | 24 | 32 | 48 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 16 | 16 | 24 |
|  | 10 | 12 | 16 | 24 | 40 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 8 | 12 | 16 | 16 |
|  | 11 | 8 | 16 | 24 | 32 | 40 | 6 | 12 | 16 | 16 | 24 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 12 | 12 | 16 |
|  | 12 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 12 | 8 | 12 |
| 14 | 4 | 48 | 48 | 48 | 48 | 48 | 48 | 48 | 48 | 48 | 48 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 |
|  | 5 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 24 | 32 | 48 | 48 | 48 |
|  | 6 | 32 | 48 | 48 | 48 | 48 | 24 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 16 | 24 | 40 | 48 | 48 |
|  | 7 | 24 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 40 | 48 | 8 | 16 | 24 | 32 | 40 |
|  | 8 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 40 | 48 | 8 | 16 | 16 | 24 | 40 | 8 | 12 | 16 | 24 | 32 |
|  | 9 | 8 | 16 | 32 | 40 | 48 | 8 | 16 | 16 | 24 | 40 | 6 | 12 | 16 | 24 | 24 | 6 | 8 | 16 | 16 | 24 |
|  | 10 | 12 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 12 | 12 | 16 |
|  | 11 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 8 | 8 | 16 |
|  | 12 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 8 | 8 | 12 |
|  | 13 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 8 | 8 |
|  | 14 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 |
| 16 | 4 | 48 | 48 | 48 | 48 | 48 | 48 | 48 | 48 | 48 | 48 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 |
|  | 5 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 |
|  | 6 | 32 | 48 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 24 | 40 | 40 | 48 |
|  | 7 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 40 | 48 | 8 | 16 | 24 | 32 | 40 |
|  | 8 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 12 | 16 | 24 | 24 |
|  | 9 | 12 | 16 | 24 | 40 | 48 | 8 | 8 | 16 | 24 | 32 | 6 | 8 | 16 | 16 | 24 | 6 | 8 | 16 | 16 | 16 |
|  | 10 | 8 | 16 | 24 | 32 | 40 | 6 | 8 | 16 | 16 | 24 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 12 | 12 | 16 |
|  | 11 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 8 | 16 | 6 | 6 | 8 | 8 | 12 |
|  | 12 | 6 | 8 | 16 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 8 | 8 | 12 | 6 | 6 | 8 | 8 | 8 |
|  | 13 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 |
|  | 14 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 8 | 12 | 6 | 6 | 6 | 8 | 8 | 6 | 6 | 6 | 6 | 8 |
|  | 15 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 6 |
|  |  | \#4 | \#5 | \#6 | \#7 | \#8 | \#4 | \#5 | \#6 | \#7 | \#8 | \#4 | \#5 | \#6 | \#7 | \#8 | \#4 | \#5 | \#6 | \#7 | \#8 |

NOTES:

1. Reinforcement to be placed on interior face of concrete wall. Effective depth of vertical rebar (exterior face of concrete to center of vertical rebar) $=6$ "
2. Table $2 B$ shall be read in conjunction with Fig 2B, and section "Notes for Tables 2A to 2D - LOGIX Below-grade Tables."
3. Steel yield strength $=40 \mathrm{ksi}$, 28 day concrete compressive strenght $=3 \mathrm{ksi}$.
4. Where cells show "- " engineering is required.

NOTE: LOGIX recommends builders, owners and/or designers using these tables confirm that on-site building conditions are $w /$ in the scope of the tables being used.

| Maximum | Maximum <br> Unbalanced <br> Backfill <br> Height, ft <br> $4-8$ | Bar Spacing, in. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Height Basement Wall, ft |  | Maximum Equivalent Density 30pcf |  |  |  |  | Maximum Equivalent Density 45pcf |  |  |  |  | Maximum Equivalent Density 60pcf |  |  |  |  | Maximum Equivalent Density 75pcf |  |  |  |  |
| 8 |  | 32 | 48 | 48 | 48 | 48 | 24 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 24 | 32 | 48 | 48 |
| 9 | 4-7 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 |
|  | 8 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 40 | 48 |
|  | 9 | 24 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 40 | 48 | 8 | 16 | 24 | 32 | 40 |
| 10 | 4-7 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 40 | 48 | 48 | 16 | 24 | 32 | 48 | 48 |
|  | 8 | 24 | 40 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 32 | 48 |
|  | 9 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 16 | 16 | 24 | 40 |
|  | 10 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 40 | 48 | 8 | 16 | 16 | 24 | 40 | 8 | 12 | 16 | 24 | 32 |
| 11 | 4-7 | 32 | 48 | 48 | 48 | 48 | 24 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 16 | 24 | 32 | 48 | 48 |
|  | 8 | 24 | 40 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 32 | 40 | 48 | 12 | 16 | 24 | 32 | 48 |
|  | 9 | 16 | 32 | 48 | 48 | 48 | 12 | 16 | 32 | 40 | 48 | 12 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 |
|  | 10 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 12 | 16 | 16 | 24 |
|  | 11 | 12 | 16 | 32 | 40 | 48 | 8 | 16 | 16 | 24 | 40 | 6 | 12 | 16 | 24 | 24 | 6 | 8 | 12 | 16 | 24 |
| 12 | 4-6 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 |
|  | 7 | 32 | 48 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 24 | 32 | 40 | 48 |
|  | 8 | 24 | 40 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 40 | 48 | 8 | 16 | 24 | 32 | 40 |
|  | 9 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 32 | 40 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 |
|  | 10 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 16 | 16 | 24 |
|  | 11 | 12 | 16 | 24 | 40 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 16 | 16 | 24 | 6 | 8 | 12 | 16 | 16 |
|  | 12 | 12 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 |
| 14 | 4-6 | 40 | 48 | 48 | 48 | 48 | 24 | 48 | 48 | 48 | 48 | 24 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 |
|  | 7 | 24 | 48 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 32 | 40 | 48 |
|  | 8 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 16 | 16 | 32 | 40 |
|  | 9 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 8 | 12 | 16 | 24 | 32 |
|  | 10 | 12 | 16 | 32 | 40 | 48 | 8 | 16 | 16 | 24 | 40 | 6 | 12 | 16 | 24 | 24 | 6 | 8 | 12 | 16 | 24 |
|  | 11 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 8 | 8 | 12 | 16 |
|  | 12 | 8 | 16 | 16 | 24 | 40 | 6 | 8 | 12 | 16 | 24 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 |
|  | 13 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 8 | 8 | 12 |
|  | 14 | 6 | 12 | 16 | 16 | 24 | 6 | 8 | 12 | 12 | 16 | 6 | 6 | 8 | 12 | 12 | 6 | 6 | 6 | 8 | 12 |
| 16 | 4-6 | 40 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 |
|  | 7 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 40 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 40 | 48 |
|  | 8 | 16 | 32 | 48 | 48 | 48 | 12 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 |
|  | 9 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 16 | 16 | 24 |
|  | 10 | 12 | 16 | 24 | 40 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 16 | 16 | 24 | 6 | 8 | 12 | 16 | 16 |
|  | 11 | 8 | 16 | 24 | 32 | 40 | 6 | 12 | 16 | 16 | 24 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 |
|  | 12 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 12 | 12 | 16 | 6 | 6 | 8 | 8 | 12 |
|  | 13 | 6 | 8 | 16 | 24 | 24 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 12 | 6 | 6 | 6 | 8 | 12 |
|  | 14 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 8 | 8 |
|  | 15 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 12 | 6 | 6 | 6 | 8 | 8 | 6 | 6 | 6 | 6 | 8 |
|  | 16 | 6 | 8 | 12 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 8 |


| Maximum Height Basement Wall, ft | Maximum <br> Unbalanced <br> Backfill <br> Height, ft | Bar Spacing, in. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Maximum Equivalent Density 30pcf |  |  |  |  | Maximum Equivalent Density 45pcf |  |  |  |  | Maximum Equivalent Density 60pcf |  |  |  |  | Maximum Equivalent Density 75pcf |  |  |  |  |
| 18 | 4-6 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 |
|  | 7 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 40 | 48 | 48 | 12 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 32 | 48 |
|  | 8 | 16 | 32 | 48 | 48 | 48 | 8 | 16 | 32 | 40 | 48 | 12 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 |
|  | 9 | 16 | 24 | 32 | 48 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 |
|  | 10 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 8 | 12 | 16 | 16 |
|  | 11 | 8 | 16 | 16 | 32 | 40 | 6 | 8 | 16 | 16 | 24 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 |
|  | 12 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 |
|  | 13 | 6 | 8 | 16 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 8 | 8 | 12 | 6 | 6 | 6 | 8 | 8 |
|  | 14 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 |
|  | 15 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 8 | 8 | 6 | 6 | 6 | 6 | 8 |
|  | 16 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 6 |
|  | 17 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 8 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
|  | 18 | 6 | 6 | 8 | 8 | 12 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
| 20 | 4-6 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 |
|  | 7 | 24 | 40 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 24 | 32 | 40 | 48 | 12 | 16 | 24 | 32 | 48 |
|  | 8 | 16 | 32 | 40 | 48 | 48 | 12 | 16 | 32 | 40 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 |
|  | 9 | 12 | 24 | 32 | 48 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 |
|  | 10 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 8 | 8 | 12 | 16 |
|  | 11 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 8 | 12 | 16 |
|  | 12 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 8 | 16 | 6 | 6 | 6 | 8 | 12 |
|  | 13 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 8 | 8 |
|  | 14 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 8 | 12 | 6 | 6 | 6 | 8 | 8 | 6 | 6 | 6 | 6 | 8 |
|  | 15 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 6 |
|  | 16 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 8 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 6 |
|  | 17 | 6 | 6 | 8 | 8 | 12 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
|  | 18 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
|  | 19 | 6 | 6 | 6 | 8 | 8 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
|  | 20 | 6 | 6 | 6 | 8 | 8 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
|  |  | \#4 | \#5 | \#6 | \#7 | \#8 | \#4 | \#5 | \#6 | \#7 | \#8 | \#4 | \#5 | \#6 | \#7 | \#8 | \#4 | \#5 | \#6 | \#7 | \#8 |

NOTES:

1. Reinforcement to be placed on interior face of concrete wall. Effective depth of vertical rebar (exterior face of concrete to center of vertical rebar $=8 \prime$
2. Table 2 C shall be read in conjunction with Fig 2 C , and section " Notes for Tables 2 A to 2 D - LOGIX Below-grade Tables."
3. Steel yield strength $=40 \mathrm{ksi}, 28$ day concrete compressive strenght $=3 \mathrm{ksi}$.
4. Where cells show "- " engineering is required.

| Maximum Height Basement Wall, ft | Maximum Unbalanced Backfill Height, ft | Bar Spacing, in. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Maximum Equivalent Density 30pcf |  |  |  |  | Maximum Equivalent Density 45pcf |  |  |  |  | Maximum Equivalent Density 60pcf |  |  |  |  | Maximum Equivalent Density 75pcf |  |  |  |  |
| 14 | 4-6 | 48 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 24 | 32 | 48 | 48 | 48 |
|  | 7 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 40 | 48 | 48 | 16 | 24 | 32 | 48 | 48 |
|  | 8 | 24 | 40 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 24 | 32 | 40 | 48 | 12 | 16 | 24 | 32 | 48 |
|  | 9 | 16 | 32 | 48 | 48 | 48 | 12 | 24 | 32 | 40 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 |
|  | 10 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 12 | 16 | 16 | 24 |
|  | 11 | 12 | 16 | 32 | 40 | 48 | 8 | 12 | 16 | 24 | 40 | 6 | 8 | 16 | 16 | 24 | 6 | 8 | 12 | 16 | 24 |
|  | 12 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 8 | 12 | 12 | 16 |
|  | 13 | 8 | 16 | 24 | 32 | 40 | 6 | 8 | 16 | 16 | 24 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 |
|  | 14 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 8 | 8 | 12 |
| 16 | 4-6 | 48 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 |
|  | 7 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 16 | 24 | 32 | 48 | 48 |
|  | 8 | 24 | 40 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 32 | 40 | 48 | 12 | 16 | 24 | 32 | 40 |
|  | 9 | 16 | 32 | 40 | 48 | 48 | 12 | 16 | 32 | 40 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 |
|  | 10 | 16 | 24 | 32 | 48 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 |
|  | 11 | 12 | 16 | 24 | 40 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 8 | 12 | 16 | 16 |
|  | 12 | 8 | 16 | 24 | 32 | 40 | 6 | 12 | 16 | 16 | 24 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 |
|  | 13 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 8 | 12 | 12 |
|  | 14 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 |
|  | 15 | 6 | 8 | 16 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 8 | 8 | 12 | 6 | 6 | 6 | 8 | 8 |
|  | 16 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 |
| 18 | 4-6 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 |
|  | 7 | 32 | 48 | 48 | 48 | 48 | 24 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 24 | 32 | 48 | 48 |
|  | 8 | 24 | 40 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 40 | 48 | 8 | 16 | 24 | 32 | 40 |
|  | 9 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 40 | 48 | 8 | 16 | 16 | 32 | 40 | 8 | 12 | 16 | 24 | 32 |
|  | 10 | 12 | 24 | 32 | 48 | 48 | 8 | 16 | 24 | 32 | 40 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 |
|  | 11 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 8 | 12 | 16 | 16 |
|  | 12 | 8 | 16 | 16 | 24 | 40 | 6 | 8 | 12 | 16 | 24 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 |
|  | 13 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 8 | 16 | 16 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 |
|  | 14 | 6 | 12 | 16 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 8 | 8 | 12 | 6 | 6 | 6 | 8 | 12 |
|  | 15 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 |
|  | 16 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 8 | 12 | 6 | 6 | 6 | 8 | 8 | 6 | 6 | 6 | 6 | 8 |
|  | 17 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 6 |
|  | 18 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 8 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 6 |
| 20 | 4-6 | 40 | 48 | 48 | 48 | 48 | 32 | 48 | 48 | 48 | 48 | 24 | 40 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 |
|  | 7 | 32 | 48 | 48 | 48 | 48 | 16 | 32 | 48 | 48 | 48 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 32 | 40 | 48 |
|  | 8 | 24 | 32 | 48 | 48 | 48 | 16 | 24 | 32 | 48 | 48 | 12 | 16 | 24 | 40 | 48 | 8 | 16 | 24 | 32 | 40 |
|  | 9 | 16 | 24 | 40 | 48 | 48 | 12 | 16 | 24 | 40 | 48 | 8 | 12 | 16 | 24 | 40 | 8 | 12 | 16 | 24 | 32 |
|  | 10 | 12 | 16 | 32 | 40 | 48 | 8 | 16 | 16 | 24 | 40 | 6 | 12 | 16 | 16 | 24 | 6 | 8 | 12 | 16 | 24 |
|  | 11 | 12 | 16 | 24 | 32 | 48 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 |
|  | 12 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 8 | 12 | 12 |
|  | 13 | 8 | 12 | 16 | 24 | 32 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 |
|  | 14 | 6 | 8 | 12 | 16 | 24 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 8 | 8 |
|  | 15 | 6 | 8 | 12 | 16 | 16 | 6 | 6 | 8 | 12 | 12 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 |
|  | 16 | 6 | 8 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 8 |
|  | 17 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 6 |
|  | 18 | 6 | 6 | 8 | 12 | 16 | 6 | 6 | 6 | 8 | 8 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
|  | 19 | 6 | 6 | 8 | 8 | 12 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
|  | 20 | 6 | 6 | 6 | 8 | 12 | 6 | 6 | 6 | 6 | 8 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
|  |  | \#4 | \#5 | \#6 | \#7 | \#8 | \#4 | \#5 | \#6 | \#7 | \#8 | \#4 | \#5 | \#6 | \#7 | \#8 | \#4 | \#5 | \#6 | \#7 | \#8 |

NOTES:

1. Effective depth (out face of concrete to center of vertical rebar) $=10$ "
2. Provide additional mat of rebar near exterior face of concrete surface:

Horizontal $=$
\#4 @32" o/c.

- Vertical = \#4
to match vertical rebar spacing

3. Table 2 D shall be read conjunction with Fig 2D, and section "Notes for Tables 2A to 2D - LOGIX Belowgrade Tables."
4. Steel yield strength $=40 \mathrm{ksi}$,

28 day concrete
compressive strength $=3$
ksi.
5. Where cells show "-"
engineering is required.

## NOTES FOR ABOVE-GRADE WALL TABLES - TABLES 3A \& 3B

Table 3A covers reinforcement for Logix above-grade walls with wind speeds up to 150 mph . For larger wind speeds see Table 3B, which covers wind speeds up to 300 mph .

Logix above-grade tables cover three different construction types:

- One storey Logix supporting wood roof frame (Fig. 3A)
- One storey Logix supporting 2nd storey wood frame plus wood roof frame (Fig. 3B)
- Two storey Logix supporting wood roof frame (Fig. 3C)

For two story buildings, the height of the second story wall is equal to the height of the first story provided the height of the first storey wall is not more than 12 feet high.

For first story walls greater than 12 feet high, the second story wall height is a maximum of 12 feet.
With the exception of 4" Logix, the second story concrete wall thickness is one size less than the concrete core thickness used for the first storey wall.


Assumed typical flooring, wall \& roof section for Tables 3A and 3B, Logix Supporting Roof Only.


Assumed typical flooring, wall \& roof section for Tables 3A and 3B, Logix Supporting 2nd Story Wood Frame \& Roof Structure.
 Assumed typical flooring, wall \& roof section for Tables 3A and 3B, Logix Supporting 2nd Story Logix \& Roof Structure.

## LOGIX® ${ }^{\circledR}$ INSULATED CONCRETE FORMS

## NOTES FOR ABOVE-GRADE WALL TABLES - Tables 3A \& 3B Cont'd

The above-grade tables shall be used in conjunction with the notes listed below, the building limitations noted in the "Reinforcement Tables" section, and Figures 3A to 3B, which form the basis of this table.

1. Vertical rebar spacing shown in the tables provide simple placement between ICF ties.
2. Steel yield strength $=40 \mathrm{ksi}$ and 60 ksi for Table 3A and 3B, respectively. 28 day concrete compressive strength $=3 \mathrm{ksi}$
3. For rebar spacing based on 40 ksi reinforcing steel multiply spacing by 1.5 if using 60 ksi steel.
4. Deflection criteria $=\mathrm{L} / 240$
5. Snow load $=70 \mathrm{psf}$
6. Assumed eccentricity $=1$ " .
7. The walls must be supported at the top and bottom of the wall.
8. Where spaces have been left blank, the corresponding bar size is presumed to be less economical and/or practical than that shown. Consult a local licensed engineer to determine proper design.
9. Except as noted for seismic considerations, vertical rebar shall be placed in middle of wall, and minimum horizontal rebar shall be:
-4" \& 6.25" Logix = \#4 @ 32" on center
-8" \& 10" Logix = \#4 @ 16" on center
Provide additional mat of rebar for 12" Logix

- Horizontal rebar = \#4 @ 32" on center (double mat)
- Vertical rebar = to match vertical bar spacing in Tables 3A or 3B, whichever applies.

Provide at least one \#4 bar (two for 12" Logix) to be placed at the bottom course and top course.
10. In Seismic Design Categories D0, D1, and D2, the reinforcing steel shall meet the requirements of ASTM A 706 for low-alloy steel with a minimum yield strength of 60 ksi .
11. For townhouses in Seismic Category C, the minimum vertical reinforcement shall be one \#5 at 24 inches on center or one \#4 bar at 16 inches on center, and the minimum horizontal reinforcement shall be one \#4 bar at 16 inches on center.
12. For all buildings in Seismic Design Categories D0, D1 and D2, the minimum vertical reinforcement shall be one \#5 at 18 inches on center or one \#4 bar at 12 inches on center, and the minimum horizontal reinforcement shall be one \#5 bar at 16 inches on center.
13. Horizontal reinforcement shall be continuous around building corners using corner bars or by bending the bars. The minimum lap splice shall be 24 inches. For townhouses in Seismic Design Categories D0, D1, and D2, each end of all horizontal reinforcement shall terminate with a standard hook or lap splice.
14. For openings provide one \#4 horizontal bar within 12 inches from the bottom of the opening to extend minimum 24 inches beyond opening. In locations with wind speeds greater than or equal to 110 mph or in Seismic Design Categories A and B, provide one \#4 bar for the full height of the wall story within 12 inches each side of the opening. In locations with wind speeds greater than 110 mph , townhouses in Seismic Design Categories D0, D1, and D2, provide two \#4 bars or one \#5 bar for full height of the wall story within 12 inches of each side of the opening.
15. Where design wind pressure exceeds 40 psf or for townhouses in Seismic Design Category C, and all buildings in Seismic Design Categories D0, D1 and D2, the vertical wall reinforcement in the top-most ICF story shall terminate with a 90-degree standard hook in accordance with IRC 2006, Section R611.7.1.5. The free end of the hook shall be within 4 inches of the top of the wall and shall be oriented parallel to the horizontal steel in the top of the wall.
16. Carefully consider floor/wall connection details for lateral loads, especially with higher backfills, walkout basements, and active seismic areas.
17. Use Table R611.3(1) to determine wind loads in Table 3A.

Table R611.3(1) is based on ultimate design wind speeds, $\mathrm{V}_{\text {ult }}$. Where documents are based only on nominal design wind speeds, $\mathrm{V}_{\text {asd }}$, use Table R301.2.1.3 to convert nominal design wind speeds to ultimate design wind speeds, $\mathrm{V}_{\text {ult }}$, before using Table R611.3(1).
18. For larger wind speeds greater than 150 mph see Table 3B.

TABLE R301.2.1.3
WIND SPEED CONVERSIONS ${ }^{\text {a }}$

| $V_{\text {wit }}$ | 110 | 115 | 120 | 130 | 140 | 150 | 160 | 170 | 180 | 190 | 200 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $V_{a c d}$ | 85 | 89 | 93 | 101 | 108 | 116 | 124 | 132 | 139 | 147 | 155 |

For SI: 1 mile per hour $=0.447 \mathrm{~m} / \mathrm{s}$.
a. Linear interpolation is permitted.

TABLE R611.3(1)
DESIGN WIND PRESSURE FOR USE WITH TABLES R611.3(2), R611.4(1), AND R611.5 FOR ABOVE GRADE WALLS ${ }^{\text {a }}$

| $\underset{(\mathrm{mph})^{6}}{\text { WIND SPEED }}$ | DESIGN WIND PRESSURE (psf) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Enclosed ${ }^{\text {b }}$ |  |  | Partially Enclosed ${ }^{\text {b }}$ |  |  |
|  | Exposure ${ }^{\text {c }}$ |  |  | Exposure ${ }^{\text {e }}$ |  |  |
|  | B | c | D | B | c | D |
| 85 | 18 | 24 | 29 | 23 | 31 | 37 |
| 90 | 20 | 27 | 32 | 25 | 35 | 41 |
| 100 | 24 | 34 | 39 | 31 | 43 | 51 |
| 110 | 29 | 41 | 48 | 38 | 52 | 61 |
| 120 | 35 | 48 | 57 | 45 | 62 | 73 |
| 130 | 41 | 56 | 66 | 53 | 73 | $85^{\text {d }}$ |
| 140 | 47 | 65 | 77 | 61 | $84^{\text {d }}$ | $99^{\text {d }}$ |
| 150 | 54 | 75 | $88{ }^{\text {d }}$ | 70 | $96^{\text {d }}$ | $114{ }^{\text {d }}$ |

For SI: 1 pound per square foot $=0.0479 \mathrm{kPa} ; 1$ mile per hour $=0.447 \mathrm{~m} / \mathrm{s} ; 1$ foot $=304.8 \mathrm{~mm} ; I$ square foot $=0.0929 \mathrm{n}^{2}$.
a. This table is based on ASCE 7-98 components and cladding wind pressures using a mean roof height of 35 ft and a tribitary area of $10 \mathrm{ft}^{2}$.
b. Buildings in wind-borne debris regions as defined in Section R202 shall be considered as "Partially Enclosed" unless glazed openings are protected in accordance with Section R301.2.1.2, in which case the building shall be considered as "Enclosed." All other buildings shall be classified as "Enclosed."
c. Exposure Categories shall be determined in accordance with Section R301.2.1.4.
d. For wind pressures greater than 80 psf, design is required in accordance with ACI 318 and approved manufacturer guidelines.
e. Interpolation is permitted between wind speeds.

Note: Logix recommends Builiders, owners and/or designers using these tables confirm that on-site building conditions are $w /$ in the scope of the tables being used.

| Ground Floor LOGIX Supporting Roof only |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4" Logix |  |  |  |  |  | 6.25" Logix |  |  |  |  |  | 8" Logix |  |  |  |  |  | 10" Logix |  |  |  |  |  | 12" Logix |  |  |  |  |  |
|  | Unfactored Wind Load (psf) |  |  |  |  |  | Unfactored Wind Load (psf) |  |  |  |  |  | Unfactored Wind Load (psf) |  |  |  |  |  | Unfactored Wind Load (psf) |  |  |  |  |  | Unfactored Wind Load (psf) |  |  |  |  |  |
|  | 20 | 40 | 60 | 80 | 90 | 114 | 20 | 40 | 60 | 80 | 90 | 114 | 20 | 40 | 60 | 80 | 90 | 114 | 20 | 40 | 60 | 80 | 90 | 114 | 20 | 40 | 60 | 80 | 90 | 114 |
| 8 | 48 | 24 | 16 | 12 | 8 | 8 | 48 | 42 | 24 | 16 | 16 | 12 | 48 | 48 | 32 | 24 | 16 | 16 | 48 | 48 | 40 | 24 | 24 | 16 | 48 | 48 | 48 | 32 | 32 | 24 |
| 9 | 48 | 16 | 12 | 8 | 8 | 6 | 48 | 32 | 16 | 12 | 12 | 8 | 48 | 40 | 24 | 16 | 16 | 12 | 48 | 48 | 32 | 16 | 16 | 16 | 48 | 48 | 32 | 24 | 24 | 16 |
| 10 | 32 | 16 | 8 | 6 | 6 |  | 48 | 24 | 16 | 8 | 8 | 8 | 48 | 32 | 16 | 12 | 12 | 8 | 48 | 40 | 24 | 16 | 16 | 12 | 48 | 48 | 24 | 16 | 16 | 12 |
| 12 | 16 | 8 | 6 |  |  |  | 32 | 16 | 8 | 6 | 6 |  | 40 | 16 | 12 | 8 | 8 | 6 | 48 | 24 | 16 | 12 | 8 | 8 | 48 | 32 | 16 | 12 | 12 | 8 |
| 14 | 16 | 6 |  |  |  |  | 24 | 12 | 6 |  |  |  | 32 | 12 | 8 | 6 | 6 |  | 40 | 16 | 12 | 8 | 8 | 6 | 48 | 16 | 12 | 8 | 8 | 6 |
| 16 | 8 |  |  |  |  |  | 16 | 8 |  |  |  |  | 24 | 8 | 6 |  |  |  | 24 | 12 | 8 | 6 | 6 |  | 32 | 16 | 8 | 8 | 6 |  |
| 18 | 8 |  |  |  |  |  | 12 | 6 |  |  |  |  | 16 | 8 |  |  |  |  | 16 | 8 | 6 |  |  |  | 24 | 12 | 8 | 6 |  |  |
| 20 | 6 |  |  |  |  |  | 8 |  |  |  |  |  | 12 | 6 |  |  |  |  | 16 | 8 |  |  |  |  | 16 | 8 | 6 |  |  |  |


| Ground Floor LOGIX Supporting 2nd Storey Wood Frame \& Roof Structure |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Height of Basemen t Wall, ft | 4" Logix |  |  |  |  |  | 6.25" Logix |  |  |  |  |  | 8" Logix |  |  |  |  |  | 10" Logix |  |  |  |  |  | 12" Logix |  |  |  |  |  |
|  | Unfactored Wind Load (psf) |  |  |  |  |  | Unfactored Wind Load (psf) |  |  |  |  |  | Unfactored Wind Load (psf) |  |  |  |  |  | Unfactored Wind Load (psf) |  |  |  |  |  | Unfactored Wind Load (psf) |  |  |  |  |  |
|  | 20 | 40 | 60 | 80 | 90 | 114 | 20 | 40 | 60 | 80 | 90 | 114 | 20 | 40 | 60 | 80 | 90 | 114 | 20 | 40 | 60 | 80 | 90 | 114 | 20 | 40 | 60 | 80 | 90 | 114 |
| 8 | 48 | 24 | 16 | 12 | 8 | 8 | 48 | 40 | 24 | 16 | 16 | 12 | 48 | 48 | 32 | 24 | 16 | 16 | 48 | 48 | 40 | 32 | 24 | 16 | 48 | 48 | 48 | 32 | 32 | 24 |
| 9 | 48 | 16 | 12 | 8 | 8 | 6 | 48 | 32 | 16 | 12 | 12 | 8 | 48 | 40 | 24 | 16 | 16 | 12 | 48 | 48 | 32 | 24 | 16 | 16 | 48 | 48 | 40 | 24 | 24 | 16 |
| 10 | 32 | 16 | 8 | 6 | 6 |  | 48 | 24 | 16 | 8 | 8 | 8 | 48 | 32 | 16 | 12 | 12 | 8 | 48 | 40 | 24 | 16 | 16 | 12 | 48 | 48 | 12 | 16 | 16 | 16 |
| 12 | 24 | 8 | 6 |  |  |  | 32 | 16 | 8 | 8 | 6 |  | 48 | 16 | 12 | 8 | 8 | 6 | 48 | 24 | 16 | 12 | 8 | 8 | 48 | 32 | 12 | 12 | 12 | 8 |
| 14 | 16 | 6 |  |  |  |  | 24 | 12 | 6 |  |  |  | 32 | 12 | 8 | 6 | 6 |  | 40 | 16 | 12 | 8 | 8 | 6 | 48 | 16 | 12 | 8 | 8 | 6 |
| 16 | 12 |  |  |  |  |  | 16 | 8 |  |  |  |  | 24 | 8 | 6 |  |  |  | 24 | 12 | 8 | 6 | 6 |  | 32 | 16 | 8 | 8 | 6 |  |
| 18 | 8 |  |  |  |  |  | 12 | 6 |  |  |  |  | 16 | 8 |  |  |  |  | 24 | 8 | 6 |  |  |  | 24 | 12 | 8 | 6 |  |  |
| 20 | 6 |  |  |  |  |  | 6 |  |  |  |  |  | 12 | 6 |  |  |  |  | 16 | 6 | 6 |  |  |  | 16 | 8 | 6 |  |  |  |


| Ground Floor LOGIX Supporting 2nd Storey LOGIX \& Roof Structure |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Height of Basemen t Wall, ft | 4" Logix |  |  |  |  |  | 6.25" Logix |  |  |  |  |  | 8" Logix |  |  |  |  |  | 10" Logix |  |  |  |  |  | 12" Logix |  |  |  |  |  |
|  | Unfactored Wind Load (psf) |  |  |  |  |  | Unfactored Wind Load (psf) |  |  |  |  |  | Unfactored Wind Load (psf) |  |  |  |  |  | Unfactored Wind Load (psf) |  |  |  |  |  | Unfactored Wind Load (psf) |  |  |  |  |  |
|  | 20 | 40 | 60 | 80 | 90 | 114 | 20 | 40 | 60 | 80 | 90 | 114 | 20 | 40 | 60 | 80 | 90 | 114 | 20 | 40 | 60 | 80 | 90 | 114 | 20 | 40 | 60 | 80 | 90 | 114 |
| 8 | 48 | 24 | 16 | 12 | 12 | 8 | 48 | 40 | 24 | 16 | 16 | 12 | 48 | 48 | 32 | 24 | 16 | 16 | 48 | 48 | 40 | 32 | 24 | 16 | 48 | 48 | 48 | 32 | 32 | 24 |
| 9 | 48 | 16 | 12 | 8 | 8 | 6 | 48 | 32 | 16 | 12 | 12 | 8 | 48 | 40 | 24 | 16 | 16 | 12 | 48 | 48 | 32 | 24 | 16 | 16 | 48 | 48 | 40 | 24 | 24 | 16 |
| 10 | 40 | 16 | 8 | 6 | 6 |  | 48 | 24 | 16 | 12 | 8 | 8 | 48 | 32 | 16 | 12 | 12 | 8 | 48 | 40 | 24 | 16 | 16 | 12 | 48 | 48 | 32 | 16 | 16 | 16 |
| 12 | 24 | 8 | 6 |  |  |  | 32 | 16 | 8 | 8 | 6 |  | 48 | 16 | 12 | 8 | 8 | 6 | 48 | 24 | 16 | 12 | 8 | 8 | 48 | 32 | 16 | 12 | 12 | 8 |
| 14 | 16 | 6 |  |  |  |  | 24 | 12 | 6 |  |  |  | 32 | 12 | 8 | 6 | 6 |  | 42 | 16 | 12 | 8 | 8 | 6 | 48 | 16 | 12 | 8 | 8 | 6 |
| 16 | 12 |  |  |  |  |  | 16 | 8 |  |  |  |  | 24 | 8 | 6 |  |  |  | 24 | 12 | 8 | 6 | 6 |  | 32 | 16 | 8 | 8 | 6 |  |
| 18 | 8 |  |  |  |  |  | 12 | 6 |  |  |  |  | 16 | 8 |  |  |  |  | 24 | 8 | 6 |  |  |  | 24 | 12 | 8 | 6 |  |  |
| 20 | 6 |  |  |  |  |  | 8 |  |  |  |  |  | 12 | 6 |  |  |  |  | 16 | 8 |  |  |  |  | 16 | 8 | 6 |  |  |  |

Notes:

1. Table 3A must be used in conjuction with the notes listed under "Notes for Above - Grade Wall Tables".
2. Vertical bar spacing is for \#4 rebar. \#5 rebar can be substituted provided the spacing is multiplied by 1.5 . Spacing shall be no more than 48 inches on center
3. Steel yield strength $=40 \mathrm{ksi}, 28$ day concrete comprehensive strenght $=3 \mathrm{ksi}$.
4. Where cells show "- ", or are blank, engineering is required.
（WIND SPEEDS GREATER THAN 150 MPH）

Note：Logix recommends Builiders，owners and／or designers using these tables confirm that on－site building conditions are w／in the scope of the tables being used．

| Ground Floor LOGIX Supporting Roof only |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Height of Basement Wall，ft | 4＂Logix |  |  |  | 6．25＂Logix |  |  |  | 8＂Logix |  |  |  | 10＂Logix |  |  |  | 12＂Logix |  |  |  |
|  | Wind Speed（mph） |  |  |  | Wind Speed（mph） |  |  |  | Wind Speed（mph） |  |  |  | Wind Speed（mph） |  |  |  | Wind Speed（mph） |  |  |  |
|  | 200 | 250 | 275 | 300 | 200 | 250 | 275 | 300 | 200 | 250 | 275 | 300 | 200 | 250 | 275 | 300 | 200 | 250 | 275 | 300 |
| 8 | 12 | 8 | 6 |  | 16 | 12 | 8 | 8 | 24 | 16 | 12 | 8 | 32 | 16 | 16 | 12 | 42 | 24 | 16 | 16 |
| 9 | 8 | 6 |  |  | 16 | 8 | 8 | 6 | 16 | 12 | 8 | 8 | 24 | 16 | 12 | 8 | 32 | 16 | 16 | 12 |
| 10 | 8 |  |  |  | 12 | 8 | 6 |  | 16 | 8 | 8 | 6 | 16 | 12 | 8 | 8 | 24 | 16 | 12 | 8 |
| 12 |  |  |  |  | 8 |  |  |  | 8 | 6 | 6 |  | 12 | 8 | 6 | 6 | 16 | 8 | 8 | 6 |
| 14 |  |  |  |  | 6 |  |  |  | 8 |  |  |  | 8 | 6 |  |  | 12 | 8 | 6 |  |
| 16 |  |  |  |  |  |  |  |  | 6 |  |  |  | 8 |  |  |  | 8 | 6 |  |  |
| 18 |  |  |  |  |  |  |  |  |  |  |  |  | 6 |  |  |  | 6 |  |  |  |
| 20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6 |  |  |  |

Ground Floor LOGIX Supporting 2nd Storey LOGIX（or 2nd Storey Wood Frame）\＆Roof Structure

| Height of Basement Wall，ft | 4＂Logix |  |  |  | 6．25＂Logix |  |  |  | 8＂Logix |  |  |  | 10＂Logix |  |  |  | 12＂Logix |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Wind Speed（mph） |  |  |  | Wind Speed（mph） |  |  |  | Wind Speed（mph） |  |  |  | Wind Speed（mph） |  |  |  | Wind Speed（mph） |  |  |  |
|  | 200 | 250 | 275 | 300 | 200 | 250 | 275 | 300 | 200 | 250 | 275 | 300 | 200 | 250 | 275 | 300 | 200 | 250 | 275 | 300 |
| 8 | 12 | 8 | 6 |  | 16 | 12 | 8 | 8 | 24 | 16 | 12 | 12 | 32 | 16 | 16 | 12 | 42 | 24 | 16 | 16 |
| 9 | 8 | 6 |  |  | 16 | 8 | 8 | 6 | 16 | 12 | 8 | 8 | 24 | 16 | 12 | 12 | 32 | 16 | 16 | 12 |
| 10 | 8 |  |  |  | 12 | 8 | 6 |  | 16 | 8 | 8 | 6 | 16 | 12 | 8 | 8 | 24 | 16 | 12 | 8 |
| 12 |  |  |  |  | 8 |  |  |  | 12 | 6 | 6 |  | 12 | 8 | 6 | 6 | 16 | 8 | 8 | 6 |
| 14 |  |  |  |  | 6 |  |  |  | 8 |  |  |  | 8 | 6 |  |  | 12 | 8 | 6 |  |
| 16 |  |  |  |  |  |  |  |  | 6 |  |  |  | 8 |  |  |  | 8 | 6 |  |  |
| 18 |  |  |  |  |  |  |  |  |  |  |  |  | 6 |  |  |  | 6 |  |  |  |
| 20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6 |  |  |  |

Notes：
1．Table 3B must be used in conjuction with the notes listed under＂Notes for Above－Grade Wall Tables＂．
2．Vertical bar spacing is for \＃4 rebar．\＃5 rebar can be substituted provided the spacing is multiplied by 1.5 ．Spacing shall be no more than 48 inches on center
3．Steel yield strength $=60 \mathrm{ksi}, 28$ day concrete comprehensive strenght $=3 \mathrm{ksi}$ ．
4．Where cells show＂－＂，or are blank，engineering is required．


Fig 4
Lintel reinforcement
The lintel tables cover a wide range of uniform and concentrated load conditions, and span lengths. The depth of the lintels range from 8 inch to 30 inches. Uniform and concentrated loading are considered to be concentric and centered on the lintel. Uniform loads act along the entire lintel span, such as from roof trusses at 2 ft spacing. Concentrated load lintel tables consider only a single concentrated load acting anywhere along the lintel span. In addition, the lintel tables do not consider uniform and concentrated loads to act simultaneously on the lintel.
The following notes are common to both uniform and concentrated load lintel tables:

1. 28 day concrete compressive strength $=3 \mathrm{ksi}$. Steel yield strength $=40 \mathrm{ksi}$.
2. Stirrups are D9.5 wire or \#3 bars, bent as shown, and conforming to ACI 318
3. Shaded areas of the lintel tables require reinforcement, except for length $Z$.
4. Dimension $D$ is to the concrete surface, not counting bucks or top plate.
5. Bottom steel must extend a min. 2 ft beyond opening, and no splices are permitted.
6. Deflection is limited to $\mathrm{L} / 360$, not considering long term effects. Long term deflection could be twice the short term depending on the nature of the load.
7. Seismic and wind loads are not considered.
8. Shear planes are not interrupted by embedded joists.
9. Top of lintel is assumed to be laterally restrained.

These tables should only be used if the above conditions are met. For other conditions, consult a structural engineer.

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| s=3", D=8" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Opening } \\ & \mathrm{ft} \end{aligned}$ | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  | 1 - \#6 |
| 5 |  |  |  | 1-\#6 | - | - |
| 6 |  |  | 1-\#6 | - | - | - |
| 7 |  | 1-\#6 | - | - | - | - |
| 8 |  | - | - | - | - | - |
| 9 | 1-\#6 | - | - | - | - | - |
| 10 | - | - | - | - | - | - |
| 12 | - | - | - | - | - | - |
| 14 | - | - | - | - | - | - |
| 16 | - | - | - | - | - | - |
| 18 | - | - | - | - | - | - |
| 20 | - | - | - | - | - | - |
| $\begin{array}{\|l\|} \hline \text { No Stirrup } \\ \text { distance, } Z \text { (in) } \\ \hline \end{array}$ | 28 | 14 | 9 | 7 | 5 | 4 |


| s=4", D=10" <br> Opening <br> ft <br>  <br>  <br>  <br> $\mathbf{3}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{4 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{1 2 0 0}$ | $\mathbf{1 6 0 0}$ | $\mathbf{2 0 0 0}$ | $\mathbf{2 4 0 0}$ |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  | $1-\# 6$ |
| $\mathbf{7}$ |  |  | $1-\# 6$ | - | - | - |
| $\mathbf{8}$ |  | $1-\# 6$ | - | - | - | - |
| $\mathbf{9}$ |  | $1-\# 6$ | - | - | - | - |
| $\mathbf{1 0}$ |  | - | - | - | - | - |
| $\mathbf{1 2}$ | - | - | - | - | - | - |
| $\mathbf{1 4}$ | - | - | - | - | - | - |
| $\mathbf{1 6}$ | - | - | - | - | - | - |
| $\mathbf{1 8}$ | - | - | - | - | - | - |
| $\mathbf{2 0}$ | - | - | - | - | - | - |
| No Stirrup <br> distance,Z (in) | $\mathbf{3 8}$ | $\mathbf{1 9}$ | $\mathbf{1 2}$ | $\mathbf{9}$ | $\mathbf{7}$ | $\mathbf{6}$ |


| s=5", D=12" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | $\mathbf{4 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{1 2 0 0}$ | $\mathbf{1 6 0 0}$ | $\mathbf{2 0 0 0}$ | $\mathbf{2 4 0 0}$ |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  | $1-\# 6$ | $1-\# 6$ |
| $\mathbf{7}$ |  |  |  | $1-\# 6$ | - | - |
| $\mathbf{8}$ |  |  | $1-\# 6$ | - | - | - |
| $\mathbf{9}$ |  | $1-\# 6$ | - | - | - | - |
| $\mathbf{1 0}$ |  | $1-\# 6$ | - | - | - | - |
| $\mathbf{1 2}$ |  | - | - | - | - | - |
| $\mathbf{1 4}$ | $1-\# 6$ | - | - | - | - | - |
| $\mathbf{1 6}$ | - | - | - | - | - | - |
| $\mathbf{1 8}$ | - | - | - | - | - | - |
| $\mathbf{2 0}$ | - | - | - | - | - | - |
| No Stirup <br> distance,Z (in) | $\mathbf{4 8}$ | $\mathbf{2 4}$ | $\mathbf{1 6}$ | $\mathbf{1 2}$ | $\mathbf{9}$ | $\mathbf{8}$ |


| s=7", D=16" |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | Factored Uniform Load, lb/ft |  |  |  |  |  |  |
|  | $\mathbf{4 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{1 2 0 0}$ | $\mathbf{1 6 0 0}$ | $\mathbf{2 0 0 0}$ | $\mathbf{2 4 0 0}$ |  |
| $\mathbf{3}$ |  |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  | $1-\# 6$ | $1-\# 6$ |  |
| $\mathbf{8}$ |  |  |  | $1-\# 6$ | $1-\# 6$ | - |  |
| $\mathbf{9}$ |  |  | $1-\# 6$ | - | - | - |  |
| $\mathbf{1 0}$ |  |  | $1-\# 6$ | - | - | - |  |
| $\mathbf{1 2}$ |  | $1-\# 6$ | - | - | - | - |  |
| $\mathbf{1 4}$ |  | - | - | - | - | - |  |
| $\mathbf{1 6}$ | $1-\# 6$ | - | - | - | - | - |  |
| $\mathbf{1 8}$ | - | - | - | - | - | - |  |
| $\mathbf{2 0}$ | - | - | - | - | - | - |  |
| No Stirrup distance,Z (in) | $\mathbf{3 3}$ | $\mathbf{2 2}$ | $\mathbf{1 6}$ | $\mathbf{1 3}$ | $\mathbf{1 1}$ |  |  |

## Notes:

1. Where not shown otherwise, bottom steel is 1-\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain "-" the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrups. For stirrup information refer to Figure 4.
5. Factored Uniform Load includes 1.2, and 1.6 for dead and live load, respectively. For example, (1.2*dead load)+(1.6*live load).
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.

| s=9", D=20" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Opening } \\ & \mathrm{ft} \end{aligned}$ | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |
| 8 |  |  |  |  | 1-\#6 | 1-\#6 |
| 9 |  |  |  | 1-\#6 | 1-\#6 | - |
| 10 |  |  | 1-\#6 | 1-\#6 | - | - |
| 12 |  | 1-\#6 | - | - | - | - |
| 14 |  | - | - | - | - | - |
| 16 | 1-\#6 | - | - | - | - | - |
| 18 | 1-\#6 | - | - | - | - | - |
| 20 | - | - | - | - | - | - |
| No Stirrup distance, Z (in) |  |  | 29 | 21 | 17 | 14 |
|  |  |  |  |  |  |  |
| s=14", D=30" |  |  |  |  |  |  |
| Opening ft | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |
| 9 |  |  |  |  |  | 1-\#6 |
| 10 |  |  |  |  | 1-\#6 | 1-\#6 |
| 12 |  |  |  | 1-\#6 | - | - |
| 14 |  |  | 1-\#6 | - | - | - |
| 16 |  | 1-\#6 | - | - | - | - |
| 18 |  | - | - | - | - | - |
| 20 | 1-\#6 | - | - | - | - | - |
| No Stirrup distance, Z (in) |  |  | 45 | 34 | 27 | 22 |

Notes:

1. Where not shown otherwise, bottom steel is 1-\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain "-" the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrups. For stirrup information refer to Figure 4.
5. Factored Uniform Load includes 1.2 , and 1.6 for dead and live load, respectively. For example, (1.2*dead load)+(1.6*live load).
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

 TABLE 4B - LOGIX 6.25" LINTEL REINFORCEMENT WITH UNIFORM LOAD| s=3", D=8" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Opening } \\ \mathrm{ft} \end{gathered}$ | Factored Uniform Load, lb/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  | 1-\#6 |
| 5 |  |  |  | 1 - \#6 | 1 - \#6 | 2 - \#5 |
| 6 |  |  | 1-\#6 | 2 - \#5 | - | - |
| 7 |  | 1-\#6 | 2-\#5 | - | - | - |
| 8 |  | 2-\#5 | - | - | - | - |
| 9 |  | - | - | - | - | - |
| 10 | 2 - \#5 | - | - | - | - | - |
| 12 | - | - | - | - | - | - |
| 14 | - | - | - | - | - | - |
| 16 | - | - | - | - | - | - |
| 18 | - | - | - | - | - | - |
| 20 | - | - | - | - | - | - |
| $\begin{aligned} & \hline \text { No stirrup } \\ & \text { distance, } Z \text { (in.) } \end{aligned}$ | 44 | 22 | 14 | 11 | 8 | 7 |
|  |  |  |  |  |  |  |
| s=5", D=12" |  |  |  |  |  |  |
| $\begin{aligned} & \text { Opening } \\ & \mathrm{ft} \end{aligned}$ | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |
| 6 |  |  |  |  | 1-\#6 | 1 - \#6 |
| 7 |  |  |  | 1-\#6 | 2-\#5 | 2-\#5 |
| 8 |  |  | 1-\#6 | 2-\#5 | 2-\#6 | 2 - \#6 |
| 9 |  | 1-\#6 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#7 |
| 10 |  | 1-\#6 | 2-\#5 | 2-\#6 | 2-\#7 | - |
| 12 | 1-\#6 | 2-\#5 | 2-\#7 | - | - | - |
| 14 | 2-\#5 | 2 -\#7 | - | - | - | - |
| 16 | 2 - \#6 | - | - | - | - | - |
| 18 | 2 - \#7 | - | - | - | - | - |
| 20 | - | - | - | - | - | - |
| No stirrup distance, $Z$ (in.) | 75 | 37 | 25 | 18 | 15 | 12 |


| s=4", D=10" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Opening } \\ \mathrm{ft} \end{gathered}$ | Factored Uniform Load, lb/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |
| 5 |  |  |  |  |  | 1 - \#6 |
| 6 |  |  |  | 1 - \#6 | 2-\#5 | 2-\#5 |
| 7 |  |  | 1 - \#6 | 2-\#5 | 2-\#6 | 2-\#6 |
| 8 |  | 1-\#6 | 2-\#5 | 2 - \#6 | 2-\#7 | - |
| 9 |  | 1 - \#6 | 2-\#6 | - | - | - |
| 10 |  | 2 - \#5 | 2-\#6 | - | - | - |
| 12 | 1-\#6 | - | - | - | - | - |
| 14 | 2-\#6 | - | $\cdot$ | - | - | - |
| 16 | - | - | - | - | - | - |
| 18 | - | $\cdot$ | $\cdot$ | $\cdot$ | - | - |
| 20 | - | - | - | - | - | - |
| $\begin{array}{\|l\|} \hline \begin{array}{l} \text { No stirrup } \\ \text { distance, } \mathrm{Z} \text { (in.) } \end{array} \\ \hline \end{array}$ | 59 | 29 | 19 | 14 | 11 | 9 |

Notes:

1. Where not shown otherwise, bottom steel is 1-\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain "-" the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrups. For stirrup information refer to Figure 4.
5. Factored Uniform Load includes 1.2 , and 1.6 for dead and live load, respectively. For example, (1.2*dead load)+(1.6*live load).
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.

LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS
TABLE 4B - LOGIX 6.25" LINTEL REINFORCEMENT WITH UNIFORM LOAD cont'd

| Opening <br> $\mathbf{f t}$ |  |  |  |  |  |  |  | Factored Uniform Load, Ib/ft |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{4 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{1 2 0 0}$ | $\mathbf{1 6 0 0}$ | $\mathbf{2 0 0 0}$ | $\mathbf{2 4 0 0}$ |  |  |  |  |  |  |  |
| $\mathbf{3}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{8}$ |  |  |  |  | $1-\# 6$ | $1-\# 6$ |  |  |  |  |  |  |  |
| $\mathbf{9}$ |  |  |  | $1-\# 6$ | $1-\# 6$ | $2-\# 5$ |  |  |  |  |  |  |  |
| $\mathbf{1 0}$ |  |  | $1-\# 6$ | $1-\# 6$ | $2-\# 5$ | $2-\# 6$ |  |  |  |  |  |  |  |
| $\mathbf{1 2}$ |  | $1-\# 6$ | $2-\# 5$ | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ |  |  |  |  |  |  |  |
| $\mathbf{1 4}$ |  | $2-\# 5$ | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ |  |  |  |  |  |  |  |
| $\mathbf{1 6}$ | $1-\# 6$ | $2-\# 5$ | $2-\# 7$ | $2-\# 7$ | $2-\# 8$ | - |  |  |  |  |  |  |  |
| $\mathbf{1 8}$ | $2-\# 5$ | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ | - | - |  |  |  |  |  |  |  |
| $\mathbf{2 0}$ | $2-\# 5$ | $2-\# 7$ | $2-\# 8$ | - | - | - |  |  |  |  |  |  |  |
| No stirrup <br> distance, $\mathbf{Z}$ (in.) |  | $\mathbf{6 8}$ | $\mathbf{4 5}$ | $\mathbf{3 4}$ | $\mathbf{2 7}$ | $\mathbf{2 2}$ |  |  |  |  |  |  |  |


| s=11", D=24" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Opening } \\ \mathrm{ft} \end{gathered}$ | Factored Uniform Load, lb/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |
| 8 |  |  |  |  |  | 1-\#6 |
| 9 |  |  |  |  | 1-\#6 | 1-\#6 |
| 10 |  |  |  | 1-\#6 | 1-\#6 | 2-\#5 |
| 12 |  |  | 1-\#6 | 2-\#5 | 2 - \#6 | 2-\#6 |
| 14 |  | 1-\#6 | 2-\#5 | 2 - \#6 | 2-\#6 | 2-\#7 |
| 16 |  | 2-\#5 | 2-\#6 | 2 - \#7 | 2-\#7 | 2 - \#8 |
| 18 | 1-\#6 | 2-\#6 | 2-\#7 | 2-\#8 | 2 - \#8 | - |
| 20 | 2-\#5 | 2 - \#6 | 2 - \#7 | 2 - \#8 | - | - |
| No stirrup distance, Z (in.) |  | 83 | 55 | 41 | 33 | 27 |


| s=14", D=30" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | $\mathbf{4 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{1 2 0 0}$ | $\mathbf{1 6 0 0}$ | $\mathbf{2 0 0 0}$ | $\mathbf{2 4 0 0}$ |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  |  |  |
| $\mathbf{8}$ |  |  |  |  |  |  |
| $\mathbf{9}$ |  |  |  |  |  | $1-\# 6$ |
| $\mathbf{1 0}$ |  |  |  |  | $1-\# 6$ | $1-\# 6$ |
| $\mathbf{1 2}$ |  |  | $1-\# 6$ | $1-\# 6$ | $2-\# 5$ | $2-\# 5$ |
| $\mathbf{1 4}$ |  | $1-\# 6$ | $1-\# 6$ | $2-\# 5$ | $2-\# 6$ | $2-\# 6$ |
| $\mathbf{1 6}$ |  | $1-\# 6$ | $2-\# 5$ | $2-\# 6$ | $2-\# 7$ | $2-\# 7$ |
| $\mathbf{1 8}$ | $1-\# 6$ | $2-\# 5$ | $2-\# 6$ | $2-\# 7$ | $2-\# 7$ | $2-\# 8$ |
| $\mathbf{2 0}$ | $1-\# 6$ | $2-\# 6$ | $2-\# 7$ | $2-\# 7$ | $2-\# 8$ | - |
| No stirrup <br> distance, $\mathbf{Z}$ (in.) |  |  | 71 | 53 | 42 | 35 |

Notes:

1. Where not shown otherwise, bottom steel is 1-\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain "-" the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrups. For stirrup information refer to Figure 4.
5. Factored Uniform Load includes 1.2 , and 1.6 for dead and live load, respectively. For example, (1.2*dead load)+(1.6*live load).
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.

LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS
TABLE 4C - LOGIX 8" LINTEL REINFORCEMENT WITH UNIFORM LOAD

| s=3", D=8" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Opening } \\ & \mathrm{ft} \end{aligned}$ | Factored Uniform Load, lb/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  | 2 -\#5 |
| 5 |  |  |  | 2 -\#5 | 2-\#5 | 2 -\#5 |
| 6 |  |  | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 |
| 7 |  | 2 -\#5 | 2-\#5 | 2 - \#6 | - | - |
| 8 |  | 2-\#5 | 2 - \#6 | - | - | - |
| 9 |  | 2 - \#5 | - | - | - | - |
| 10 | 2-\#5 | - | - | - | - | - |
| 12 | - | - | - | - | - | - |
| 14 | - | - | - | - | - | - |
| 16 | - | - | - | - | - | - |
| 18 | - | - | - | - | - | - |
| 20 | - | - | - | - | - | - |
| No stirrup distance, $Z$ (in.) |  | 28 | 18 | 14 | 11 | 9 |
|  |  |  |  |  |  |  |
| $s=5^{\prime \prime}, \mathrm{D}=12^{\prime \prime}$ |  |  |  |  |  |  |
| $\begin{aligned} & \text { Opening } \\ & \mathrm{ft} \end{aligned}$ | Factored Uniform Load, lb/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |
| 8 |  |  |  |  | 2 - \#6 | 2-\#6 |
| 9 |  |  |  | 2-\#6 | 2 - \#6 | - |
| 10 |  |  | 2-\#6 | 2-\#6 | - | - |
| 12 |  | 2 - \#6 | - | - | - | - |
| 14 | 2-\#5 | 2-\#6 | - | - | - | - |
| 16 | 2-\#6 | - | - | - | - | - |
| 18 | - | - | - | - | - | - |
| 20 | - | - | - | - | - | - |
| $\begin{array}{\|l} \hline \begin{array}{l} \text { No stirrup } \\ \text { distance, } Z \text { (in.) } \end{array} \end{array}$ |  | 48 | 32 | 24 | 19 | 16 |


| s=4", D=10" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  | $2-\# 5$ |
| $\mathbf{6}$ |  |  |  | $2-\# 5$ | $2-\# 5$ | $2-\# 5$ |
| $\mathbf{7}$ |  |  | $2-\# 5$ | $2-\# 5$ | $2-\# 6$ | $2-\# 6$ |
| $\mathbf{8}$ |  |  | $2-\# 5$ | $2-\# 6$ | $2-\# 7$ | - |
| $\mathbf{9}$ |  |  | $2-\# 6$ | $2-\# 6$ | - | - |
| $\mathbf{1 0}$ |  |  | $2-\# 6$ | - | - | - |
| $\mathbf{1 2}$ | $2-\# 5$ | - | - | - | - | - |
| $\mathbf{1 4}$ | $2-\# 6$ | - | - | - | - | - |
| $\mathbf{1 6}$ | - | - | - | - | - | - |
| $\mathbf{1 8}$ | - | - | - | - | - | - |
| $\mathbf{2 0}$ | - | - | - | - | - | - |
| No stirrup <br> distance, $\mathbf{Z}$ (in.) |  | 38 | 25 | 19 | 15 | 12 |


| s=7", D=16" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> $\mathbf{f t}$ | Factored Uniform Load, lb/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | $\mathbf{2 0 0 0}$ | 2400 |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  | $2-\# 5$ | $2-\# 5$ |
| $\mathbf{8}$ |  |  |  | $2-\# 5$ | $2-\# 5$ | $2-\# 5$ |
| $\mathbf{9}$ |  |  |  | $2-\# 5$ | $2-\# 5$ | $2-\# 6$ |
| $\mathbf{1 0}$ |  |  | $2-\# 5$ | $2-\# 5$ | $2-\# 6$ | $2-\# 6$ |
| $\mathbf{1 2}$ |  | $2-\# 5$ | $2-\# 6$ | $2-\# 6$ | - | - |
| $\mathbf{1 4}$ |  | $2-\# 5$ | - | - | - | - |
| $\mathbf{1 6}$ | $2-\# 5$ | $2-\# 6$ | - | - | - | - |
| $\mathbf{1 8}$ | $2-\# 5$ | - | - | - | - | - |
| $\mathbf{2 0}$ | $2-\# 6$ | - | - | - | - | - |
| No stirrup <br> distance, Z (in.) |  | 67 | 45 | 33 | 27 | 22 |

## Notes:

1. Where not shown otherwise, bottom steel is 2-\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain "-" the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrups. For stirrup information refer to Figure 4.
5. Factored Uniform Load includes 1.2, and 1.6 for dead and live load, respectively. For example, (1.2*dead load)+(1.6*live load).
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.

TABLE 4C - LOGIX 8" LINTEL REINFORCEMENT WITH UNIFORM LOAD cont'd

| s=9", D=20" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | FactoredUniform Load, lb/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | $\mathbf{2 0 0 0}$ | 2400 |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  |  |  |
| $\mathbf{8}$ |  |  |  |  | $2-\# 5$ | $2-\# 5$ |
| $\mathbf{9}$ |  |  |  | $2-\# 5$ | $2-\# 5$ | $2-\# 5$ |
| $\mathbf{1 0}$ |  |  |  | $2-\# 5$ | $2-\# 5$ | $2-\# 6$ |
| $\mathbf{1 2}$ |  |  | $2-\# 5$ | $2-\# 6$ | $2-\# 6$ | - |
| $\mathbf{1 4}$ |  | $2-\# 5$ | $2-\# 6$ | - | - | - |
| $\mathbf{1 6}$ |  | $2-\# 6$ | - | - | - | - |
| $\mathbf{1 8}$ | $2-\# 5$ | $2-\# 6$ | - | - | - | - |
| $\mathbf{2 0}$ | $2-\# 5$ | - | - | - | - | - |
| No stirrup <br> distance, Z (in.) |  | 87 | 58 | 43 | 34 | 29 |


| s=11", D=24" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | $\mathbf{2 0 0 0}$ | $\mathbf{2 4 0 0}$ |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  |  |  |
| $\mathbf{8}$ |  |  |  |  |  |  |
| $\mathbf{9}$ |  |  |  |  | $2-\# 5$ | $2-\# 5$ |
| $\mathbf{1 0}$ |  |  |  | $2-\# 5$ | $2-\# 5$ | $2-\# 5$ |
| $\mathbf{1 2}$ |  |  | $2-\# 5$ | $2-\# 5$ | $2-\# 6$ | $2-\# 6$ |
| $\mathbf{1 4}$ |  | $2-\# 5$ | $2-\# 5$ | $2-\# 6$ | - | - |
| $\mathbf{1 6}$ |  | $2-\# 5$ | $2-\# 6$ | - | - | - |
| $\mathbf{1 8}$ |  | $2-\# 6$ | - | - | - | - |
| $\mathbf{2 0}$ | $2-\# 5$ | $2-\# 6$ | - | - | - | - |
| No stirrup <br> distance, Z (in.) |  |  | 71 | 53 | 42 | 35 |


| s=14", D=30" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| $\mathbf{3}$ |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  |  |  |
| $\mathbf{8}$ |  |  |  |  |  |  |
| $\mathbf{9}$ |  |  |  |  |  |  |
| $\mathbf{1 0}$ |  |  |  |  | $2-\# 5$ | $2-\# 5$ |
| $\mathbf{1 2}$ |  |  |  | $2-\# 5$ | $2-\# 5$ | $2-\# 5$ |
| $\mathbf{1 4}$ |  |  | $2-\# 5$ | $2-\# 5$ | $2-\# 6$ | $2-\# 6$ |
| $\mathbf{1 6}$ |  | $2-\# 5$ | $2-\# 5$ | $2-\# 6$ | - | - |
| $\mathbf{1 8}$ |  | $2-\# 5$ | $2-\# 6$ | - | - | - |
| $\mathbf{2 0}$ |  | $2-\# 6$ | - | - | - | - |
| No stirrup <br> distance, $\mathbf{Z}$ (in.) |  |  |  |  | 54 | 45 |

Notes:

1. Where not shown otherwise, bottom steel is 2-\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain "-" the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrups. For stirrup information refer to Figure 4.
5. Factored Uniform Load includes 1.2, and 1.6 for dead and live load, respectively. For example, (1.2*dead load)+(1.6*live load)
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.

LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS TABLE 4D - LOGIX 10" LINTEL REINFORCEMENT WITH UNIFORM LOAD

| Factored Uniform Load, Ib/ft |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft |  |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |
| 6 |  |  |  |  | $2-\# 6$ | $2-\# 6$ |
| 7 |  |  |  | $2-\# 6$ | - | - |
| 8 |  |  | $2-\# 6$ | - | - | - |
| 9 |  |  | - | - | - | - |
| 10 |  | - | - | - | - | - |
| 12 | - | - | - | - | - | - |
| 14 | - | - | - | - | - | - |
| 16 | - | - | - | - | - | - |
| $\mathbf{1 8}$ | - | - | - | - | - | - |
| 20 | - | - | - | - | - | - |
| No stirrup <br> distance, $\mathbf{Z}$ (in.) |  | 35 | 23 | 17 | 14 | 11 |


| Opening <br> ft |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  |  | $2-\# 6$ |
| $\mathbf{8}$ |  |  |  | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ |
| $\mathbf{9}$ |  |  | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ |
| $\mathbf{1 0}$ |  |  | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ | - |
| $\mathbf{1 2}$ |  | $2-\# 7$ | $2-\# 8$ | - | - | - |
| $\mathbf{1 4}$ | $2-\# 6$ | $2-\# 8$ | - | - | - | - |
| $\mathbf{1 6}$ | $2-\# 8$ | - | - | - | - | - |
| $\mathbf{1 8}$ | - | - | - | - | - | - |
| $\mathbf{2 0}$ | - | - | - | - | - | - |
| No stirrup <br> distance, Z (in.) |  | 47 | 31 | 23 | 19 | 15 |


| s=5", D=12" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  |  |  |
| $\mathbf{8}$ |  |  |  |  | $2-\# 6$ | $2-\# 6$ |
| $\mathbf{9}$ |  |  |  | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ |
| $\mathbf{1 0}$ |  |  | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ |
| $\mathbf{1 2}$ |  | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ | $2-\# 8$ | - |
| $\mathbf{1 4}$ |  | $2-\# 7$ | $2-\# 8$ | - | - | - |
| $\mathbf{1 6}$ | $2-\# 6$ | - | - | - | - | - |
| $\mathbf{1 8}$ | $2-\# 7$ | - | - | - | - | - |
| $\mathbf{2 0}$ | - | - | - | - | - | - |
| No stirrup <br> distance, $\mathbf{Z}$ (in.) |  | 60 | 40 | 30 | 24 | 20 |


| s=7", D=16" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | $\mathbf{2 0 0 0}$ | $\mathbf{2 4 0 0}$ |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  |  |  |
| $\mathbf{8}$ |  |  |  |  |  |  |
| $\mathbf{9}$ |  |  |  |  |  | $2-\# 6$ |
| $\mathbf{1 0}$ |  |  |  |  | $2-\# 6$ | $2-\# 6$ |
| $\mathbf{1 2}$ |  |  | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ |
| $\mathbf{1 4}$ |  | $2-\# 6$ | $2-\# 7$ | $2-\# 7$ | $2-\# 8$ | - |
| $\mathbf{1 6}$ |  | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ | - | - |
| $\mathbf{1 8}$ | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ | - | - | - |
| $\mathbf{2 0}$ | $2-\# 6$ | $2-\# 8$ | - | - | - | - |
| No stirrup <br> distance, $\mathbf{Z}$ (in.) |  | 84 | 56 | 42 | 33 | 28 |

## Notes:

1. Where not shown otherwise, bottom steel is 2-\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain "-" the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrups. For stirrup information refer to Figure 4.
5. Factored Uniform Load includes 1.2 , and 1.6 for dead and live load, respectively. For example, ( $1.2 *$ dead load) $+(1.6 *$ live load).
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.

TABLE 4D - LOGIX 10" LINTEL REINFORCEMENT WITH UNIFORM LOAD cont'd

| s=9", D=20" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Opening } \\ \mathrm{ft} \end{gathered}$ | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |
| 9 |  |  |  |  |  |  |
| 10 |  |  |  |  |  | 2 - \#6 |
| 12 |  |  |  | 2 - \#6 | 2 - \#6 | 2-\#7 |
| 14 |  |  | 2 - \#6 | 2-\#7 | 2-\#7 | 2 - \#8 |
| 16 |  | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#8 | - |
| 18 |  | 2-\#6 | 2-\#7 | 2 - \#8 | - | - |
| 20 | 2 - \#6 | 2 - \#7 | 2 - \#8 | - | - | - |
| No stirrup distance, $Z$ (in.) |  | 109 | 72 | 54 | 43 | 36 |


| s=11", D=24" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Opening } \\ \mathrm{ft} \end{gathered}$ | Factored Uniform Load, lb/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |
| 9 |  |  |  |  |  |  |
| 10 |  |  |  |  |  |  |
| 12 |  |  |  |  | 2-\#6 | 2 - \#6 |
| 14 |  |  |  | 2-\#6 | 2-\#7 | 2-\#7 |
| 16 |  |  | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#8 |
| 18 |  | 2 - \#6 | 2-\#7 | 2 - \#8 | 2 - \#8 | - |
| 20 |  | 2-\#7 | 2-\#8 | 2-\#8 | - | - |
| $\begin{array}{\|l} \hline \begin{array}{l} \text { No stirrup } \\ \text { distance, } Z \text { (in.) } \end{array} \end{array}$ |  | 134 | 89 | 67 | 53 | 44 |


| s=14", D=30" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Opening } \\ \mathrm{ft} \end{gathered}$ | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |
| 9 |  |  |  |  |  |  |
| 10 |  |  |  |  |  |  |
| 12 |  |  |  |  |  |  |
| 14 |  |  |  |  | 2 - \#6 | 2 - \#6 |
| 16 |  |  | 2 - \#6 | 2 - \#6 | 2-\#7 | 2-\#7 |
| 18 |  |  | 2-\#6 | 2-\#7 | 2 - \#8 | 2 - \#8 |
| 20 |  | 2-\#6 | 2-\#7 | 2 - \#8 | 2-\#8 | - |
| No stirrup distance, $Z$ (in.) |  |  |  | 85 | 68 | 56 |

Notes:

1. Where not shown otherwise, bottom steel is 2-\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain " - " the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrups. For stirrup information refer to Figure 4.
5. Factored Uniform Load includes 1.2, and 1.6 for dead and live load, respectively. For example, (1.2*dead load)+(1.6*live load).
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.

LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS TABLE 4E - LOGIX 12" LINTEL REINFORCEMENT WITH UNIFORM LOAD

| s=3", D=8" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  | $2-\# 6$ | $2-\# 6$ |
| $\mathbf{7}$ |  |  |  | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ |
| $\mathbf{8}$ |  |  | $2-\# 6$ | $2-\# 7$ | $2-\# 7$ | - |
| $\mathbf{9}$ |  |  | $2-\# 7$ | - | - | - |
| $\mathbf{1 0}$ |  | $2-\# 7$ | - | - | - | - |
| $\mathbf{1 2}$ | $2-\# 6$ | - | - | - | - | - |
| $\mathbf{1 4}$ | - | - | - | - | - | - |
| $\mathbf{1 6}$ | - | - | - | - | - | - |
| $\mathbf{1 8}$ | - | - | - | - | - | - |
| $\mathbf{2 0}$ | - | - | - | - | - | - |
| No stirrup <br> distance, $\mathbf{Z}$ (in.) |  | 42 | 28 | $\mathbf{2 1}$ | 17 | 14 |


| s=5", D=12" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | Factored Uniform Load, lb/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | $\mathbf{2 0 0 0}$ | $\mathbf{2 4 0 0}$ |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  |  |  |
| $\mathbf{8}$ |  |  |  |  | $2-\# 6$ | $2-\# 6$ |
| $\mathbf{9}$ |  |  |  | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ |
| $\mathbf{1 0}$ |  |  | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ |
| $\mathbf{1 2}$ |  | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ | $2-\# 8$ | - |
| $\mathbf{1 4}$ |  | $2-\# 7$ | $2-\# 8$ | - | - | - |
| $\mathbf{1 6}$ | $2-\# 6$ | - | - | - | - | - |
| $\mathbf{1 8}$ | $2-\# 7$ | - | - | - | - | - |
| $\mathbf{2 0}$ | - | - | - | - | - | - |
| No stirrup <br> distance, $\mathbf{Z}$ (in.) |  | 72 | 48 | 36 | $\mathbf{2 8}$ | $\mathbf{2 4}$ |


| s=4", D=10" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | $\mathbf{4 0 0}$ | 800 | 1200 | 1600 | $\mathbf{2 0 0 0}$ | 2400 |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  |  | $2-\# 6$ |
| $\mathbf{8}$ |  |  |  | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ |
| $\mathbf{9}$ |  |  | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ |
| $\mathbf{1 0}$ |  |  | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ | - |
| $\mathbf{1 2}$ |  | $2-\# 6$ | $2-\# 8$ | - | - | - |
| $\mathbf{1 4}$ | $2-\# 6$ | $2-\# 8$ | - | - | - | - |
| $\mathbf{1 6}$ | $2-\# 8$ | - | - | - | - | - |
| $\mathbf{1 8}$ | - | - | - | - | - | - |
| $\mathbf{2 0}$ | - | - | - | - | - | - |
| No stirrup <br> distance, $\mathbf{Z}$ (in.) |  | 57 | 38 | $\mathbf{2 8}$ | $\mathbf{2 2}$ | 19 |


| s=7", D=16" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | $\mathbf{4 0 0}$ | $\mathbf{8 0 0}$ | $\mathbf{1 2 0 0}$ | $\mathbf{1 6 0 0}$ | $\mathbf{2 0 0 0}$ | $\mathbf{2 4 0 0}$ |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  |  |  |
| $\mathbf{8}$ |  |  |  |  |  |  |
| $\mathbf{9}$ |  |  |  |  |  | $2-\# 6$ |
| $\mathbf{1 0}$ |  |  |  |  | $2-\# 6$ | $2-\# 6$ |
| $\mathbf{1 2}$ |  |  | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ |
| $\mathbf{1 4}$ |  | $2-\# 6$ | $2-\# 7$ | $2-\# 7$ | $2-\# 8$ | - |
| $\mathbf{1 6}$ |  | $2-\# 6$ | $2-\# 8$ | - | - | - |
| $\mathbf{1 8}$ | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ | - | - | - |
| $\mathbf{2 0}$ | $2-\# 6$ | $2-\# 8$ | - | - | - | - |
| No stirrup <br> distance, $\mathbf{Z}$ (in.) |  | 101 | 67 | 50 | 40 | 33 |

Notes:

1. Where not shown otherwise, bottom steel is 2-\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain "-" the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrups. For stirrup information refer to Figure 4.
5. Factored Uniform Load includes 1.2 , and 1.6 for dead and live load, respectively. For example, (1.2*dead load)+(1.6*live load).
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.

TABLE 4E - LOGIX 12" LINTEL REINFORCEMENT WITH UNIFORM LOAD cont'd

| s=9", D=20" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  |  |  |
| $\mathbf{8}$ |  |  |  |  |  |  |
| $\mathbf{9}$ |  |  |  |  |  |  |
| $\mathbf{1 0}$ |  |  |  |  |  | $2-\# 6$ |
| $\mathbf{1 2}$ |  |  |  | $2-\# 6$ | $2-\# 6$ | $2-\# 7$ |
| $\mathbf{1 4}$ |  |  | $2-\# 6$ | $2-\# 7$ | $2-\# 7$ | $2-\# 8$ |
| $\mathbf{1 6}$ |  | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ | $2-\# 8$ | - |
| $\mathbf{1 8}$ |  | $2-\# 7$ | $2-\# 8$ | $2-\# 8$ | - | - |
| $\mathbf{2 0}$ | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ | - | - | - |
| No stirup <br> distance, $\mathbf{Z}$ (in.) |  |  | 87 | 65 | 52 | 43 |


| s=11", D=24" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening <br> ft | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| $\mathbf{3}$ |  |  |  |  |  |  |
| $\mathbf{4}$ |  |  |  |  |  |  |
| $\mathbf{5}$ |  |  |  |  |  |  |
| $\mathbf{6}$ |  |  |  |  |  |  |
| $\mathbf{7}$ |  |  |  |  |  |  |
| $\mathbf{8}$ |  |  |  |  |  |  |
| $\mathbf{9}$ |  |  |  |  |  |  |
| $\mathbf{1 0}$ |  |  |  |  |  |  |
| $\mathbf{1 2}$ |  |  |  |  | $2-\# 6$ | $2-\# 6$ |
| $\mathbf{1 4}$ |  |  |  | $2-\# 6$ | $2-\# 7$ | $2-\# 7$ |
| $\mathbf{1 6}$ |  |  | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ | $2-\# 8$ |
| $\mathbf{1 8}$ |  | $2-\# 6$ | $2-\# 7$ | $2-\# 8$ | $2-\# 8$ | - |
| $\mathbf{2 0}$ |  | $2-\# 7$ | $2-\# 8$ | - | - | - |
| No stirrup <br> distance, $\mathbf{Z}$ (in.) |  |  |  | 80 | 64 | 53 |


| D=30" |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Opening } \\ \mathrm{ft} \end{gathered}$ | Factored Uniform Load, Ib/ft |  |  |  |  |  |
|  | 400 | 800 | 1200 | 1600 | 2000 | 2400 |
| 3 |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |
| 9 |  |  |  |  |  |  |
| 10 |  |  |  |  |  |  |
| 12 |  |  |  |  |  | 2 - \#6 |
| 14 |  |  |  | 2 - \#6 | 2-\#6 | 2-\#6 |
| 16 |  |  | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 |
| 18 |  | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#8 | 2 - \#8 |
| 20 |  | 2-\#6 | 2-\#7 | 2 - \#8 | 2 - \#8 | - |
| No stirrup distance, Z (in.) |  |  |  |  | 82 | 68 |

Notes:

1. Where not shown otherwise, bottom steel is 2-\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain "-" the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrups. For stirrup information refer to Figure 4.
5. Factored Uniform Load includes 1.2, and 1.6 for dead and live load, respectively. For example, (1.2*dead load)+(1.6*live load).
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.

| $s=3$ ", D=8" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c\|} \hline \begin{array}{c} \text { Opening } \\ \mathrm{ft} \end{array} \\ \hline \end{array}$ | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | - | - |
| 4 |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - |
| 5 |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - |
| 6 |  |  |  |  |  |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - |
| 7 |  |  |  |  |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - |
| 8 |  |  |  |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - |
| 9 |  |  |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 10 |  |  |  | - | $-$ | - | - | - | - | - | - | - | - | - | - | - | - |
| 12 |  |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 14 |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 16 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 18 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | $-$ |
| 20 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| s=4", D=10" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \begin{array}{c} \text { Opening } \\ \mathrm{ft} \end{array} \\ \hline \end{gathered}$ | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | - | - |
| 5 |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - |
| 6 |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - | - | - |
| 7 |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - |
| 8 |  |  |  |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - |
| 9 |  |  |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - | - |
| 10 |  |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - |
| 12 |  |  |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 14 |  |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 16 |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 18 |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| s=5", D=12" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c\|} \hline \text { Opening } \\ \mathrm{ft} \\ \hline \end{array}$ | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - |
| 6 |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - |
| 7 |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - | - |
| 8 |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - |
| 9 |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - |
| 10 |  |  |  |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - |
| 12 |  |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - |
| 14 |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - |
| 16 |  |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 18 |  |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| s=7", D=16" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Opening } \\ \mathrm{ft} \end{gathered}$ | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1 - \#6 | 1-\#6 |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1 - \#6 | - |
| 8 |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | - | - |
| 9 |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - |
| 10 |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - | - |
| 12 |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - |
| 14 |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - |
| 16 |  |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - |
| 18 |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - |

Build Anything Better. ${ }^{\text {™ }}$

| s=9", D=20" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ft | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 |
| 8 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 |
| 9 |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | - |
| 10 |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - |
| 12 |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - | - |
| 14 |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - |
| 16 |  |  |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - | - |
| 18 |  |  |  |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 |  |  |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - |


| s=11", D=24" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\qquad$ | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 |
| 9 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 |
| 10 |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - |
| 12 |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - |
| 14 |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - | - | - |
| 16 |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - |
| 18 |  |  |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - | - |
| 20 |  |  |  | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - |


| s=14", D=30" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\qquad$ | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 |
| 12 |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - |
| 14 |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - |
| 16 |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - | - |
| 18 |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - |
| 20 |  |  |  |  |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - |

Notes:

1. Where not shown otherwise, bottom steel is 1-\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain " " the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrup. For stirrup information refer to Figure 4.
5. Factored Point Load includes 1.2, and 1.6 for dead and live load, respectively. For example, (1.2*dead load)+(1.6*live load)
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

TABLE 5B - LOGIX 6.25" LINTEL REINFORCEMENT WITH CONCENTRATED LOAD

NOTE: LOGIX recommends builders, owners and/or designers using these tables confirm that on-site building conditions are $\mathbf{w} / \mathrm{in}$ the scope of the tables being used.

| s=3", D=8" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ft | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 2 - \#5 |
| 4 |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | - | - |
| 5 |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | - | - | - | - |
| 6 |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | - | - | - | - | - | - |
| 7 |  |  |  |  |  | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | - | - | - | - | - | - | - | - |
| 8 |  |  |  |  | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | - | - | - | - | - | - | - | - | - |
| 9 |  |  |  | 1-\#6 | 1-\#6 | 2-\#5 | - | - | - | - | - | - | - | - | - | - | - |
| 10 |  |  |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 12 |  |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 14 |  | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 16 |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 18 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| s=4", D=10" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c\|} \hline \text { Opening } \\ \mathrm{ft} \end{array}$ | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 |
| 5 |  |  |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 |
| 6 |  |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2 - \#6 |
| 7 |  |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | - |
| 8 |  |  |  |  |  |  | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | - | - |
| 9 |  |  |  |  |  | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | - | - | - |
| 10 |  |  |  |  | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | - | - | - | - | - |
| 12 |  |  |  | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | - | - | - | - | - | - | - | - |
| 14 |  |  | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#6 | - | - | - | - | - | - | - | - | - | - | - |
| 16 |  | 1-\#6 | 2-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 18 | 1-\#6 | 1-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 | 1-\#6 | 2-\#5 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| s=5", D=12" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Opening | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ft | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1 - \#6 |
| 4 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 |
| 5 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 |
| 6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 |
| 7 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 |
| 8 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 |
| 9 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | - |
| 10 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | - | - |
| 12 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | - | - | - | - |
| 14 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | - | - | - | - | - | - |
| 16 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | - | - | - | - | - | - | - | - | - | - | - |
| 18 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#6 | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - |


| D=16" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ft | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 |
| 4 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 |
| 5 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 |
| 6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 |
| 7 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 |
| 8 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 |
| 9 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 |
| 10 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 |
| 12 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 14 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | - | - |
| 16 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | - | - | - |
| 18 | 1-\#6 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | - | - | - | - | - |
| 20 | 1-\#6 | 1-\#6 | 1-\#6 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | - | - | - | - | - | - | - | - |


| D=20" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ft | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 |
| 4 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 |
| 5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 |
| 6 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 |
| 7 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 |
| 8 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 |
| 9 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 |
| 10 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 |
| 12 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 |
| 14 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 |
| 16 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | - |
| 18 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | - | - |
| 20 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#5 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | - | - | - |


| D=24" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c\|} \hline \text { Opening } \\ \mathrm{ft} \end{array}$ | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3-7 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 8 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 9 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 10 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 12 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 14 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 16 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 18 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 |
| 20 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | - | - |


| D=30" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c} \hline \text { Opening } \\ \mathrm{ft} \end{array}$ | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3-9 | 2-\#6 | 2-\#6 | 2-\#6 | 2 - \#6 | 2-\#6 | 2 - \#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 10 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 12 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 14 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 16 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 18 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 20 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |

Notes:

1. Refer to Notes for Table 5A

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

 TABLE 5C - LOGIX 8" LINTEL REINFORCEMENT WITH CONCENTRATED LOAD| s=3", D=8" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Openin | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| gft | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | - |
| 6 |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | - | - | - |
| 7 |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | - | - | - | - |
| 8 |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | - | - | - | - | - | - |
| 9 |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | - | - | - | - | - | - | - | - |
| 10 |  |  |  |  |  | 2-\#6 | - | - | - | - | - | - | - | - | - | - | - |
| 12 |  |  |  | 2 - \#6 | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 14 |  |  | 2-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 16 |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 18 | 2-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| D=10" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c\|} \hline \text { Openin } \\ \mathrm{g} \\ \hline \end{array}$ | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 |
| 8 |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 |
| 9 |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | - |
| 10 |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | - | - |
| 12 |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | - | - | - | - | - |
| 14 |  |  |  |  |  | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | - | - | - | - | - | - | - | - |
| 16 |  |  |  | 2-\#7 | 2-\#7 | - | - | - | - | - | - | - | - | - | - | - | - |
| 18 |  |  | 2-\#7 | 2-\#7 | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 |  | 2-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| D=12" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Openin g ft | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 |
| 8 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 |
| 9 |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 |
| 10 |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 |
| 12 |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 |
| 14 |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 | - |
| 16 |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 | 2-\#8 | - | - | - | - | - |
| 18 |  |  |  |  | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 | 2-\#8 | - | - | - | - | - | - | - |
| 20 |  |  |  | 2-\#6 | 2-\#7 | 2-\#8 | 2-\#8 | - | - | - | - | - | - | - | - | - | - |


| D=16" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Openin$\mathrm{g} \mathrm{ft}^{\prime}$ | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 |
| 10 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 |
| 12 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 |
| 14 |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 |
| 16 |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#8 |
| 18 |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 |
| 20 |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 | - | - |


| D=20" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Openin } \\ \mathrm{g} \mathrm{ft} \end{gathered}$ | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3-11 | 2 - \#6 | 2 - \#6 | 2 - \#6 | 2 - \#6 | 2-\#6 | 2-\#6 | 2 - \#6 | 2 - \#6 | 2-\#6 | 2 - \#6 | 2 - \#6 | 2 - \#6 | 2 - \#6 | 2-\#6 | 2 - \#6 | 2 - \#6 | 2-\#6 |
| 12 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 14 | 2-\#6 | 2-\#6 | 2 - \#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 16 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 18 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 |
| 20 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 |


| D=24" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Openin | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| g ft | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3-13 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 14 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 16 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 18 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 20 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |


| D=30" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { Openin } \\ \mathrm{g} \mathrm{ft} \\ \hline \end{gathered}$ | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3-17 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 18 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 20 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |

## Notes:

1. Where not shown otherwise, bottom steel is 2-\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain "-" the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrup. For stirrup information refer to Figure 4.
5. Factored Point Load includes 1.2, and 1.6 for dead and live load, respectively. For example, (1.2*dead load)+(1.6*live load)
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

 TABLE 5D - LOGIX 10" LINTEL REINFORCEMENT WITH CONCENTRATED LOAD| s=3", D=8" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c\|} \hline \text { Opening } \\ \mathrm{ft} \end{array}$ | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | - |
| 6 |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | - | - |
| 7 |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | - | - | - | - |
| 8 |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | - | - | - | - | - | - |
| 9 |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | - | - | - | - | - | - | - | - |
| 10 |  |  |  |  |  | 2-\#6 | - | - | - | - | - | - | - | - | - | - | - |
| 12 |  |  |  | 2-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 14 |  |  | 2-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 16 |  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 18 | 2-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| s=4", D=10" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c\|} \hline \text { Opening } \\ \mathrm{ft} \end{array}$ | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#7 |
| 8 |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 |
| 9 |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#8 |
| 10 |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 |
| 12 |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 | 2-\#8 | - | - |
| 14 |  |  |  |  |  | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 | 2-\#8 | - | - | - | - | - | - |
| 16 |  |  |  | 2-\#6 | 2-\#7 | 2-\#8 | 2-\#8 | - | - | - | - | - | - | - | - | - | - |
| 18 |  |  | 2-\#6 | 2-\#8 | 2-\#8 | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 |  | 2-\#6 | 2-\#8 | 2-\#8 | - | - | - | - | - | - | - | - | - | - | - | - | - |


| s=5", D=12" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ft | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 |
| 8 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 |
| 9 |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 |
| 10 |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 |
| 12 |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 |
| 14 |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 | - |
| 16 |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 | 2-\#8 | - | - | - | - | - |
| 18 |  |  |  |  | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 | - | - | - | - | - | - | - | - |
| 20 |  |  |  | 2-\#6 | 2-\#7 | 2-\#8 | 2-\#8 | - | - | - | - | - | - | - | - | - | - |


| s=7", D=16" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Openi ng ft | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3-8 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2 - \#6 | 2-\#6 |
| 9 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 10 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 12 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 14 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 |
| 16 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 |
| 18 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 |
| 20 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 | - | - |


| D=20" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Openi ng ft | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3-11 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 12 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 14 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 16 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 18 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 20 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 |


| D=24" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Openi ng ft | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3-13 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 14 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 16 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 18 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 20 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |


| D=30" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Openi ng ft | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3-15 | 2-\#8 | 2 - \#8 | 2-\#8 | 2-\#8 | 2 - \#8 | 2 - \#8 | 2 - \#8 | 2 - \#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2 - \#8 | 2-\#8 | 2 - \#8 | 2-\#8 |
| 16 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 |
| 18 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2 - \#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 |
| 20 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2 - \#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 |

Notes:

1. Where not shown otherwise, bottom steel is 2-\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain "-" the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrup. For stirrup information refer to Figure 4.
5. Factored Point Load includes 1.2, and 1.6 for dead and live load, respectively. For example, (1.2*dead load)+(1.6*live load)
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.

LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS TABLE 5E - LOGIX 12" LINTEL REINFORCEMENT WITH CONCENTRATED LOAD

| S=3", D=8" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Opening } \\ \mathrm{ft} \end{gathered}$ | Factored Point Load, Ib |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 |
| 6 |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 |
| 7 |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | - |
| 8 |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | - | - |
| 9 |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | - | - | - | - | - |
| 10 |  |  |  |  |  |  | 2-\#6 | 2-\#7 | 2-\#7 | - | - | - | - | - | - | - | - |
| 12 |  |  |  |  | 2-\#6 | 2-\#7 | - | - | - | - | - | - | - | - | - | - | - |
| 14 |  |  |  | 2-\#7 | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 16 |  | 2-\#7 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 18 | 2-\#6 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| s=4", D=10" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ft | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#7 |
| 8 |  |  |  |  |  |  |  |  |  |  |  | 2 - \#6 | 2 - \#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 |
| 9 |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 |
| 10 |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2 - \#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 |
| 12 |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 | 2-\#8 | - | - |
| 14 |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 | - | - | - | - | - | - |
| 16 |  |  |  | 2-\#6 | 2-\#7 | 2-\#8 | 2-\#8 | - | - | - | - | - | - | - | - | - | - |
| 18 |  |  | 2-\#6 | 2-\#8 | 2-\#8 | - | - | - | - | - | - | - | - | - | - | - | - |
| 20 |  | 2-\#6 | 2-\#8 | - | - | - | - | - | - | - | - | - | - | - | - | - | - |


| s=5", D=12" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ft | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 |
| 8 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 |
| 9 |  |  |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 |
| 10 |  |  |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 |
| 12 |  |  |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 |
| 14 |  |  |  |  |  |  |  | 2-\#6 | 2-\#6 | 2 - \#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 | 2-\#8 | - |
| 16 |  |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#8 | 2-\#8 | 2-\#8 | - | - | - | - | - |
| 18 |  |  |  |  | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#8 | 2-\#8 | - | - | - | - | - | - | - | - |
| 20 |  |  |  | 2-\#6 | 2-\#7 | 2-\#8 | 2-\#8 | - | - | - | - | - | - | - | - | - | - |


| s=7", D=16" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Opening } \\ \text { ft } \end{gathered}$ | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3-8 | 2-\#6 | 2-\#6 | 2 - \#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2 - \#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2 - \#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2 - \#6 | 2-\#6 |
| 9 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 10 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 |
| 12 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 |
| 14 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 |
| 16 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 |
| 18 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#6 | 2-\#7 | 2-\#8 | 2-\#8 | 2-\#8 |
| 20 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#6 | 2-\#7 | 2-\#6 | 2-\#7 | 2-\#7 | 2-\#6 | 2-\#8 | 2-\#8 | - | - |


| ( ${ }^{\text {a }}$ s=9", D=20" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Opening ft | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3-11 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2 - \#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 12 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 14 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 16 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 18 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2 - \#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 |
| 20 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#7 | 2-\#8 |


| s=11", D=24" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c} \hline \begin{array}{c} \text { Opening } \\ \mathrm{ft} \end{array} \\ \hline \end{array}$ | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3-13 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 |
| 14 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2 - \#8 |
| 16 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 |
| 18 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 |
| 20 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 | 2-\#8 |


| s=14", D=30" |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c} \hline \begin{array}{c} \text { Opening } \\ \mathrm{ft} \end{array} \\ \hline \end{array}$ | Factored Point Load, lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 | 6000 | 6500 | 7000 | 8000 | 9000 | 10000 |
| 3-15 | 3-\#7 | 3- \#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3- \#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3- \#7 | 3- \#7 | 3-\#7 |
| 16 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3- \#7 | 3- \#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3- \#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 |
| 18 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 |
| 20 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 | 3-\#7 |

1. Where not shown otherwise, bottom steel is 2 -\#5
2. Table is to be read in conjunction w/ Figure 4.
3. Where spaces contain "-" the bar is presumed to be less economical and/or practical. Alternatively, consult with a local engineer to determine if a practical bar size is possible based on local load conditions.
4. Blank regions require no stirrups. Shaded regions require stirrup. For stirrup information refer to Figure 4.
5. Factored Point Load includes 1.2, and 1.6 for dead and live load, respectively. For example, (1.2*dead load)+(1.6*live load)
6. Table values are based on concrete with a minimum specified compressive strength of 3 ksi and 40 ksi reinforcing steel.
7. Based on 40 ksi reinforcing steel. Lintels tables for 60 ksi reinforcing steel are available for download at www.logixicf.com.


Flexural reinf. single bar
(Applies to 4, 6.25, 8 \& 10" LOGIX)


Double mat flexural reinf. w/ ties, as req'd

| Vertical |
| :--- |
| shear reinf | | Horizontal |
| :--- |
| shear reinf |

FIGURE 7: PLAN VIEW
LOGIX SHEAR WALL - DOUBLE MAT FLEXURAL REINF.
(Applies to 4, 6.25, 8 \& 10" LOGIX)

Double mat horiz.
\& vert. shear reinf.


FIGURE 8: PLAN VIEW
LOGIX SHEAR WALL - DOUBLE MAT FLEXURAL \& SHEAR REINF.

(Applies to 12" LOGIX)
NOTES:

1. Shear wall Figures 6 to 8 to be used in conjunction with Tables 6A and 6B.
2. Provide double mat of reinforcement for 12" Logix wall. See Figure 8.
3. Fully develop flexural reinforcement into the footing.
4. Min. 28 day concrete compressive strength $=3 \mathrm{ksi}$. Steel yield strength $=60 \mathrm{ksi}$.
5. Clear spacing between flexural reinforcement bars $=3$ in

These tables should only be used if the above conditions are met. For other conditions, consult a structural engineer.

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

TABLE 6A - SHEAR WALL: HORIZONTAL \& VERTICAL SHEAR REINFORCEMENT

| 4" LOGIX SHEAR WALL REINFORCEMENT SPACING,in |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SHEAR REINFORCEMENT (applies to horizontal \& vertical reinforcement) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | SHEAR FORCE, Vu, kpf |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Bar Size | Wall Length, | 0.5 |  | 1 |  | 1.5 |  | 2 |  | 2.5 |  | 3 |  | 3.5 |  | 4 |  |
|  |  | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. |
| $\begin{gathered} \# 4, ~ \# 5, \text { or } \\ \# 6 \end{gathered}$ | 2 | 12 | 12 | 12 | 12 | 12 | 12 | 4 | 8 | 4 | 8 | 4 | 8 | 4 | 8 | 4 | 8 |
|  | 4 | 12 | 12 | 12 | 12 | 12 | 12 | 8 | 16 | 8 | 16 | 8 | 16 | 8 | 16 | 8 | 16 |
|  | >4 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 20 | 12 | 20 | 12 | 20 | 12 | 20 | 12 | 20 |


| 6.25" LOGIX SHEAR WALL REINFORCEMENT SPACING,in |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SHEAR REINFORCEMENT (applies to horizontal \& vertical reinforcement) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Bar Size | Wall Length, | SHEAR FORCE, Vu, kpf |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 1 |  | 2 |  | 3 |  | 4 |  | 5 |  | 6 |  | 7 |  | 8 |  |
|  |  | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. |
|  | 2 | 12 | 16 | 12 | 16 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| \#4, \#5, or | 4 | 12 | 16 | 12 | 16 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| \#6 | 6 | 12 | 16 | 12 | 16 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
|  | >6 | 12 | 16 | 12 | 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 |

8" LOGIX SHEAR WALL REINFORCEMENT SPACING,in
SHEAR REINFORCEMENT (applies to horizontal \& vertical reinforcement)

| Bar Size | Wall Length, | SHEAR FORCE, Vu, kpf |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1.5 |  | 2.5 |  | 5 |  | 6 |  | 7 |  | 8 |  | 9 |  | 10 |  |
|  |  | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. |
| $\begin{gathered} \# 4, \# 5 \text {, or } \\ \# 6 \end{gathered}$ | 2 | 12, 12, 16 | 16 | 12, 16, 16 | 16 | 4 | 16 | 4 | 16 | 4 | 16 | 4 | 16 | 4 | 16 | 4 | 16 |
|  | 4 | 12, 12, 16 | 16 | 12, 16, 16 | 16 | 8 | 16 | 8 | 16 | 8 | 16 | 8 | 16 | 8 | 16 | 8 | 16 |
|  | 6 | 12, 12, 16 | 16 | 12, 16, 16 | 16 | 12 | 16 | 12 | 16 | 12 | 16 | 12 | 16 | 12 | 16 | 12 | 16 |
|  | >6 | 12, 12, 16 | 16 | 12, 16, 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 | 16 |

## 10" LOGIX SHEAR WALL REINFORCEMENT SPACING,in

SHEAR REINFORCEMENT (applies to horizontal \& vertical reinforcement)

| Bar Size | Wall Length, | SHEAR FORCE, Vu, kpf |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1.5 |  | 2.5 |  | 5 |  | 6 |  | 7 |  | 8 |  | 9 |  | 10 |  |
|  |  | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. | Horiz. | Vert. |
| $\begin{gathered} \text { \#4, \#5, or } \\ \# 6 \end{gathered}$ | 2 | 8,12,16 | 16 | 8,12,16 | 16 | 4 | 8 | 4 | 8 | 4 | 8 | 4 | 8 | 4 | 8 | 4 | 8 |
|  | 4 | 8,12,16 | 16 | 8,12,16 | 16 | 8 | 16 | 8 | 16 | 8 | 16 | 8 | 16 | 8 | 16 | 8 | 16 |
|  | 6 | 8,12,16 | 16 | 8,12,16 | 16 | 12 | 24 | 12 | 24 | 12 | 24 | 12 | 24 | 12 | 24 | 12 | 24 |
|  | >6 | 8, 12,16 | 16 | 8, 12, 16 | 16 | 16 | 24 | 16 | 24 | 16 | 24 | 16 | 24 | 16 | 24 | 16 | 24 | 12" LOGIX SHEAR WALL REINFORCEMENT SPACING,in

SHEAR REINFORCEMENT (applies to horizontal \& vertical reinforcement)


NOTES:

1. Table 6A to be read in conjunction with Shear Wall Figures 6 to 8.
2. Steel yield strength $=60 \mathrm{ksi}, 28$ day concrete compresive strength $=3 \mathrm{ksi}$.

| 4" LOGIX - FLEXURAL REINFORCEMENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wall Length, | 0.5 |  |  | 1 |  |  | 1.5 |  |  | SHEAR FORCE, Vu, kpf <br> 2 |  |  |  |  |  | 3 |  |  | 3.5 |  |  | 4 |  |  |
|  | \#4 | \#5 | \#6 | \#4 | \#5 | \#6 | \#4 | \#5 | \#6 | \#4 | \#5 | \#6 | \#4 | \#5 | \#6 | \#4 | \#5 | \#6 | \#4 | \#5 | \#6 | \#4 | \#5 | \#6 |
| 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
| 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
| 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
| 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 |
| 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 |


| 6.25" LOGIX - FLEXURAL REINFORCEMENT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wall Length, Iw, ft | 1 |  |  | 2 |  |  | 3 |  |  | SHEAR FORCE, Vu, kpf |  |  |  |  |  |  |  |  | 7 |  |  | 8 |  |  |
|  |  |  |  |  | 4 |  |  |  |  |  | 5 |  | 6 |  |  |  |  |  |  |  |  |
|  | \#4 | \#5 | \#6 |  |  |  | \#4 | \#5 | \#6 | \#4 | \#5 | \#6 | \#4 | \#5 | \#6 | \#4 | \#5 | \#6 | \#4 | \#5 | \#6 | \#4 | \#5 | \#6 | \#4 | \#5 | \#6 |
| 2 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| 4 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| 6 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| 8 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
| 10 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| 15 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| 20 | 13 | 13 | 13 | 13 | 13 | 13 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 |

NOTES:

1. Table 6B to be used in conjunction with Shear Wall Figures 6 to 8 .
2. Where spaces contain "-" consult with a local licensed engineer.
3. Where more than one bar is shown use double mat for flexural reinforcement. See Figure 7 (or Figure 8 for 12" Logix).
4. Steel yield strength $=60 \mathrm{ksi}, 28$ day concrete compressive strength $=3 \mathrm{ksi}$.

NOTE: Logix recommends builders, owners and/or designers using these tables confirm that on-site building conditions are w/in the scope of the tables being

Load Bearing Soil Classifications ${ }^{1}$

| MINIMUM LOAD BEARING VALUE <br>  <br> psf | SOIL DESCRIPTION |
| :--- | :--- |
| 2000 psf | Clay, sandy clay, silty clay, and clayey silt |
| 3000 psf | Sand, silty sand, clayey sand, silty gravel, and <br> clayey gravel |
| 4000 psf | Sandy gravel and medium stiff clay |
| $>4000$ psf | Stiff clay, gravel, sand, sedimentary rock, and <br> crystalline bedrock. |

1. User must verify that the values in this table agree with local codes and practices.
2. Tabulated values are the presumed strength of the soil, undisturbed (the maximum design load bearing value for the basement or foundation wall footing).

Equivalent Fluid Density Soil Classification ${ }^{1,2}$

| MAXIMUM <br> EQUIVALENT <br> FLUID <br> DENSITY, pcf | USC $^{2}$ CLASSIFICATION | SOIL DESCRIPTION |
| :---: | :--- | :--- |
| 30 pcf | GW, GP, SW, SP | Well-drained cohesionless soils such as clean (few <br> or no fines) sand and gravels. |
| 45 pcf | GM, GC, SM, SM-SC, <br> ML | Well-drained cohesionless soils such as sand and <br> gravels containing silt or clay. |
| 60 pcf | SC, MH, CL, CH, ML-CL | Well-drained inorganic silts or clays that are <br> broken up into smaller pieces. |

1. User must verify that the values in this table agree with local codes and practices.
2. USC - Uniform soil classification

NOTE: Logix recommend builders, owners and/or designers using these tables confirm that on-site loading conditions are within the scope of the tables being used.

## Minimum width of concrete footing for Logix walls

| Maximum <br> Number of Storeys | MINIMUM LOAD BEARING VALUE OF SOIL |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2000 psf | 2500 psf | 3000 psf | 3500 psf | 4000 psf |
| 6.25" Logix Wall Thickness |  |  |  |  |  |
| One Storey | 15" | 12" | 10" | 9" | 8" |
| Two Storey | 20" | 16" | 13" | 12" | 10" |
| 8" Logix Wall Thickness |  |  |  |  |  |
| One Storey | 18" | 14" | 12" | 10" | 8" |
| Two Storey | 24" | 19" | 16" | 14" | 12" |
| 10" Logix Wall Thickness |  |  |  |  |  |
| One Storey | 20" | 16" | 13" | 11" | 10" |
| Two Storey | 27" | 22" | 18" | 15" | 14" |

- Minimum 28 day concrete compressive strength $=3000$ psi ( 20 MPa )
- Table does not consider seismic. Footing design must also consider local design loads and building practices.
- Footings shall be minimum 8" thick, and shall have a width that allows for a nominal 2 inch projection from either face of the concrete in the wall to the edge of the footing.
- Table values are based on 40 ft building width (floor and roof clear span).
- Applicable for storey heights not greater than 9'-4".
- Basement wall shall not be considered as a storey in determining footing widths.
- Applicable also for 8 inch thick or 10 inch thick Logix foundation wall supporting 4 inch Logix storeys.
- Applicable also for 10 inch thick or 10 inch thick Logix foundation wall supporting 6.25 inch Logix storeys.
7.1- US CODE REPORTS ..... 7-2
7.1 - WISCONSIN BUILDING PRODUCTS ..... 7-3
7.2 - STATE OF FLORIDA CERTIFICATE OF APPROVAL ..... 7-11
7.3 - MIAMI-DADE COUNTY ..... 7-13
7.4 - CITY OF NEW YORK - MEA (MATERIALS \& EQUIPMENT ACCEPTANCE). ..... 7-16
7.5 - NON-COMBUSTIBLE CONSTRUCTION (I-CODES) ..... 7-18
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## 7.1 - WISCONSIN BUILDING PRODUCTS

Approval \# 20199000
(Replaces 201307-I)
Industry Services Division 4822 Madison Yards Way P.O. Box 7302

Madison, WI 53701-7302

## Wisconsin Building Product Evaluation


Manufacturer

| AMC Foam Technologies, Inc. |
| :---: |
| 35 Headingley St. |
| Headingley, MB R4H0A8 |
| Canada |

## SCOPE OF EVALUATION

GENERAL: This report evaluates the use of the Logix Insulated Concrete Form Wall System, manufactured by AMC Foam Technologies, Inc., evaluated as permanent form work and insulation system for reinforced concrete beams, lintels, exterior and interior walls, and foundation and retaining walls. The Logix Insulated Concrete Form Wall System was evaluated for safety requirements of the foam plastic and structural requirements for the codes listed below.

This review includes code requirements in accordance with the current Wisconsin Uniform Dwelling Code for $1 \& 2$ family dwellings (UDC):

- Foam Plastic: The Logix Insulated Concrete Form Wall System was evaluated in accordance with the fire safety requirements of SPS 321.11.
- Structural: The Logix Insulated Concrete Form Wall System was evaluated in accordance with the structural requirements of SPS 321.02(3)(d).

This review includes the cited International Building Code (IBC) requirements below in accordance with the Wisconsin Amended IBC Code:

- Foam Plastic \& Fire Endurance: The Logix Insulated Concrete Form Wall System was evaluated in accordance with the fire safety requirements IBC 2603.


## 7.1 - WISCONSIN BUILDING PRODUCTS EVALUATION continued

Commercial Building Product Evaluation No. 20199000
Page 2

- Structural: The Logix Insulated Concrete Form Wall System was evaluated in accordance with the requirements of IBC Chapter 16.
- Fire-Resistance Rating and Fire Tests: The Logix Insulated Concrete Form Wall System was evaluated in accordance with the requirements of IBC 703.1 and 703.2.

Note: Structural calculations shall be submitted (job-to-job basis) in accordance with IBC Chapter 16 for applicable Live, Ground Snow, Roof, Wind, and Seismic Loads.

## DESCRIPTION AND USE

General: The Logix Insulated Concrete Form Wall System consists of expanded polystyrene (EPS) forms which are stacked in running bond and serve as forms for a 4-inch-thick, 6.25-inchthick, 8 -inch-thick, 10 -inch-thick, and 12 -inch or more-thick reinforced concrete wall. The EPS forms remain in place to provide insulation for the wall. The reinforced concrete wall system may be used as a foundation wall, above grade wall, basement wall, shear wall, exterior loadbearing wall, non-load bearing, and lintel section.

The Logix EPS forms are 48 inches long and 16 inches high. The 4-inch Logix form for 4-inchthick reinforced concrete walls is $91 / 2$ inches wide. The 6.25 -inch Logix form for 6 -inch-thick reinforced concrete walls is $113 / 4$ inches wide. The 8 -inch Logix form for 8 -inch-thick reinforced concrete walls is $131 / 2$ inches wide. The 10 -inch Logix form for 10 -inch-thick reinforced concrete walls is $15 \frac{1}{2}$ inches wide. The 12 -inch Logix form for 12 -inch-thick reinforced concrete walls is $171 / 2$ inches wide. Thicker walls are achieved by the use of Logix Xtender Ties.

The forms are available as solid-form blocks or knock-down blocks. The solid-form blocks consist of opposing form panels connected by 6 polypropylene web ties embedded into the panels forming a solid form block. The knock-down blocks consist of opposing form panels connected by 6 polypropylene snap-in-place ties. The polypropylene plastic web ties are spaced 8 inches on center and black in color.

Material: Logix Form Blocks are molded from modified expandable polystyrene beads.
Manufacturers include:
Product $\quad$ Manufacturer
BFL-422
The blocks are manufactured to a nominal density of 1.68 pounds per cubic foot.

The blocks are manufactured to a nominal density of 1.68 pounds per cubic foot.
Concrete: Normal-weight concrete complying with SPS 321.02(3)(d) and IBC 1903.1 with maximum aggregate size of $3 / 4$ inch and a minimum compressive strength of $2,500 \mathrm{psi}$.

Reinforcement: The concrete is reinforced with Nos. 3, 4, 5 and 6 deformed steel reinforcing bars, Type A615, Grade No. 40, with a minimum yield strength of 40,000 psi and Grade No. 60, with a minimum yield strength of $60,000 \mathrm{psi}$. All steel reinforcement shall be in accordance with IBC 1901.2 \& ACI 318 as modified by IBC 1905.

## 7.1 - WISCONSIN BUILDING PRODUCTS EVALUATION continued

Commercial Building Product Evaluation No. 20199000
Page 3
Each pallet of Logix forms shall bear a label with the manufacturer's name, and the quality control inspection agency.

## TESTS AND RESULTS

Intertek Testing Services, ETL SEMKO, conducted testing on the Logix forms. The Logix insulated concrete forms produced by Foam Technologies, Inc. have been subject to and complied with the following testing:

- EPS has a maximum flame-spread rating of 25 and a maximum smoke-developed rating of 450. Testing was done in accordance with ASTM E 84.
- Meets 3-hour fire rating in accordance with ASTM E119 and CAN/ULC S101 conducted by Intertek Testing Services NA Ltd, on April 24, 2002 filed with previous approval report.

| Assembly Rating, hours | Minimum ICF Cavity Thickness, in. |
| :---: | :---: |
| 2 | 4 |
| 3 | 6.25 (4-hr. rating with 5/8" drywall) |
| 4 | Greater than or equal to 8 |
| NOTE. 1. Unless not |  |

NOTE: 1. Unless noted otherwise, ratings are based on wall assembly having $1 / 2^{\prime \prime}$ drywall on fire exposed side.
2. Load bearing during test $=36,000 \mathrm{lb} / \mathrm{ft}$.

- Room fire Test Standard for Interior of Foam Plastics Systems in accordance with ASTM D1929, D635 and D2843.
- Crawl Space evaluation conducted in accordance with ICC ES requirements.
- Conforms to ASTM C578, with equivalency CAN/ULC S701 (Standard Specification for Rigid, Cellular Polystyrene Thermal Insulation) as a Type II Thermal Insulating Material.
- Fastener Withdrawal Evaluation in accordance with ASTM D1761.
- Fastener Lateral Resistance tested in accordance with ASTM D1761.
- Polypropylene web material conforms to CC1 Plastic material when tested in accordance with ASTM D1929, D635, and D2843.

The Rigid Cellular (RCPS) Polystyrene Thermal Insulation was tested May 10, 2002 for apparent density, compressive properties, and flexural properties in accordance with ASTM C578-95 "Standard Specification for Rigid, Cellular Polystyrene Thermal Insulation," using the following test methods:

- Apparent Density: ASTM D1622-98 "Standard Test Method for Apparent Density of Rigid Cellular Plastics".

| Type | Test Result | Minimum Requirement | Status |
| :---: | :---: | :---: | :---: |
| Type II | 1.68 | $1.35 \mathrm{lbs} / \mathrm{ft}^{3}$ | Complied |

- Compressive Properties: ASTM C165-00 "Standard Test Method for Measuring Compressive Properties of Thermal Insulation".

| Type | Test Result | Minimum Requirement | Status |
| :---: | :---: | :---: | :---: |
| Type II | 24.5 psi | 15.0 psi | Complied |

## All documents are downloadable at logixicf.com

## 7.1 - WISCONSIN BUILDING PRODUCTS EVALUATION continued

Commercial Building Product Evaluation No. 20199000
Page 4

- Flexural Properties: ASTM C203-99 "Standard Test Method for Breaking Load and Flexural Properties of Block-Type Thermal Insulation"

| Type | Test Result | Minimum Requirement | Status |
| :---: | :---: | :---: | :---: |
| SC Type II | 44.9 psi | 40.0 psi | Complied |

Physical properties testing on May 10, 2002 of polypropylene reinforcing web material was performed in general accordance with the following test methods:

- Screw Withdrawal: ICC ES AC 116 (July 2001) "Acceptance Criteria for Nails and Spikes," in conjunction with ASTM D1761-88 (Re-approved 2000) "Standard Test Methods for Mechanical Fasteners in Wood", Sections 1 through 12 (two types of fasteners were tested: a type ' $W$ ' coarse thread drywall screw, and a type 'S' fine thread drywall screw)
- Lateral Screw Resistance: ICC ES AC 116 (July 2001) "Acceptance Criteria for Nails and Spikes," in conjunction with ASTM D1761-88 (Re-approved 2000) "Standard Test Methods for Mechanical Fasteners in Wood", Sections 13 through 20

|  | Fastener Type | Withdrawal | Lateral |
| :---: | :---: | :---: | :---: |
|  |  | Max Load (lbs.) | Max Load (lbs.) |
| Average | Type 'W' Coarse Thread Drywall Screw | 166 | 367 |
| COV | Type 'W' Coarse Thread Drywall Screw | $10.6 \%$ | $8.4 \%$ |
| Average | Type 'S' Fine Thread Drywall Screw | 169 | 328 |
| COV | Type 'S' Fine Thread Drywall Screw | $8.4 \%$ | $4.1 \%$ |

- Tensile Strength: ASTM D638-01 "Standard Test Method for Tensile Properties of Plastics"

|  | Ultimate Tensile Strength (lbs.) |
| :---: | :---: |
| Average | 842 |
| COV | $1.7 \%$ |

DISCUSSION: ICC ES AC 116 references ASTM D1761 for lateral and withdrawal testing. The ASTM D6117 and ASTM D1761 are very similar in methodology, however ASTM D6117 is used for solid sections of plastic members and not for sheets of plastic material. In addition to this, the ICC ES AC 116 document gives guidance on establishing allowable loads, which ASTM D6117 does not provide. In the absence of a standard that more specifically addresses this issue, ITS (Intertek Testing Services) recommends that AC 116 is more appropriate.

It is ITS's opinion that it is appropriate to state specific loads for this material. ASTM D5456-99 clause A2.6.1 states, "The equivalent specific gravity is determined from Table 12.21 or Ref. (3) such that the table value for the tested nail does not exceed the average ultimate withdrawal resistance in pounds per inch ( $\mathrm{N} / \mathrm{mm}$ ) from A2.4 divided by 5.0 ..." The safety factor for withdrawal in ASTM D5456 matches that of AC 116, again justifying its applicability to this issue. ASTM D5456 does not have a comparable safety factor for lateral load resistance. In the absence of a standard that more specifically addresses this issue, ITS suggests that AC 116 is more appropriate.

Given the low C.O.V. of the web tensile test results, it is the opinion of ITS that a safety factor of approximately three is appropriate. ITS chose to use the lateral resistance factors of AC 116 for consistency.

## CALCULATIONS:

1. Web Tensile: $842 \mathrm{lbs} . \mathrm{x} 0.75=631 \mathrm{lbs}$. (Proportional limit assumed to be the same as ultimate load - brittle failure) $842 \mathrm{lbs} . \div 3.2=263 \mathrm{lbs}$. (Based on average ultimate load)
2. Fastener Testing:
(A) Withdrawal Resistance: Type "S" Screw Type "W" Screw
(B) Lateral Resistance:

Type "S" Screw $\quad \mathrm{F}_{\text {allow }}=\mathrm{F} \div 3.2=328 \mathrm{lbs} . \div 3.2=102.5 \mathrm{lbs}$. Type "W" Screw $\quad F_{\text {allow }}=\mathrm{F} \div 3.2=367 \mathrm{lbs} . \div 3.2=114 \mathrm{lbs}$.

## 7.1 - WISCONSIN BUILDING PRODUCTS EVALUATION continued

Commercial Building Product Evaluation No. 20199000
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## CONCLUSIONS: <br> Physical Properties of Polypropylene Reinforcing Webs

The polypropylene reinforcing webs were found to have the following allowable loads, as recommended by ITS when analyzed in accordance with ICC ES AC 116 (July 2001) "Acceptance Criteria for Nails and Spikes." (The withdrawal resistance utilized a safety factor of five as per ICC ES AC 116, Section 4.2. The lateral resistance of both the Type "W" screws and the Type "S" screws utilize a safety factor of 3.2 when analyzed in accordance with ICC ES AC 116, Section 4.1.):

- Withdrawal resistance of a Type " S " fine thread drywall screw is 35 lbs .
- Withdrawal resistance of a Type "W" coarse thread drywall screw is 33 lbs .
- Lateral resistance of a Type "S" fine thread drywall screw is 102 lbs .
- Lateral resistance of a Type "W" coarse thread drywall screw is 114 lbs .

The polypropylene reinforcing web tensile strength is recommended by ITS to be 263 lbs. , based on a safety factor of 3.2 analyzed in accordance with ICC ES AC 116, Section 4.1. The maximum negative wind pressure for a cladding system attached to the EPS foam plastic panels is based on the maximum fastener values connected into the polypropylene reinforcing webs. For a screwed system into the webs, 8 inches on center vertically, and 6 inches on center horizontally, the allowable negative withdrawal is $99 \mathrm{lbs} . / \mathrm{ft}^{2}$. This withdrawal capacity can be converted to a wind speed based on the following formula extrapolated from the 1997 Uniform Building Code Table 16-F at a standard height of 33 feet:
$\mathrm{q}_{\mathrm{s}}=\mathrm{Kv}^{2}$
where: $\mathrm{q}_{\mathrm{s}}=$ wind pressure ( $\mathrm{lbs} . / \mathrm{ft}^{2}$ )
and: $\quad \mathrm{v}=$ basic wind speed ( mph )
and: $\quad \mathrm{K}=0.00256$
thus: $\quad \mathrm{v}=\left(\mathrm{q}_{\mathrm{s}} \div 0.00256\right)^{1 / 2}$
given: $\mathrm{q}_{\mathrm{s}}=99 \mathrm{lbs} . / \mathrm{ft}^{2}$ (allowable negative withdrawal)
then: $\quad \mathrm{v}=197 \mathrm{mph}$

- Three Hour Fire Endurance Test: ASTM E119-98, "Standard Test Methods for Fire Tests of Building Construction and Materials"

[^2]
## LIMITATIONS OF APPROVAL

## 7.1 - WISCONSIN BUILDING PRODUCTS EVALUATION continued

Commercial Building Product Evaluation No. 20199000
Page 6

The limitations below are in accordance with the current Wisconsin Uniform Dwelling Code (UDC), for $1 \& 2$ family dwellings:

- Foam Plastic: The ICF wall system is approved for use with a thermal barrier to separate the blocks from interior spaces in accordance with SPS 321.11(1). Where a 1-inch thickness of masonry does not separate the polystyrene blocks from the building interior, including at the top of the wall, a thermal barrier, which has a finish rating of at least 15 minutes, shall be provided.

1. Logix Form Blocks are approved for use in combustible non-rated construction in accordance with SPS 321.11. In one- or two-family dwellings, thermal barriers shall be provided to separate the forms from the occupied space of the dwellings per SPS 321.11.
2. The exterior face of the blocks shall be finished with an approved weather covering and must be protected from ultraviolet light.

- Structural: The Logix Form Blocks are approved as structural building elements.

1. The units are approved for use as concrete forms for basement walls and exterior walls when the resulting concrete core thickness satisfies Table 321.18-B for one- or twofamily dwellings, or when structural calculations for the product are submitted for review.
2. Walls shall be anchored to all floors and roofs. Walls shall be interconnected at corners by embedding and lapping the reinforcement.
3. Structures are limited to two stories in height.
4. The forms are approved for use as concrete forms for basement walls, exterior walls and retaining walls when structural calculations are submitted to the local building inspector.
5. Below grade walls shall be damp-proofed when required by the local building department.
6. Damp-proofing and water-proofing materials shall be approved by AMC Foam Technologies, Inc. and the local building official, and shall be free of solvents that will adversely affect the EPS foam.

NOTE: The Logix Insulated Concrete Form Wall System was not evaluated for compliance with the thermal requirements of Subchapter III and IV of chapter SPS 322 provisions.

The 2015 IBC limitations below are in accordance with the 2018 Wisconsin Commercial Building Code:

- Foam Plastic: The Logix ICF wall system is approved for use with a thermal barrier to separate the blocks from interior spaces in accordance with IBC 2603.4.

1. In accordance with IBC 2603.4.1.6, when the Logix ICF is used within the attic or crawl space where entry is made only for service utilities, the foam plastic insulation shall be protected against ignition by $1 \frac{1}{2} / 2$ thick mineral fiber insulation, a $1 / 4 "$ thick wood structural panel, particleboard or hardboard, gypsum wallboard, corrosion-resistant steel or other approved material installed so that the foam plastic is not exposed.
2. The protective covering shall be consistent with the requirements for the type of construction.

## 7.1 - WISCONSIN BUILDING PRODUCTS EVALUATION continued

Commercial Building Product Evaluation No. 20199000
Page 7
3. The crawl space shall not be used for storage or air handling purposes, there are no interconnected basement areas and entry to the crawl space is only for service of utilities.
4. The exterior face of the blocks shall be finished with an approved weather covering per IBC 1405.2 and must be protected from ultraviolet light per IBC 1404.13 \& IECC C303.2.1.

- Structural: Design of concrete formed by Logix Forms must comply with IBC Chapter 19 with the following requirements:

1. *The forms are approved for use as concrete forms for basement walls, exterior walls and retaining walls when structural calculations are submitted to the department by a Wisconsin registered professional engineer or architect.
2. *Design calculations of walls must comply with section IBC 1901.2. Use of the empirical masonry design approach specified in IBC 2109.1 [SPS 362.2109] is prohibited.
3. Design of lintels shall comply with the applicable provisions of IBC Chapter 16.
4. Wall loading shall be in accordance with IBC Chapter 16.
5. Minimum wall reinforcement shall conform to IBC 1901.2. When the code requires that vertical and horizontal reinforcement be spaced no further apart than 18 inches or three times the wall thickness, whichever is less, the maximum concrete wall thickness along the length of the wall is permitted to be used to determine rebar spacing.
6. Walls shall be anchored to floors and roofs in accordance with IBC 1604.8.2. Walls shall be interconnected at corners by embedding and lapping reinforcement in accordance with the code.
7. Design of shear walls shall be in accordance with sections IBC 1901.2 and 1905.
8. Structures are limited to two stories in height plus a basement.
9. Below grade walls shall be damp-proofed when required by the local building department. Water proofing shall be in accordance with IBC 1805.
10. Damp-proofing and water-proofing materials shall be approved by AMC Foam Technologies, Inc. and the local building official, and shall be free of solvents that will adversely affect the EPS foam.
11. Special inspection per IBC chapter $\mathbf{1 7}$ are not required when meeting these limitations:
a) Wall systems are a maximum of 8 feet high and are limited to use in single-story construction of Group R-3, or Group U occupancies.
b) Maximum height of a concrete pour is 48 inches. Succeeding lifts must be placed in accordance with ACI 318 as modified by IBC 1905.
c) Installation is by properly trained installers approved by AMC Foam Technologies, Inc.
d) The installation instructions indicate methods used to verify proper placement of concrete.
12. Walls constructed with Logix ICF are considered Type V Construction.
[^3]
## 7.1 - WISCONSIN BUILDING PRODUCTS EVALUATION continued

Commercial Building Product Evaluation No. 20199000
Page 8

NOTE: The Logix Insulated Concrete Form Wall System was not evaluated for compliance with the thermal requirements of IECC chapters C4 \& R4.

Identification: Each package bears a label specifying the name and address of the manufacturer (AMC Foam Technologies, Inc., Headingley, MB R4H0A8, Canada). Additionally, product labels indicate the Wisconsin Building Product Evaluation Number and the name and logo of the quality control agency.

## DISCLAIMER

This approval will be valid through December 31, 2024, unless manufacturing modifications are made to the product or a re-examination is deemed necessary by the department. The Wisconsin Building Product Evaluation Number must be provided when plans that include this product are submitted for review. This approval addresses only the specified applications for the product and does not waive any code requirement not specified in this document.
Reviewed by: Gack a. Miller

Approval Date: $\quad$ February 19, $2019 \quad$ By: Jack A. Miller $\quad$ Commercial building plan examiner and product reviewer

## 7.2 - STATE OF FLORIDA CERTIFICATE OF APPROVAL

2/20/2021


Florida Building Code Online


Submit Surcharge $\mid$ Stats \& Facts


Product Approval
USER: Public User

Product Approval Menu > Product or Application Search > Application List > Application Detail

- OFFICE OF THE

FL \#
Application Type Code Version Application Status

FL14469-R3

2017
Approved
*Approved by DBPR. Approvals by DBPR shall be reviewed and ratified by the POC and/or the Commission if necessary.

| Comments |  |  |
| :---: | :---: | :---: |
| Archived | $\square$ |  |
| Product Manufacturer | Logix Insulated Concrete Forms |  |
| Address/Phone/Email | 199-1917 West 4th Avenue <br> Vancouver, FL 33133 <br> (866) 944-0153 <br> francis@logixicf.com |  |
| Authorized Signature | Francis Roma francis@logixicf.com |  |
| Technical Representative | Francis Roma |  |
| Address/Phone/Email | 2755 Columbia Street Vancouver (866) 944-0153 francis@logixicf.com |  |
| Quality Assurance Representative | Francis Roma |  |
| Address/Phone/Email | 106 Perma R Road Johnson City, TN 37063 francis@logixicf.com |  |
| Category | Structural Components |  |
| Subcategory | Insulation Form Systems |  |
| Compliance Method | Certification Mark or Listing |  |
| Certification Agency | QAI Laboratories |  |
| Validated By | QAI Laboratories |  |
| Referenced Standard and Year (of Standard) | Standard | Year |
|  | ASTM C578 | 2012 |
|  | ASTM D1761 | 2006 |
|  | ASTM D1929 | 2012 |
|  | ASTM D635 | 2010 |
|  | ASTM E119 | 2012 |
|  | ASTM E2634 | 2011 |
|  | ASTM E84 | 2013 |

Equivalence of Product Standards
Certified By

## 7.2 - STATE OF FLORIDA CERTIFICATE OF APPROVAL continued

Product Approval Method

Date Submitted
Date Validated
Date Pending FBC Approval
Date Approved

Method 1 Option A

07/21/2017
07/21/2017

07/25/2017

Summary of Products

| FL \# | Model, Number or Name | Description |
| :---: | :---: | :---: |
| 14469.1 | Logix Insulated Concrete Forms | Insulated concrete forms |
| Limits of Use <br> Approved for use in HVHZ: Yes <br> Approved for use outside HVHZ: Yes <br> Impact Resistant: Yes <br> Design Pressure: N/A <br> Other: |  | Certification Agency Certificate <br> FL14469 R3 C CAC 3. B1031-1 Edition 2 - Logix - ICF Listing <br> Page 2015.pdf <br> FL14469 R3 C CAC Logix-Load Bearing Exterior Wall <br> Assembly Design Listing.pdf <br> Quality Assurance Contract Expiration Date 01/01/2022 <br> Installation Instructions <br> FL14469 R3 II Logix-Design-Manual-2017 Part I.pdf <br> FL14469 R3 II Logix-Design-Manual-2017 Part II.pdf <br> FL14469 R3 II Logix-Design-Manual-2017 Part III.pdf <br> Verified By: QAI Laboratories <br> Created by Independent Third Party: <br> Evaluation Reports <br> Created by Independent Third Party: |

Back Next

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Under Florida law, email addresses are public records. If you do not want your e-mail address released in response to a public-records request, do not send electronic Florida statutes, effective contact the office by phone or by traditional mail. If you have any questions, please contact 850.487 .1395 . *Pursuant to Section $455.275(1)$, provided may be used for official communication with the licensee. However email addresses are public record. If you do not wish to supply a personal address, please provide the Department with an email address which can be made available to the public. To determine if you are a licensee under Chapter 455, F.S., please click here.

Product Approval Accepts:
M

| Credit Card |
| :---: |
| Safe |
| securitymetrics |

## 7.3 - MIAMI-DADE COUNTY

## MIAMI-DADE <br> COUNTY

DEPARTMENT OF REGULATORY AND ECONOMIC RESOURCES (RER) BOARD AND CODE ADMINISTRATION DIVISION
NOTICE OF ACCEPTANCE (NOA)

MIAMI-DADE COUNTY PRODUCT CONTROL SECTION

11805 SW 26 Strect, Room 208
Miami, Florida 33175-2474
$\mathrm{T}(786)$ 315-2590 $\quad \mathrm{F}(786) 315-2599$

Perma R Products, Inc.
P.O. Box 5235

Johnson City, TN 37602
Scope:
This NOA is being issued under the applicable rules and regulations governing the use of construction materials. The documentation submitted has been reviewed and accepted by Miami-Dade County RERProduct Control Section to be used in Miami Dade County and other areas where allowed by the Authority Having Jurisdiction (AHJ).
This NOA shall not be valid after the expiration date stated below. The Miami-Dade County Product Control Section (In Miami Dade County) and/or the AHJ (in areas other than Miami Dade County) reserve the right to have this product or material tested for quality assurance purposes. If this product or material fails to perform in the accepted manner, the manufacturer will incur the expense of such testing and the AHJ may immediately revoke, modify, or suspend the use of such product or material within their jurisdiction. RER reserves the right to revoke this acceptance, if it is determined by Miami-Dade County Product Control Section that this product or material fails to meet the requirements of the applicable building code.
This product is approved as described herein, and has been designed to comply with the Florida Building Code, including the High Velocity Hurricane Zone.

## DESCRIPTION: Logix Insulating Concrete Forms

APPROVAL DOCUMENT: Drawing No. SB-Rev7, tifled "Logix Standard Forms", sheet 1 of 1, prepared by Logix Insulated Concrete Forms, dated 09/16/2014, signed and sealed by Hermes F. Norero, P.E. on 09/27/2019, bearing the Miami-Dade County Product Control revision stamp with the Notice of Acceptance number and expiration date by the Miami-Dade County Product Control Section.

## Missile Impact Rating: None

LABELING: Each unit shall bear a permanent label with the manufacturer's name or logo, city, state, model/series, and following statement: "Miami-Dade County Product Control Approved", unless otherwise noted berein.
RENEWAL of this NOA shall be considered after a renewal application has been filed and there has been no change in the applicable building code negatively affecting the performance of this product.
TERMINATION of this NOA will occur after the expiration date or if there has been a revision or change in the materials, use, and/or manufacture of the product or process. Misuse of this NOA as an endorsement of any product, for sales, advertising or any other purposes shall automatically terminate this NOA. Failure to comply with any section of this NOA shall be cause for termination and removal of NOA.
ADVERTISEMENT: The NOA number preceded by the words Miami-Dade County, Florida, and followed by the expiration date may be displayed in advertising literature. If any portion of the NOA is displayed, then it shall be done in its entirety.
INSPECTION: A copy of this entire NOA shall be provided to the user by the manufacturer or its distributors and shall be available for inspection at the job site at the request of the Building Official. This NOA renews and revises NOA \#14-0715.04 and consists of this page 1, evidence page E-1, as well as approval document mentioned above.
The submitted documentation was reviewed by Carlos M. Utrera, P.E.

NOA No 19-0925.02

MIAMI-DADE COUNTY


Expiration Date: September 23, 2024
Approval Date: November 31, 2019
Page 1

## 7.3 - MIAMI-DADE COUNTY continued

Perma R Products, Inc.

## NOTICE OF ACCEPTANCE: EVIDENCE SUBMITTED

1. Evidence submitted under previous NOA's
A. DRAWINGS "Submitted under NOA \#14-0715.04"
2. Drawing No. SB-Rev7, titled "Logix Standard Forms", sheet 1 of 1, prepared by Logix Insulated Concrete Forms, dated 09/16/2014, signed and sealed by Christopher W.C. Bowness, P.E.
B. TESTS "Submitted under NOA \#14-0715.04"

|  | Report | Test | Date | Signature |
| :---: | :---: | :---: | :---: | :---: |
| 1. | RJ3526-1 Rev. 1 | ASTM D1929 | 10/23/14 | C. Bowness, P.E. |
| 2. | RJ3526-2 Rev. 1 | ASTM D1929 | 10/23/14 | C. Bowness, P.E. |
|  | "Submitted under NOA \# 03-0319.01" |  |  |  |
|  | Report | Test | Date | Signature |
| 3. | RAD-3015 | ASTM C303 | April 2002 | J. D. Waldman |
| 4. | RAD-3015 | ASTM C518 | April 2002 | J. D. Waldman |
| 5. | RAD-3015 | ASTM E96 | April 2002 | J. D. Waldman |
| 6. | RAD-3015 | ASTM C272 | April 2002 | J. D. Waldman |
| 7. | RAD-2725 | ASTM D1929 | Feb 2001 | M. L. Zieman. |
| 8. | UL R-7503 | ASTM E84 | 06/18/98 | No signature. |
| 9. | UL R-7503 | ASTM E84 | 06/18/98 | No signature. |
| 10. | ETL 3050535 | ASTM G21 | 03/17/04 | S. J, Emermas, P.E. |

C. CALCULATION

1. None.
D. QUALITY ASSURANCE
2. Miami-Dade Department of Regulatory and Economic Resources (RER)
E. MATERIAL CERTIFICATION
3. None.
F. STATEMENTS
4. Statement letter of code conformance to $6^{\text {th }}$ edition (2017) FBC and of no financial interest issued by Building Drops, Inc., dated $09 / 27 / 2019$, signed and sealed by Hermes E. Norero, P.E.


Carlos M. Utrera, P.E. Product Control Examiner NOA No 19-0925.02
Expiration Date: September 23, 2024
E-1 Approval Date: November 31, 2019

## 7.3 - MIAMI-DADE COUNTY continued



## 7.4 - CITY OF NEW YORK - MEA (MATERIALS \& EQUIPMENT ACCEPTANCE)



## Report of Materials and Equipment Acceptance Division

Pursuant to Administrative Code Section 27-131, the following equipment or material has been found acceptable for use subject to the terms and conditions contained herein.

MEA 273-04-M

| Manufacturer: | Logix Insulated Concrete Forms Ltd., <br> Cobourg, Ontario, Canada K9A 4J9. |
| :--- | :--- |
| Trade Name(s): | Logix. | | Froduct: | Fire rated exterior insulation concrete forms wall assembly <br> for combustible construction. |
| :--- | :--- |
| Pertinent Code Section(s): | 27-297, 27-107, 27-133. |

Description: The Logix Insulated Concrete Forms are stay-in-place concrete forms for reinforced concrete wall systems. The wall system shall be constructed using a minimum $1 / 2$ inch thick gypsum drywall to achieve the required fire resistance rating, and installed as shown in Figure 1.

| Form Size (Wall Thickness) | Fire Rating |
| :---: | :---: |
| $4^{\prime \prime}$ | 2 hours |
| $6.25^{\prime \prime}$ | 3 hours |
| $8^{\prime \prime}$ and larger | 4 hours |

## 7.4 - CITY OF NEW YORK - MEA continued



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Figure 1. Logix Insulated Concrete Form wall system

1. Insulated Concrete Forms - Standard form units comprised of two $48^{\prime \prime} \times 16^{\prime \prime} \times 2.75^{\prime \prime}$ thick expanded polystyrene (EPS) panels linked by polypropylene webs spaced at $8^{\prime \prime}$ on center. The widths of the wall cavity are $4^{\prime \prime}, 6.25^{\prime \prime}$, and $10^{\prime \prime}$. Height adjusters consist of $24^{\prime \prime}$ long, by $4^{\prime \prime}$ high, by $2.75^{\prime \prime}$ thick flat EPS panels. End caps are $16^{\prime \prime}, 2.75^{\prime \prime}$ thick and range in widths are $4^{\prime \prime}, 6.25^{\prime \prime}, 8^{\prime \prime}$ and $10^{\prime \prime}$. For a complete listing of products visit the Logix website, www.logixicf.com. Logix ICF's bear the Warnock Hersey certification mark.
2. Steel Reinforcement - steel reinforcement shall be placed as per the Logix ICF Product Manual, or as per local engineering design and building code requirements.
3. Normal Weight Concrete $-145 \pm 5 \mathrm{lb} / \mathrm{ft}^{3}$ density, 2900 psi compressive strength.
4. Gypsum Board __Classified or unclassified $1 / 2^{"}$ thick, $48^{\prime \prime}$ wide gypsum wallboard fastened to flanges of polypropylene webs with $1.5^{\prime \prime}$ long drywall screws spaced on center $12^{\prime \prime}$ vertically and $16^{\prime \prime}$ horizontally. Minimum weight 1.6 psf. Joints covered with joint compound. Screwheads covered with joint compound.

Terms and Conditions - The above described wall assembly consisting of exterior concrete form and other components be accepted as having fire resistance classification listed above for combustible construction only, when installation complies with the applicable New York City Codes, Rules and Regulations and in particular with Section 27-297A, Tables 3-4, and 4-2 of the Building Code, for 1, 2 or 3 family, when interior and exterior of the concrete form is covered with accepted one hour fire rated material.

This acceptance does not include structural adequacy of wall design, which must be certified by a P.E., or R.A. for particular structures for compliance with the Building Code prior to plan examination by department engineers.

All shipments and deliveries of such materials shall be accompanied by a certificate or label certifying that the materials shipped or delivered are equivalent to those tested and acceptable for use, as provided for in Section 27-131 of the Building Code.

Final Acceptance

## All documents are downloadable at logixicf.com

## 7.5 - NON-COMBUSTIBLE CONSTRUCTION (I-CODES)

## Intertek ETL SEMKO

February 2, 2006
Francis Roma
Logix Insulated Concrete Forms Ltd.
327-801 Klahanie Drive
Port Moody, BC V3H 5K4
Dear Mr. Roma,
RE: Installation of Logix ICF in Non-Combustible Construction, Project \# 3091401

## INTRODUCTION

Intertek Testing Services NA Ltd. (Intertek) has reviewed, at the request of Logix Insulated Concrete Forms (ICF) Ltd., the requirements for Non-Combustible Construction as it relates to Insulated Concrete Forms (ICFs) under the 2003 International Building Code (IBC). This evaluation is based on past test reports, and Logix ICF Ltd. current application to ICC-ES to include multi-storey construction.

## STANDARDS AND CRITERIA

- 2003 International Building Code
- ICC-ES AC12 "Acceptance Criteria for Foam Plastic Insulation"


## EVALUATION

Section 3.3 of ICC-ES AC12 states that in some instances foam plastic can be permitted where non-combustible materials are required if conditions of the 2003 IBC, Section 2603.5 are met. This section has been summarized below, and evidence provided to demonstrate how Logix ICF complies for use in non-combustible construction.

1) 2603.5.1 Fire Resistance rated Walls: Where the wall is required to have a fireresistance rating, data based on tests conducted in accordance with ASTM E119 shall be provided.


#### Abstract

This report is for the exclusive use of Intertek's Client and is provided pursuant to the agreement between Intertek and its Client. Intertek's responsibility and liability are limited to the terms and conditions of the agreement. Intertek assumes no liability to any party, other than to the Client in accordance with the agreement, for any loss, expense or damage occasioned by the use of this report. Only the Client is authorized to copy or distribute this report and then only in its entirety. Any use of the Intertek name or one of its marks for the sale or advertisement of the tested material, product or service must first be approved in writing by Intertek. The observations and test results in this report are relevant only to the sample tested. This report by itself does not imply that the material, product, or service is or has ever been under an Intertek certification program.


## 7.5 - NON-COMBUSTIBLE CONSTRUCTION (I-CODES) continued

Logix Insulated Concrete Forms Ltd.
Project \# 3091401

February 2, 2006
Page 2 of 3

The Logix ICFs achieved a 3 hour fire resistance rating when tested by Intertek in Intertek Test Report 3020964(d) dated June 2, 2004. A further study was conducted in which, the Intertek Letter dated November 11, 2003 showed that the presence of plastic ties in the concrete would not affect the ability of the wall to achieve a fire resistance rating of up to 4 hours.

## 2) 2603.5.2 Thermal Barrier: Any foam plastic insulation shall be separated from the building interior by a thermal barrier meeting the provisions of Section 2603.4.

Section 2603.4 requires that the interior of a building be separated from the foam plastic by an approved thermal barrier of $1 / 2$ inch ( 12.7 mm ) gypsum wallboard or equivalent thermal barrier that will limit the average temperature rise of the unexposed surface to not more than $250^{\circ} \mathrm{F}\left(120^{\circ} \mathrm{C}\right)$ after 15 minutes of fire exposure. The thermal barrier must also be installed in a manner that will remain in place for 15 minutes based on UL1715 (UBC Standard 26-3).

ASTM E119 testing per Intertek Test Report 3020964(d) was conducted using a $1 / 2$ inch gypsum wallboard, and results showed that the temperature rise after 15 minutes was less than $60^{\circ} \mathrm{F}$ on the unexposed side.

A standard room fire test per Intertek Test Report 3020964(a) was also conducted in accordance with UBC Standard 26-3, and results showed that the $1 / 2$ inch gypsum wallboard remained intact.
3) 2603.5.3 Potential Heat: The potential heat of the foam plastic insulation shall be determined by tests conducted in accordance with NFPA 259.

One of the polystyrene beads used in Logix ICF are Huntsmen Grade 40 and 54, for which Southwest Research Institute conducted testing per NFPA 259 and have reported in SwRI Project No. 01.03049.01.303. Results showed potential heat ratings of 17,293 Btu/lb and 17,269 Btu/lb for Grade 40 and 54 respectively.

## 4) 2603.5.4 Flame Spread and Smoked Developed Indexes: Foam plastic insulation shall have a flame spread index of 25 or less and a smoke-developed index of 450 or less as determined in accordance with ASTM E84.

Flame Spread and Smoke Developed indexes have been obtained for Huntsmen Grade 40 and 54, one of the main polystyrene beads used in Logix ICF. These results are reported in Underwriters Laboratories Inc. Test Report 96RT6559, which show that various densities of Huntsmen polystyrene beads all achieve flame spread index ratings less than 25 and smoke-developed indices below 450 when tested in accordance to UL 723.

All documents are downloadable at logixicf.com

## 7.5 - NON-COMBUSTIBLE CONSTRUCTION (I-CODES) continued

## 5) 2603.5.5 Test Standard: The wall assembly shall be tested in accordance with and comply with the acceptance criteria of NFPA 285.

Testing to NFPA 285 is done on the finished wall assembly which includes the cladding (ex. Exterior Insulation and Finish System (EIFs)). This is a test that is primarily done by the cladding manufacturers to show conformance to NFPA 285 per the requirements of Section 3.3.2.1 and 3.3.2.2 of ICC-ES AC12. This is beyond the scope for an ICF manufacturer.

## 6) 2603.5.6 Label Required: The edge or face of each piece of foam plastic insulation shall bear the label of an approved agency.

Logix ICFs are manufactured under a third party inspection and listing program by Intertek, and all complying Logix ICF are marked with the Intertek - Warnock Hersey Certification Mark.

Each ICF is labeled with the following information: Company Name \& Contact Information, Manufacturer's Location, Product Description, Complying Test Standards, Warnock Hersey Certification Mark, and Traceability Information (operator name, date, time).

## 7) 2603.5.7 Ignition: Exterior walls shall not exhibit sustained flaming when tested in accordance with NFPA 268.

This section lists a few exceptions that result in the foam plastic insulation not requiring testing in accordance to NFPA 268. Logix ICFs meet the exceptions as a thermal barrier ( $1 / 2$ " gypsum wallboard) complying with Section 2603.4 is used.

## CONCLUSION

It is Intertek's professional opinion after reviewing Section 2603.5 of the 2003 IBC and the evidence shown above, that the Logix ICF meets the requirements for noncombustible construction for exterior walls of buildings of Type I, II, III or IV construction.

If you have any questions, please do not hesitate to contact us at 604-520-3321.
intertek testing services na lid. Warnock Hersey


Enclosure

## 7.6 - VAPOR BARRIER (I-CODES)

The following evaluation report, although evaluated to the Canadian Codes, determines the permeance value of Logix. (Both l-codes and Canadian Codes determines permeance in accordance with ASTM E96)

The permeance value, as per the report, is noted as
$36 \mathrm{ng} / \mathrm{Pa}-\mathrm{s}-\mathrm{m}^{2}$ (or 0.63 perms), which meets the requirement as a vapor retarder/barrier, according to the l-codes.

## All documents are downloadable at logixicf.com

## 7.6 - VAPOR BARRIER (I-CODES) continued

## 1 Introduction

Intertek Testing Services NA Ltd. (Intertek) has conducted an engineering evaluation for Logix Insulated Concrete Forms Ltd., on Logix ICF, to evaluate the vapor permeance properties of the product. The evaluation was conducted to determine if Logix ICF meets the 2005 National Building Code (NBC) for use as a vapor barrier.

## 2 Sample Description

Logix ICF consists of rigid interlocking expanded polystyrene (EPS) foam plastic boards that serve as permanent formwork for reinforced concrete, exterior and interior walls, and foundation and retaining walls.

## 3 Reference Documents

- 2005 National Building Code (NBC)
- ASTM E96/96M-05, Standard Test Methods for Water Vapor Transmission of Materials (ASTM E96)
- Intertek Test Report 3048347 dated October 14, 2003
- Intertek Letter dated January 6, 2005


## 4 Evaluation Method

Vapor barrier properties and installation are described in detail in Section 5.5.1.2 of the 2005 NBC. These details are summarized below:

1) The vapor barrier shall have sufficiently low permeance and shall be positioned in the building component or assembly so as to
a) minimize moisture transfer by diffusion, to surfaces within the assembly that would be cold enough to cause condensation at the design temperature and humidity conditions, or
b) reduce moisture transfer by diffusion, to surfaces within the assembly that would be cold enough to cause condensation at the design temperature and humidity conditions, to a rate that will not allow sufficient accumulation of moisture to cause deterioration or otherwise adversely affect any of
i. the health or safety of building users,
ii. the intended use of the building, or
iii. the operation of building services.
2) Coatings applied to gypsum wallboard to provide required resistance to vapour diffusion shall conform to the requirements of Sentence (1) when tested in accordance with CAN/CGSB-1.501-M, "Method for Permeance of Coated Wallboard."

## 7.6 - VAPOR BARRIER (I-CODES) continued

Logix Insulated Concrete Forms Ltd.
January 30, 2007
Project No. 3109888-R1
Revised: January 31, 2007
Page 3 of 4
3) Coatings applied to materials other than gypsum wallboard to provide required resistance to vapor diffusion shall conform to the requirements of Sentence (1) when tested in accordance with ASTM E96, "Water Vapor Transmission of Materials" by the desiccant method (dry cup).

Vapor Barrier materials are further discussed in Section 9.25.4.2 of the 2005 NBC under Sentence (1) which is summarized below:

1) Vapor barriers shall have a permeance not greater than $60 \mathrm{ng} / \mathrm{Pa}-\mathrm{s}-\mathrm{m} 2$ measured in accordance with ASTM E96, "Water Vapor Transmission of Materials" by the desiccant method (dry cup).

Logix ICF fall under Sentence (3) of Section 5.5.1.2 of the 2005 NBC and have been tested by Intertek in accordance with ASTM E96 using the desiccant method. The results were summarized in Intertek Test Report 3048347 dated October 14, 2003 and showed that a 1-inch Logic ICF had a water permeance of $100 \mathrm{ng} / \mathrm{Pa}-\mathrm{s}-\mathrm{m}^{2}$. In the field, Logic ICF is installed with a 2.75 -inch thickness and thus the calculated water permeance at this thickness is $36 \mathrm{ng} / \mathrm{Pa}-\mathrm{s}-\mathrm{m}^{2}$. The detailed calculations are shown in Intertek Letter dated January 5, 2005. Based on these results, Logic ICF meets the requirements of Section 9.25.4.2, Sentence (1) of the 2005 NBC and can be installed without the use of a vapor barrier.

## 5 Conclusion

Intertek has conducted an engineering evaluation for Logix Insulated Concrete Forms Ltd., on Logix ICF, to determine if the Logic ICF meets the 2005 National Building Code as a vapor barrier. The analysis, per Section 4 above, showed that Logix ICF meets the water permeance requirements and can be installed without a vapor barrier.

INTERTEK TESTING SERVICES NA LTD.

Reported by:


Matt Lansdowne, EIT
Engineer, Building Products

Reviewed by:


Kab Kooner, EIT
Team Leader, Engineering Services Canada

## All documents are downloadable at logixicf.com

## 7.7 - LEED V4 EVALUATION

## TECHNICAL BULLETIN <br> No. 37-053014 <br> LEED v4 BD+C for Logix <br> (US \& Canada)

POTENTIAL LEED POINTS CONTRIBUTION WITH LOGIX ${ }^{1}$

| Sustainable Sites | Applicable <br> Building <br> Types | Maximum Points <br> Contribution | Comments |
| :--- | :---: | :---: | :--- |
| Protect or Restore Habitat | All | 2 (1 for healthcare) | Although the points may not apply to LOGIX, <br> wall bracing for LOGIX is one of a combination of <br> actions that, together with other procedures, can <br> result in proper protection or restoration <br> of natural areas around the job site. <br> LOGIX is typically placed within the building <br> perimeter. This type of assembly avoids <br> disturbance to existing natural areas and keeps <br> construction activity close to the building <br> perimeter. |


| Energy \& Atmosphere | Applicable <br> Building <br> Types | Maximum Points <br> Contribution | Comments |
| :--- | :---: | :---: | :--- |
| Minimum Energy <br> Performance | All | $\mathrm{n} / \mathrm{a}$ <br> (required) | The continuous insulation and air barrier <br> properties of Logix can help meet required <br> minimum levels of efficiency for the building. |
| Optimize Energy <br> Performance | All | 18 except Schools <br> and Healthcare (16 <br> for Schools, 20 for <br> Healthcare) | The continuous insulation and air barrier <br> properties of Logix can help achieve the levels <br> of energy performance that go beyond the <br> prerequisite standard. |


| Material \& Resources | Applicable <br> Building <br> Types | Maximum Points <br> Contribution | Comments |
| :--- | :---: | :---: | :--- |
| Construction and <br> Demolition Waste <br> Management Planning | All | n/a <br> (required) | Logix products produce little waste compared to <br> wood, which should ease the waste management <br> planning. In addition, EPS recycling programs can <br> be implemented as part of the waste management <br> planning. |
| Building Life-cycle Impact <br> Reduction | All |  |  |
| Can help contribute 3 points under "Option 4. <br> Whole-Building-Life-Cycle Assessment." <br> The high energy efficient walls Logix creates <br> contributes to the reduction of a building's impact <br> on global warming. |  |  |  |
| Building Product Disclosure <br> \& Optimization - <br> Environmental Product <br> Declarations. | All |  | Can help contribute 1 point under "Option 1. <br> Environmental Product Declaration (EPD)." Logix <br> uses EPS which carries EPD documents, which <br> conform to ISO 14025. |
| Building Product Disclosure <br> \& Optimization - Sourcing <br> of Raw Materials. | All | 2 | Logix products are made with up to 10\% recycled <br> pre-consumer EPS. |
| Building Product Disclosure <br> \& Optimization - Material | All | 1 | Contributes to 1 point under "Option 3. Product <br> Manufacturer Supply Chain Optimization." |
| Ingredients. |  |  |  |

## 7.7 - LEED V4 EVALUATION continued

| TECHNICAL BULLETIN | LEED v4 BD+C for Logix |
| ---: | :--- |
| No.37-053014 | (US \& Canada) |


| Material \& Resources | Applicable <br> Building <br> Types | Maximum Points <br> Contribution | Comments |
| :--- | :---: | :---: | :--- |
| Construction \& Demolition <br> Waste Management | All | 2 | Programs can be put in place to recycle EPS from <br> job sites. EPS is also light in weight, and produces <br> less waste than wood products. |


| Indoor Environmental Quality | Applicable Building Types | Maximum Points Contribution | Comments |
| :---: | :---: | :---: | :---: |
| Minimum Acoustic Performance | Schools | N/a (required) | Logix can help increase the acoustical performance of wall and ceiling assemblies. |
| Low-emitting Materials | All | 3 | Logix Platinum is made with BASF Neopor, which is Greenguard Certified. In addition, the EPS used for Logix has been tested to show no signs of harmful emissions. |
| Thermal Comfort | All except Core \& Shell | 1 | Logix offers continuous insulation in wall and ceiling assemblies, and is made with BASF Neopor, which offer the highest thermal value of any EPS material. |
| Acoustic Performance | All except Core \& Shell | 1 | Logix can contribute to the STC ratings of wall and ceiling assemblies. STC testing of various wall assemblies have been conducted with Logix. |

${ }^{1}$ The total LEED point contribution from Logix is a best estimate based on available information and test data. The actual LEED point contribution may change based on project specifics, and should be determined by a LEED Accredited Professional for each project seeking LEED accreditation.

For more information about the LEED green building rating system visit www.usgbc.org or www.cagbc.org.

## 7.8 - QAI FIRE RESISTANCE RATING

Standards: ASTM E119-"Standard Test M ethods for Fire Tests of Building Construction and M aterials";

CAN/ULC S101 - "Standard M ethods of Fire Endurance Tests of Building Construction and M aterials"

|  | Rating | Product <br> Density | Maximum <br> Cavity Width | Maximum Panel <br> Thickness |
| :---: | :---: | :---: | :---: | :---: |
| ASTM E119/ | 2-Hour | 1.35 pcf | 4 inches | $23 / 4$ inches |
| CAN/ULC 5701 | 3-Hour | 1.35 pcf | $61 / 8$ inches | $23 / 4$ inches |
| Ratings: | 4-Hour | 1.35 pcf | 8 inches | $23 / 4$ inches |

Structural Rating at above durations for concrete wall at structural design load.


Assembly Details:

1. Insulated Concrete Forms - Standard forms made of two $16^{\prime \prime} \times 48^{\prime \prime}$ by $2.75^{\prime \prime}$ thick expanded polystyrene (EPS) block panels connected by polypropylene detail webs at 8" O.C. The minimum width of the cavity is $4^{\prime \prime}$ as shown in the ratings table above (rating depends on cavity thickness).
2. Reinforcing Steel - No. 4 steel reinforcing bars placed horizontally in each course and vertically at 16" O.C. along centerline of wall cavity thickness.
3. Sand-Limestone Concrete - 145 +/- 5 pcf density, 2900 psi nominal compressive strength concrete.
4. Gypsum W allboard - M in. $1 / 2^{\prime \prime}$ thick, 1.5 psf minimum density, 48 " wide gypsum wallboard fastened to flanges of polypropylene webs with $2^{\prime \prime}$ long drywall screws at $16^{\prime \prime}$ horizontally and vertically. Joints covered with joint compound, covered with joint tape, and covered with an additional coat of joint compound. Screw heads covered with joint compound.

## 7.9 - QAI LISTING REPORT

## BUILDING PRODUCTS LISTING PROGRAM

| Class: | Insulated Concrete Forms (ICF) |
| :---: | :---: |
| Customer: | LOGIX Insulated Concrete Forms, Ltd. |
| Location: | 9242 Pinetree Place, Whistler, BC, Canada, V0N 1B9 |
| Website: | www.LOGIXicf.com |
| Listing No. | B1031-1 |
| Effective Date: | September 27, 2010 |
| Last Revised: | May 27, 2014 |
| Expires: | N/A |
| Product: | LOGIX Insulated Concrete Forms (ICF) |
| Standard(s): | ASTM E2634 "Standard Specification for Flat Wall Insulating Concrete Form (ICF) Systems". |
|  | CAN/ULC S717.1 "Standard for Flat Wall Insulating Concrete Form (ICF) Systems". |
|  | CAN/ULC S701 "Thermal Insulation, Polystyrene, Boards and Pipe Covering". |
|  | CAN/ULC S 102.2 "Standard Method of Test for Surface Burning Characteristics of Flooring, Floor Coverings, and Miscellaneous Materials and Assemblies". |
|  | ASTM C578 "Standard Specification for Rigid, Cellular Polystyrene Thermal Insulation". |
|  | ASTM E84 - "Standard Test Method for Surface Burning Characteristics of Building Materials". |
|  | UBC 26-3 "Room Fire Test Standard For Interior of Foam Plastic Systems". |
|  | CAN/ULC-S101 "Standard Methods of Fire Endurance Tests of Building Construction and Materials". |
|  | ASTM E119 / ANSI / UL 263 "Standard Test Methods for Fire Tests of Building Construction and Materials". |
| Label: | Product is marked with labels supplied by LOGIX Insulated Concrete Forms, Ltd. The label includes the manufacturer's name, trademark, or other recognized symbol of identification, the product model designation, month and year of manufacture or equivalent, QAI logo with the 'US' and "C" identifier, and CAN/ULC S701 Type 2, ASTM C578 Type II, ASTM E84 FSI and SDI Rating, and CAN/ULC S102.2 FSI and SDI Rating. Labels are applied to palletized finished products to ensure visibility on the jobsite. |
| Ratings: | The following outlines LOGIX ICF test results determined in accordance with the noted standards. |


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| :--- | :--- | :--- |

## 7.8 - QAI LISTING REPORT continued

LOGIX ICF Fastener Resistance Ratings

| FASTENER | ALLOWABLE WITHDRAWAL |  | ALLOWABLE LATERAL <br> SHEAR |  |
| :---: | :---: | :---: | :---: | :---: |
|  | lbs | $\mathbf{k g}$ | $\mathbf{l b s}$ | $\mathbf{k g}$ |
| \#ength Coarse <br> Lenread Drywall <br> Screw | 23 | 10 | 59 | 26 |

LOGIX ICF Type 2 Specifications per CAN/ULC S701

| PROPERTY | LOGIX SPECIFICATION |
| :---: | :---: |
| Thermal Resistance <br> $\mathrm{m}^{2} *^{\circ} \mathrm{C} / \mathrm{W}$ at 25 mm Thickness | Minimum 0.70 |
| Water Vapour Permeance <br> $\mathrm{Ng} / \mathrm{Pa}^{*} \mathrm{~s}^{*} \mathrm{~m}^{2}$ at 25 mm Thickness <br> \% Linear Shability | Maximum 200 |
| Flexural Strenge <br> kPa | Maximum 1.5 |
| Water Absorption <br> \% Volume | Minimum 240 |
| Compressive Strength <br> kPa at $10 \%$ Deformation | Maximum 4.0 |
| Limiting Oxygen Index <br> $\%$ | Minimum 110 |

LOGIX ICF Type II Specifications per ASTM C578

| PROPERTY | LOGIX SPECIFICATION |
| :---: | :---: |
| Compressive Resistance <br> psi at Yield or 10\% Deformation | Minimum 15.0 |
| Thermal Resistance <br> $\mathrm{F}^{2} \mathrm{ft}^{2} \mathrm{~h} /$ Btu at 1.00 Inch Thickness | Minimum 4.0 |
| Flexural Strength <br> psi | Minimum 35.0 |
| Water Vapor Permeance <br> Perms at 1.00 Inch Thickness | Maximum 3.5 |
| Water Absorption <br> \% Volume | Maximum 3.0 |
| Dimensional Stability <br> \% Change Dimensions | Maximum 2.0 |
| Oxygen Index <br> \% Volume | Minimum 24.0 |
| Density <br> lbs/ft ${ }^{3}$ | Minimum 1.35 |

LOGIX ICF Surface Burning Characteristics per CAN/ULC S102.2

| LOGIX <br> COMPONENT | DENSITY | MAXIMUM <br> THICKNESS | FLAME <br> SPREAD <br> INDEX (FSI) | SMOKE <br> DEVELOPED <br> INDEX (SDI) |
| :---: | :---: | :---: | :---: | :---: |
| Expanded <br> Polystyrene <br> (EPS Panel) | $22-29$ | 100 mm <br> Maximum | $\leq 210$ | $\geq 500$ |

LOGIX ICF Surface Burning Characteristics per ASTM E84 ${ }^{1}$

| LOGIX | DENSITY | MAXIMUM | FLAME | SMOKE |
| :--- | :---: | :---: | :---: | :---: |

## 7.8 - QAI LISTING REPORT continued

| COMPONENT | THICKNESS | SPREAD <br> INDEX (FSI) | DEVELOPED <br> INDEX (SDI) |  |
| :---: | :---: | :---: | :---: | :---: |
| Expanded <br> Polystyrene <br> (EPS Panel) | $1.35-1.80$ <br> $\mathrm{lbs} / \mathrm{ft}^{3}$ | 4.0 Inches <br> Maximum | $\leq 75$ | $\leq 450$ |

${ }^{1}$ Ceiling Measurement Only. This measurement is conducted through determination of flame spread index and smoke developed index with the removal of any contribution of molten materials ignited on the floor of the tunnel assembly.

## LOGIX UBC 26-3 Configuration

Meets requirements with $1 / 2$ inch thickness gypsum fastened with $21 / 4$ inch length standard drywall screws at 12 inch on center. Fasteners must be anchored into LOGIX ICF web ties.

QAI Design Listing B1031-1 LOGIX Insulated Concrete Form (ICF) - CAN/ULC
S101 / ASTM E119
Load Bearing Fire-Resistance-Rated Wall Assembly ${ }^{1}$

| ASSEMLY <br> RATING <br> (Hours) | MINIMUM CONCRETE <br> CORE THICKNESS <br> (MM) | MINIMUM CONCRETE <br> CORE THICKNESS <br> (INCHES) |
| :---: | :---: | :---: |
| 2 | 102 | 4 |
| 3 | 159 | 6.25 |
| 4 | 204 | 8 |

(See pdf Attachment)

\begin{tabular}{|c|c|c|}
\hline NO. \& COMPONENT \& DESCRIPTION <br>
\hline ren

1 \& Interior Sheathing \& | Minimum $1 / 2$ inch ( 12 mm ) thickness ASTM C1396 listed gypsum wall board, installed with 51 mm (2 inch) length drywall screws spaced at 406 mm ( 16 inches) on center horizontally and vertically. |
| :--- |
| For $61 / 4$ inch concrete LOGIX ICF product used in load bearing fire-resistance-rated wall assemblies, listed 16 mm ( $5 / 8 \mathrm{inch}$ ) thickness Type X gypsum wall board complying with ASTM C1396 is required fastened as noted above. |
| Gypsum is required to be taped and mudded per industry standard and the applicable model code. | <br>

\hline 2 \& | Expanded |
| :--- |
| Polystyrene (EPS) Insulation | \& LOGIX ICF component $70 \mathrm{~mm}\left(2^{3 / 4}\right)$ inch thickness Type 2 (CAN/ULC S701) / Type II (ASTM C578) QAI certified expanded polystyrene thermal insulation. LOGIX ICF EPS panels have interlocking teeth to allow stacking onsite to create the forming wall. <br>

\hline 3 \& Web Ties \& LOGIX polypropylene web tie component, spaced at 203 mm ( 8 inches) on center spacing through LOGIX ICF. Web ties can be stacked or staggered vertically during installation (staggered web tie system shown). <br>
\hline 4 \& Concrete Core \& Minimum core as noted in Table above of 20 MPa ( $2,900 \mathrm{psi}$ ) compressive strength concrete. Steel reinforcing, while not shown, is approved for use. Rebar addition is to be designed and approved by a registered design professional, or authority having jurisdiction in accordance with the applicable code <br>
\hline
\end{tabular}

## 7.8 - QAI LISTING REPORT continued

|  |  | requirements. |
| :--- | :--- | :--- |
|  |  | Exterior claddings are approved for use with the <br> LOGIX ICF load bearing fire-resistance-rated wall <br> assemblies without negatively impacting the fire rating. |
| These exterior claddings include: brick veneer, stucco, |  |  |
| f | Exterior Cladding <br> (Not Shown) <br> fire rated exterior insulating finish systems where no <br> additional EPS is added, cultured stone, aluminum and <br> steel products. All exterior claddings are to be installed <br> with the applicable building code, and the <br> manufacturer's approved installation instructions. |  |

Note 1: The allowable load for LOGIX ICF Load Bearing Fire-Resistance-Rated Construction is to be determined by a registered design professional, or authority having jurisdiction in accordance with the applicable codes.

Note: $\quad$ Final acceptance of the product in the intended application is to be determined by the authority having jurisdiction.

Product is to be installed in accordance with the manufacturer's published installation instructions by qualified installing personnel.

The materials, products or systems listed herein have been qualified to bear the QAI Listing Mark under the conditions stated with each Listing. Only those products bearing the QAI Listing Mark are considered to be listed by QAI.

No warrantee is expressed or implied, and no guarantee is provided that any jurisdictional authority will accept the Listing found herein. The appropriate authorities should be contacted regarding the acceptability of any given Listing.

Visit the QAI Online Listing Directory located at www.qai.org for the most up to date version of this Listing and to validate that this QAI Listing is active.

Questions regarding this listing may be directed to info@qai.org. Please include the listing number in the request.

FORM History

| History Date | Version | Change Description | Reviewed By | Approved By |
| :--- | :--- | :--- | :--- | :--- |
| $04 / 17 / 2014$ | 3.0 | Added disclaimer to <br> form. | J. Johnson | K. Adamson |


| Effective Date: September 15, 2006 | QM0604 Draft Listing Page | Page 4 of 4 |
| :--- | :---: | :---: |

## 8.0 - SPECIFICATIONS \& REFERENCES

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## 8.1 - TECHNICAL SPECIFICATIONS

## LOGIX INSULATED CONCRETE FORMS MATERIAL PROPERTY DATA SHEET

This document is intended for general information purposes only regarding specifications for Logix Insulated Concrete Forms (herein referred to as Logix ICF). Technical specification sheet, as per Construction Specifications institute (CSI) formatting, can be downloaded at www.logixicf.com.

## 1 PRODUCT DESCRIPTION

- Logix ICF consists of two flame-resistant EPS boards separated by polypropylene webs.
- Logix ICF consists of solid form units (LOGIX Pro Forms) or knock-down forms (LOGIX KD Forms) or a combination of both Logix form and Logix KD forms, referred to as LOGIX Hybrid Forms.
- The EPS foam boards are a minimum 70 mm ( 2.75 inch) thick. Increased EPS foam boards are available by utilizing D-Rv insert panels, which provides additional thickness in increments of 50 mm (2 inch).
- The webs separate the EPS boards to form 102 mm ( 4 inch), 159 mm ( 6.25 inc ), 203 mm ( 8 inch ), 254 mm ( 10 inch ) and 305 mm ( 12 inch) cavities, which create the concrete wall thicknesses. With Logix Xtenders the concrete wall thickness can be increased to virtually any thickness.
- The webs are spaced every 203 mm ( 8 inch ) on centre horizontally and 406 mm ( 16 inch ) on centre vertically, and contain a 32 mm ( 1.25 inch) wide furring strip that extends the height of each ICF block. The furring strips shall facilitate fasteners for attachment of both exterior and interior finishes.
- A furring strip is located in the corners of corner forms. The furring strip consists of both a vertical and horizontal component. The vertical component extends nearly the full height of the form, extends a minimum of 64 mm ( 2.5 inches) from both sides of the corner, and a minimum of 5 mm ( 0.2 inches) thick. The horizontal component is a minimum 51 mm ( 2 inches) in height, extend a minimum of 152 mm (6 inches) from both sides of the corner, and a minimum of 5 mm ( 0.2 inches) thick.
- The webs facilitate rebar placement in accordance with CAN/CSA A23.1, and ACI 318


## 8.1 - TECHNICAL SPECIFICATIONS continued

## 2 LOGIX PRODUCTS

Logix manufactures both assembled and unassembled insulated concrete form units. Logix assembled forms, known simply as "Logix PRO", are delivered to the job site as assembled form blocks. Logix unassembled forms (or knock-down forms), known as "Logix KD", are delivered to the job site in components that make up the form blocks - the form panels and KD Connectors. Logix KD are assembled on the job site.

Below is a summary of the types of Logix and Logix KD forms available.
LOGIX (assembled form blocks)

|  | Description |
| :--- | :--- |
| Logix Pro | White in color |
| Logix Pro Platinum $^{3}$ | Grey in color. Offers higher R-value ${ }^{1}$ than Logix Pro. |
| Logix Pro TX | Logix Pro with termite resistant additive Preventol ${ }^{2}$. |
| Logix Pro Platinum ${ }^{3}$ TX | Logix Platinum with Preventol. |

LOGIX KD (unassembled form blocks)

|  | Description |
| :--- | :--- |
| Logix KD | White in color |
| Logix KD Platinum $^{3}$ | Grey in color. Offers higher R-value ${ }^{1}$ than LOGIX Pro. |
| Logix KD TX $^{\text {Logix }}$ KD Platinum ${ }^{3}$ TX | Logix Pro with termite resistant additive Preventol ${ }^{2}$. |
| Loginum with Preventol. |  |
| Notes: |  | Notes:

1. See Logix Design Manual, Section 8.5 for Logix R-values.
2. Preventol is an effective termite resistant additive.
3. Care should be taken to protect exposed foam surfaces from reflected sunlight and prolonged solar exposure until wall cladding or finish material is applied. Shade exposed foam areas, or remove sources of reflective surfaces, where heat buildup onto exposed foam might occur. For more information refer to BASF Technical Leaflet N-4 Neopor,
"Recommendations for packaging, transporting, storing and installing building insulation products made from Neopor EPS
foam." (The BASF Technical Leaflet is attached to every bundle of LOGIX Platinum forms delivered to a job site).

## 8.1 - TECHNICAL SPECIFICATIONS continued

CODE/CERTIFICATION APPROVALS

- QAI evaluation to IBC and IRC 2012
- Miami-Dade County Approval No.19-0925.02
- State of Florida Certification of Approval No.FL14469-R3
- Wisconsin Building Products Evaluation No. 20199000
- City of New York Materials and Equipment Acceptance - MEA 273-04-M
- QAI listed QM0503
- ASTM E2634, Standard Specification for Flat Wall Insulating Concrete Form (ICF) Systems
- ASTM C578, Standard Specification for Rigid, Cellular Polystyrene Thermal Insulation
- CAN/ULC S717, Standard for Flat Wall Insulating Concrete Form (ICF) Units - Material Properties
- CAN/ULC S701, Standard for Thermal Insulation, Polystyrene Boards


## 4 DESIGN/PERFORMANCE OF LOGIX ICF

A brief description of each test is outlined in the attached Appendix. Test reports are available upon request.

| Test Description | Result | Pass/Fail Criteria | Referenced Standard Test Method |
| :---: | :---: | :---: | :---: |
| $\begin{array}{\|l\|} \hline \text { R-Value (Thermal } \\ \text { Resistance) per inch (per } \\ 25.4 \mathrm{~mm} \text { ) } \\ \hline \end{array}$ | R 4.13 (RSI 0.72) | Min. R 4.00 (RSI 0.70) | ASTM C518 |
| Water Absorption | 0.18\% | Max. 3.0\% | ASTM D2842 |
| Water Vapor Presence | 100.0ng/Pa-s-m2 (1.74perm-in.) | Max. 201 ng/Pa-s-m2 (3.5perm-in.) | ASTM E96 |
| Compressive Strength | 165kPa (23.9psi) | Min. 104 kPa (15.0psi) | ASTM D1621 \& ASTM C165 |
| Flexural Strength | 365kPa (53.0psi) | Min. 240kPa (35.0psi) | ASTM C203 |
| Dimensional Stability Thermal \& Humid Aging | 0.5\% | Max. 2.0\% | ASTM D2126 |
| Density | $27.5 \mathrm{~kg} / \mathrm{m} 3$ (1.72pcf) | Min. $22 \mathrm{~kg} / \mathrm{m} 3$ (1.35pcf) | ASTM C1622 \& ASTM C303 |
| Dimensions | Min. length variation $=0.0 \%$ <br> Max. length variation $=0.4 \%$ <br> Min. width variation $=0.1 \%$ <br> Max. width variation $=0.4 \%$ <br> Min. thickness variation $=-0.3 \mathrm{~mm}$ <br> Max. thickness variation $=0.9 \mathrm{~mm}$ <br> Max. squareness $=3 \mathrm{~mm}$ | Min. -0.2\% <br> Max. 0.4\% <br> Min. -0.2\% <br> Max. 0.4\% <br> Max. -2 mm <br> Max. 4 mm <br> Max. 3mm | ASTM C303 |
| Limiting Oxygen Index | 29.1\% | Min. 24.0\% | ASTM D2863 |
| Formaldehyde Emission | No formaldehyde detected | N/A* | AATTC-112 |
| Fungi Resistance | No fungal growth detected | N/A* | ASTM G21 |
| Flame Spread Rating | <25 | N/A* | ASTM E84/CAN ULC S102 |

## 8.1 - TECHNICAL SPECIFICATIONS continued

LOGIX INSULATED CONCRETE FORMS GENERAL SPECIFICATIONS SHEET, CONT'D

| Test Description | Result | Pass/Fail Criteria | Referenced <br> Standard Test <br> Method |
| :--- | :--- | :--- | :--- |
| Smoke Developed Rating | < 450 | N/A* | ASTM E84/CAN ULC <br> S102 |
| Fire Endurance Test | See Fire Resistance Rating table | N/A* | ASTM E119/CAN <br> ULC S101 |
| Standard Room Fire Test | w/in acceptable limits | Met conditions required <br> for exposure to fire for 15 <br> minutes. | UBC 26-3/CAN ULC <br> 1715 |
| Concrete Pour-in-place | Observations of deflection <br> recorded. | N/A* | CCMC Masterformat <br> 03131 |
| Sound Transmission | STC 56 for 6.25" Logix wall system <br> (2 layers of 5/8" drywall \& 2x2 <br> wood strips on one side, $1 / 2^{\prime \prime}$ <br> drywall on the other side) <br> STC 50 for 4" Logix wall system <br> (1/2" drywall \& 2x2 wood strips on <br> one side, $1 / 2^{\prime \prime}$ drywall on the other <br> side). | N/A* | ASTM E90 |
| UPITT Toxicity | Pass | LC50 < 19.7g | University of <br> Pittsburgh Toxicity <br> Test |

*Code body or referenced test standard required reporting test results only - no Pass/Fail criteria specified.

## 8.1 - TECHNICAL SPECIFICATIONS continued

Bild Anything Better
LOGIX INSULATED CONCRETE FORMS GENERAL SPECIFICATIONS SHEET, CONT'D

TESTS CONDUCTED ON POLYPROPYLENE WEB

| Test Description | Result | US Requirements | Referenced Standard Test Method |
| :---: | :---: | :---: | :---: |
| Flammability | Flame Front Distance $=100 \mathrm{~mm}$ (4") <br> Avg. Linear Burn Rate $=17.9 \mathrm{~mm} /$ $\min (0.70 \mathrm{in} / \mathrm{min})$ | Max. linear burn rate = $40.0 \mathrm{~mm} / \mathrm{min}(1.57 \mathrm{in} / \mathrm{min})$ for Flame Front Dist. = 100 mm (4") | ASTM D635 |
| Smoke Density Rating | 19.1\% | Max. 75\% | ASTM D2843 |
| Average Lateral Fastener Resistance of Drywall Screws | 1.63kN (367lbs) | N/A* | ASTM D1761 |
| Average Withdrawal Fastener Resistance of Drywall Screws | 0.75 kN (169lbs) | N/A* | ASTM D1761 |
| Shear Strength of Polypropylene Web | 26.1MPa (37.9psi) | N/A* | ASTM D732, CCMC Masterformat 03131 |
| Average Tensile Strength of Polypropylene Web | 3.75 kN (842lbs) | N/A* | ASTM D638 |
| Average Withdrawal Resistance of Staples 1.59 mm 16 ga . | 105N (24lbs) | N/A* | ASTM D1761 (under cyclic temperatures) |
| Average Withdrawal <br> Resistance of Plane Shank <br> 1.5" long, 3/8" head | 155N (35lbs) | N/A* | ASTM D1761 <br> (under cyclic temperatures) |
| Average Withdrawal Resistance of Ring Shank 1.5" long, 3/8" head | 431N (97lbs) | N/A* | ASTM D1761 (under cyclic temperatures) |
| Average Withdrawal Resistance of Spiral Shank 1.5" long, 3/8" head | 135N (30lbs) | N/A* | ASTM D1761 (under cyclic temperatures) |
| Average Lateral Resistance of Staples 1.59 mm 16 ga . | 169N (38lbs) | N/A* | ASTM D1761 (under cyclic temperatures) |
| Average Lateral Resistance of Plane Shank 1.5" long, 3/8" head | 520N (117lbs) | N/A* | ASTM D1761 (under cyclic temperatures) |
| Average Lateral Resistance of Ring Shank 1.5" long, 3/8" head | 378N (85lbs) | N/A* | ASTM D1761 (under cyclic temperatures) |
| Average Lateral Resistance of Spiral Shank 1.5" long, 3/8" head | 200N (45lbs) | N/A* | ASTM D1761 (under cyclic temperatures) |

## 8.1 - TECHNICAL SPECIFICATIONS continued

Updated 12/10/19

LOGIX INSULATED CONCRETE FORMS GENERAL SPECIFICATIONS SHEET, CONT'D

| Test Description | Result | US Requirements | Referenced <br> Standard Test <br> Method |
| :--- | :--- | :--- | :--- |
| Average Withdrawal <br> Resistance of Corrosion <br> Resistance No.8-18 x 0.323 <br> HD x 1.5/8" | 567N (127lbs) | N/A* | ASTM D1761 |
| Average Withdrawal <br> Resistance of Corrosion <br> Resistance 6d (0.113" <br> shank x 0.267 HD x 2" <br> long) | 93N (21lbs) | N/A* |  |
| \#6 Coarse Drywall Screw, <br> 1-5/8" long** | 787N (177lbs) | N/A* | ASTM D1761 |
| \#6 Fine Drywall Screw, <br> 1-5/8" long** | 765N (172lbs) | N/A* | ASTM D1761 |
| 16ga. Staple, 1-1/2" long** | 124N (28lbs) | N/A* | ASTM D1761 |
| Galvanized Ringed <br> Wallboard Nail, 1-1/2" <br> long** | 462N (104lbs) | N/A* | ASTM D1761 |
| Hot-dipped Galvanized <br> Spiral Nail, 2" long** | 226N (51lbs) | N/A* | ASTM D1761 |
| \#8 Wood Screw, 2" long** | 920 N (207lbs) | N/A* | ASTM D1761 |
| \#8 Exterior Deck Screw, 2" <br> long** | $934 N$ (210lbs) | ASTM D1761 |  |
| \#10 Wood Screw, 2" <br> long** | A80N (198lbs) | AST1761 |  |

*Code body or referenced test standard required reporting test results only - no Pass/Fail criteria specified.
**Applicable to corner web only.
FIRE RESISTANCE RATING

| Form Size (Concrete Wall Thickness) | Rating with $1 / 2^{\prime \prime}$ drywall |
| :--- | :--- |
| $100 \mathrm{~mm}\left(4^{\prime \prime}\right)$ | 2 hrs |
| $159 \mathrm{~mm}\left(6.25^{\prime \prime}\right)$ | 3hrs (4hrs if $5 / 8^{\prime \prime}$ drywall used) |
| $203 \mathrm{~mm}\left(8^{\prime \prime}\right)$ and above | 4hrs |

*Bearing load applied to wall $=360,000 \mathrm{lbs}$ (360kips)

## 8.2 - MATERIAL SAFETY DATA SHEET

Safety Data Sheet - Expanded Polystyrene (EPS) in Logix ${ }^{\circledR}$ Insulated Concrete Forms

## SAFETY DATA SHEET

Safety Data Sheet - Expanded Polystyrene (EPS) in Logix ${ }^{\circledR}$ Insulated Concrete Forms

| SECTION 1 - IDENTIFICATION |  |
| :--- | :--- |
| Product identifier: | Logix ${ }^{\circledR}$ Insulated Concrete Forms, Logix ${ }^{\circledR}$ Pro Buck, Logix ${ }^{\circledR}$ XP-1 |
| Other means of <br> identification: | Logix ICF |
| Recommended use: | Stay-In-Place Insulated Concrete Forms |

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## 8.2 - MATERIAL SAFETY DATA SHEET continued

Safety Data Sheet - Expanded Polystyrene (EPS) in Logix ${ }^{\circledR}$ Insulated Concrete Forms

| SECTION 4 - FIRST AID MEASUREMENTS |  |
| :---: | :---: |
| Inhalation: | When hot-knifing vapors may cause irritation to nose and throat. Dizziness may occur in poorly ventilated areas when hot-knifing. Remove affected individual into fresh air and keep the person calm. If difficulties occur, seek medical attention. |
| Skin contact: | This material is not considered to be a skin irritant. In cases where irritation may occur to extra sensitive skin, wash with soap and water for several minutes. Get medical attention if skin irritation develops or persists. |
| Eye contact: | Flush eyes with water for several minutes. Get medical attention if eye irritation persists or particulates are difficult to remove from the eye. |
| Ingestion: | This material is not considered to be hazardous when ingested but may cause blockage of air passage if large pieces are ingested. Get medical attention and apply proper first aid for persons with air passage blocked. |
| Physical state: | Solid |
| Odour \& appearance: | Slight hydrocarbon odour, White in color |
| SECTION 5 - FIRE-FIGHTING MEASURES |  |
| Suitable extinguishing media: | Use water spray, dry chemical, foam or carbon dioxide to extinguish flames. |
| Special protective equipment and precautions for firefighters: | Firefighters should be equipped with self-contained breathing apparatus and turn-out gear. |
| Flash Point: | $175-185^{\circ} \mathrm{C}\left(347-365{ }^{\circ} \mathrm{F}\right)$, ASTM D3278 |
| Autoignition: | $285{ }^{\circ} \mathrm{C}\left(571{ }^{\circ} \mathrm{F}\right)$, DIN 51794 |
| Lower explosion limit: | 1.4 \% (V) (air) |
| Upper explosion limit: | 8.3 \% (V) (air) |
| Flammability: | Not highly (UN Test N. 1 (ready combustible solids)) |
| Self-ignition temperature: | Not self-igniting |
| Further information: | Fire gives off black smoke consisting of carbon monoxide ( $<10 \mathrm{ppm}$ ), carbon dioxide ( 500 ppm ), oxides of nitrogen ( 4 ppm ), including trace of amounts of pentane, aldehydes and keytones. Fire hazards increase with presence of ignition sources or high concentrations of dust from work sites. |

## 8.2 - MATERIAL SAFETY DATA SHEET continued

SNEA

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## 8.2 - MATERIAL SAFETY DATA SHEET continued


Safety Data Sheet - Expanded Polystyrene (EPS) in Logix ${ }^{\text {® }}$ Insulated Concrete Forms
Issue Date: Oct 30, 2018

| Vapour pressure: | $\mathrm{N} / \mathrm{A}$ |
| :--- | :--- |
| Vapour density: | $\mathrm{N} / \mathrm{A}$ |
| Solubility: | Insoluble in water. Soluble with materials containing primarily of hydrocarbons, <br> aldehydes, esters and amines. |
| Partition coefficient - n- <br> octanol/water: | $\mathrm{N} / \mathrm{A}$ |
| Viscosity: | $\mathrm{N} / \mathrm{A}$ |
| SECTION 10 - STABILITY AND REACTIVITY |  |
| Reactivity: | Products react to high temperatures and strong oxidizers. |
| Chemical stability: | Stable under normal use conditions. |
| Possibility of hazardous <br> reactions: | None. <br> Conditions to avoid:Avoid all sources of ignition, such as heat, sparks, open flame. <br> Unstable when exposed to high temperatures. Recommended maximum use <br> temperature of $60^{\circ} \mathrm{C}\left(166^{\circ} \mathrm{F}\right)$. |
| Incompatible materials: | Not compatible with materials containing primarily of hydrocarbons, aldehydes, esters <br> and amines. |
| Hazardous decomposition <br> products: | High heat or combustion produces black smoke consisting of carbon monoxide $(<$ <br> 10ppm), carbon dioxide $(500 \mathrm{ppm})$, oxides of nitrogen (4ppm), including trace of <br> amounts of pentane, aldehydes and keytones. |

SECTION 11 - TOXICOLOGICAL INFORMATION

| Primary route of entry: | Eyes, skin and inhalation. |
| :--- | :--- |
| Effects of Acute Exposure: | When hot-knifing material, vapors may cause irritation to eyes. |
| Eyes: | This material is not considered to be a skin irritant. Products may contain small <br> particulates of dust accumulated naturally from surrounding environment, which may <br> cause skin irritation with possible mild discomfort on extra sensitive skin. |
| Skin: | When hot-knifing vapors may be cause irritation to nose and throat. Dizziness may <br> occur in poorly ventilated areas when hot-knifing. |
| Inhalation: | Exposure to vapors may aggravate existing respiratory conditions, such as asthma, <br> bronchitis and inflammatory or fibrotic respiratory disease. |
| Effects of chronic <br> exposure: |  |

## SECTION 12 - ECOLOGICAL INFORMATION

Non-biodegradable.
SECTION 13 - DISPOSAL CONSIDERATIONS
Loose material can be vacuumed or swept and placed in disposal containers.
This material can be disposed of in accordance with local, state/provincial and federal regulations. This material is not considered a hazardous waste.

## 8.2 - MATERIAL SAFETY DATA SHEET continued

Safety Data Sheet - Expanded Polystyrene (EPS)
in Logix ${ }^{\text {I }}$ Insulated Concrete Forms

TO THE BEST OF OUR KNOWLEDGE THE INFORMATION CONTAINED HEREIN IS BELIEVED TO bE ACCURATE. HOWEVER, NEITHER THE ABOVE NAMED MANUFACTURER OR SUPPLIER NOR ANY OF ITS SUBSIDIARIES ASSUMES ANY LIABILITY WHATSOEVER FOR THE ACCURACY OR COMPLETENESS OF THE INFORMATION CONTAINED HEREIN. FINAL DETERMINATION OF SUITABILITY OF ANY MATERIAL IS THE SOLE RESPONSIBILITY OF THE USER. ALL MATERIALS MAY PRESENT UNKNOWN HAZARDS AND SHOULD BE USED WITH CAUTION. ALTHOUGH CERTAIN HAZARDS ARE DESCRIBED HEREIN, WE CANNOT GUARANTEE THAT THESE ARE THE ONLY HAZARDS THAT EXIST.

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## RECOMMENDED INDUSTRY PRACTICE FOR PLACING REINFORCING BARS*

## 1. Introduction

These recommendations for placing reinforcing bars are partially based upon the ACI Building Code.

## 2. General

Reinforcing bars should be accurately placed in the positions shown on the placing drawings and adequately tied and supported before concrete is placed, and secured against displacement within the tolerances recommended in Section 8.

Welding of crossing bars (tack welding) should not be permitted for assembly of reinforcement unless authorized by the Architect/Engineer.

## 3. Surface Condition of Reinforcement

At the time of concrete placement, all reinforcing bars should be free of mud, oil, or other deleterious materials. Reinforcing bars with rust, mill scale, or a combination of both should be considered as satisfactory, provided the minimum dimensions, weight, and height of deformations of a hand-wire-brushed test specimen are not less than the applicable ASTM specification requirements.

## 4. Bending

Reinforcing bars should not be bent or straightened in a manner that will injure the material. Bars with kinks or improper bends should not be used. Except for realignment of \#7 through \#18 rebar up to about $30^{\circ}$ bend and \#3 through \#6 rebar up to about a $45^{n}$ bend, no bars partially embedded in concrete should be field bent, except as shown on the project drawings or permitted by the Architect/Eingineer.

## 5. Spacing of Reinforcement

The clear distance berween parallel reinforcing bars in a layer should not be less than the nominal diameter of the bars, nor 1 in. Clear distance should also not be less than one and one-third times the nominal maximum size of the coarse aggregate, except if in the judgement of the Architect/Engineer, workability and methods of consolidation are such that concrete can be placed without honeycomb or voids.

Where parallel reinforcement is placed in two or more layers, the bars in the upper layers should be placed directly above those in the bottom layer with the clear distance between layers not less than I in.

Groups of parallel reinforcing bars bundled in contact, assumed to act as a unit, not more than four in any one bundle may be used only when stimrups or ties enclose the bundle. Bars larger than \#11 should not be
bundled in beams or girders. Individual bars in a bundle cut off within the span of flexural members should terminate at different points with at least 40 bar diameters stagger: Where spacing limitations and minimum clear cover are based on bar size, a unit of bundled bars should be treated as a single bar of a diameter derived from the equivalent total area.

In walls and slabs other than concrete joist construefion, the principal reinforcement should not be spaced farther apart than three times the wall or slab thickness. nor more than 18 in.

In spirally reinforced and tied columns, the clear distance between longitudinal bars should not be less than one and one-half times the nominal bar diameter, nor $71 / 2$ in.

The clear distance limitation between bats should also apply to the clear distance between a contact lap splice and adjacent splices or bars.

## 6. Splices in Reinforcement ${ }^{* *}$

### 6.1 General

Splicing of reinforcing bars should be either by lapping, mechanical connections, of by welding.

Splices of reinforcing bars should be made only as required or permitted on the project drawings or in the project specifications, or as authorized by the Architect/Engimeer All welding should conform to the current edition of "Structural Welding CodeReinforcing Steel" (ANSI/AWS D1,4).

### 6.2 Lap Splices

Lap splices of \#14 and \#18 bars should not be used, except in compression only to \#11 and smaller bars.

Lap splices of bundled bars should be based on the lap splice length recommended for individual bars of the same size as the bars spliced, and such individual splices within the bundle should not overlap each other. The length of lap should be increased 20 percent for a 3-bar bundle and 33 percent for a 4 -bar bundle.

Bar laps placed in contact should be securely wired together in suct a manner as to maintain the alignment of the bars and to provide minimum clearances.

Bars spliced by noncontact lap splices in flexural members should not be spaced transversely Farther apart than one-fifth the required length of lap nor 6 in.

[^4]
## 8.4 - STANDARD PRACTICE - SPLICING \& DOWELS

## Lap Splices



Figure 1a: Contact lap splices


Figure 1b: Non-contact lap splices

A lap is when two pieces of rebar overlap to form a continuous line. This helps transfer loads properly throughout the structure. There are two types of lap splices: contact lap and non-contact lap splices (see Figure 1a and 1b). The lapped sections of contact lap splices are wired together. Lapped sections of non-contact lap splices do not touch and are permitted in practice provided the distance between lap sections meet the specified code requirements.

When using LOGIX ICFs non-contact lap splices can be used in lieu of contact lap splices.

## Lap Splices in Horizontal Rebar

In traditional construction methods, contact lap splices are more commonly used because it offers the most reliable method of ensuring the lapped sections are secure against displacement, especially during concrete pours. LOGIX ICFs can accommodate contact lap splices. However, the rebar slots in the LOGIX webs are also designed to accommodate non-contact lap splices,

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## 8.4 - STANDARD PRACTICE - SPLICING \& DOWELS continued



Figure 2a: Contact lap splices


Figure 2b: Non-contact lap splices


Figure 3: Vertical rebar in LOGIX ICF wall system
ensuring the horizontal rebar stays in place (see
Figure 2a and 2b). This minimizes the need to wire tie lapped sections and reduces labor.

The length of a lapped section (or lap length) varies depending mainly on the loading conditions, rebar size, rebar spacing, rebar grade and concrete strength. As a general rule, LOGIX recommends a lap length of 40 d or $24^{\prime \prime}$, whichever is greater, for residential construction (see Figure 1a and 1b).

## Lap Splices in Vertical Rebar

For the same reason as horizontal rebar, contact lap splices are also more commonly used in traditional construction methods. However, contact lap splices are not necessary when using LOGIX ICFs. The LOGIX web ties, which are spaced horizontally every 8 " ( 203 mm ) and about $5.25^{\prime \prime}$ ( 133 mm ) vertically per block, provides enough stability for placement of vertical rebar. Vertical rebar can be further secured if it is slid through a staggered pattern of horizontal rebar. The slots in the webs have been designed to accommodate this (see Figure 3).

## 8.4 - STANDARD PRACTICE - SPLICING \& DOWELS continued

## Footing Dowels



Figure 4: Wall/Footing connection


R611.7.1.4

Footing dowels connects the wall to the footing (see Figure 4). This prevents wall movement at the wall/footing joint caused mainly by soil loads. In residential construction, the vertical rebar in the wall itself does not contribute to the strength of the wall/footing connection and hence is not required to splice with the footing or match the spacing of the footing dowels. In cases, where lap splice may be required, non-contact lap splices are permitted.

## Lap Splices -Building \& Design Code References

International Building Code 2003 (IBC 2003), R611.7.1.4:
"R611.7.1.4 Lap Splices. Where lap slicing of vertical or horizontal reinforcing steel is necessary, the lap slice shall be in accordance with Figure R611.7.1.4 and a minimum of 40 db , where db is the diameter of the smaller. The maximum distance between noncontact parallel bars at a lap slice shall not exceed 8db."

National Building Code 1995 (NBC 1995), 4.3.3.1:

Clause 4.3.3.1 references concrete design code, CSA
A23.3 (specifically CSA A23.3, 12.14.2.3):
"12.14.2.3
Bars spliced by lap splices in flexural members shall have a transverse spacing not exceeding the lesser of one-fifth of the required lap splice length or 150mm."

## LOGIX ${ }^{\circledR}$ INSULATED CONCRETE FORMS

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## 8.5 - LOGIX R-VALUES



1. R1 denotes total R-value of form panels only (per ASTM C518 at average mean temperature of 75 deg F.). R2 denotes total R-value of a wall assembly consisting of form panels, 4 inch concrete core, $1 / 2$ inch drywall and interior airfilm. R1 and R2 are based on imperial units. R-values are based on independent testing conducted by Intertek Testing Services.

## Connect

## with a Local

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840 Division St.
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888.453.5961

11581-272 St.
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888.453.5961

6333 Unsworth Rd.
Chilliwack, BC V2R 5M3
877.789.7622

35 Headingley Rd.
Headingley, MB R4H 0A8


[^0]:    STEP 7: Solid wood bucks will require additional concrete anchors to create a permanent attachment to the concrete.

[^1]:    

[^2]:    The objective of the test: to determine whether the polypropylene reinforcing web, a component of the form system, would melt out and cause a loss of support for the non-fire side standard $1 / 2$-inch gypsum thermal barrier and consequently create a through opening in the concrete wall, and/or flaming of the polypropylene reinforcing web and expanded polystyrene foam on the unexposed side, or create openings in the concrete wall that would result in the ignition of cotton waste.

    The April 23, 2002 Intertek Testing Services NA Ltd./Warnock Hersey fire test sample was constructed to be representative of the code requirements for a foam insulated concrete wall system. The Beaver Plastics Ltd. Insulating concrete form system was tested in accordance with UBC 26-3, "Room Fire Test Standard for Interior of Foam Plastic Systems," [refer to ITS/Warnock Hersey report \#3020964(a)] and met the conditions of acceptance for a 15-minute index.

    ## CONCLUSIONS:

    The Beaver Plastics Ltd. "Logix" insulating concrete forms (EPS) protected by a $1 / 2$ " standard gypsum wallboard thermal barrier met the criteria of acceptance of ASTM E119-98, "Standard Test Methods for Fire Tests of Building Construction and Materials" for a three-hour fire resistance rating. The polypropylene web did not melt out and did not cause a loss of support for the non-fire side standard $1 / 2$ " gypsum thermal barrier. As no through-openings developed in the concrete wall section, no possibility of ignition of cotton waste occurred. There was no occurrence of burn-through or through-openings in the concrete wall, nor was there flaming of the polypropylene web and expanded polystyrene foam on the unexposed side.

    The Beaver Plastics Ltd. "Logix" insulating concrete forms (EPS) are consequently eligible for a three-hour fire resistance rating.

[^3]:    *Alternate Design: In lieu of calculations, the structural design of reinforced concrete formed by Logix Insulated Concrete Form Wall System insulated concrete form blocks for residential construction is permitted to comply with the Prescriptive Design of Exterior Concrete Walls for One- and 2-Family Dwellings (PCA 100), published by the Portland Cement Association (PCA). Buildings constructed with the Logix Insulated Concrete Form Wall System insulated concrete form system and designed in accordance with the alternate design, will not exceed a height of two stories plus a basement, where the maximum unsupported wall height is 10 feet.

[^4]:    *For more complete recommendations on bar placement, see Flacing Reinforcing Bars available from the Concrete Reinforcing Steel lnstute
    "See Reinforcement. Anchorages, Lap Splices and Connections by the Concrete Reinforcing Steel Institute

